

DMS DR-2521

NASA-CR 167,694

RESULTS OF THE AFRSI REWATERPROOFING
SYSTEMS SCREENING TEST
IN THE NASA/AMES RESEARCH CENTER (ARC)
2x2-FOOT TRANSONIC WIND TUNNEL
(OS-310)

(NASA-CR-167694) RESULTS OF THE AFRSI
REWATERPROOFING SYSTEMS SCREENING TEST IN
THE NASA/AMES RESEARCH CENTER (ARC) 2 X
2-FOOT TRANSONIC WIND TUNNEL (Chrysler
Corp.) 117 p HC A06/MF A01

N85-22467

CSCI 22B G3/16

Unclass
20521

SPACE SHUTTLE AEROTHERMODYNAMIC DATA REPORT



Data Management Services

MICHAUD ENGINEERING OFFICE



CHRYSLER
CORPORATION

March 1985

DMS DR-2521
NASA-CR 167,694

RESULTS OF THE AFRS1 REWATERPROOFING
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2x2-FOOT TRANSONIC WIND TUNNEL
(OS-310)

by

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Prepared under NASA Contract Number NAS9-17179

by

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for

Systems Engineering Division
Johnson Space Center
National Aeronautics and Space Administration
Houston, Texas

WIND TUNNEL TEST SPECIFICS:

Test Facility: ARC 2x2-Foot
Facility Test Number: 560-1-22
NASA Series Number: OS-310
Model Number: 126-0
Test Start Date: November 10, 1982
Test Completion Date: November 23, 1982
Occupancy Hours: 80

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ABSTRACT

An experimental investigation was conducted in the NASA/Ames Research Center 2x2-foot Transonic Wind Tunnel from November 10 through 23, 1982 to evaluate two AFRSI rewaterproofing systems and to investigate films as a means of reducing blanket joint distortion. The wind tunnel wall slot configuration influence on the flow field over the test panel was investigated, primarily using oil flow data, and resulted in a closed slot configuration to provide a satisfactory screening environment flow field for the test. Sixteen AFRSI test panels, configured to represent the test system or film, were subjected to this screening environment (a flow field of separated and reattached flow at a freestream Mach number of 0.65 and $q = 650$ or 900 psf). Each condition was held until damage to the test article was observed or 55 minutes if no damage was incurred.

The data used to evaluate the candidate AFRSI configurations consisted of a comparison of the time to failure of the AFRSI panels from this test with the time to failure of previous successful AFRSI test panels. All objectives related to AFRSI rewaterproofing and to the use of films to stiffen the blanket fibers were achieved.

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INTRODUCTION

A sequence of environments test program was initiated in May 1982 to provide experimental data on the life of AFRSI material under expected environmental loadings. This program was designed to sequentially expose the AFRSI to wind/rain environments, aerodynamic and acoustic ascent loadings, and radiant thermal heating. This sequence simulates the loading environments encountered during each flight; on the launch pad, during lift-off, and during ascent and entry.

During the initial series of wind/rain, acoustic, and heating tests, the candidate rewaterproofing material for the AFRSI proved inadequate when subjected to entry temperatures above 1500°F. In addition, wind tunnel tests revealed that the blanket joints were easily distorted. As a result, films were being contemplated for use in stiffening the blanket ends to minimize gaps between the blankets due to ascent airloads. Some of these films were candidate rewaterproofing materials to be applied to the AFRSI.

Test OS-310 was developed in response to these findings and was conducted in the NASA/Ames Research Center 2x2-foot Transonic Wind Tunnel from November 10 through November 23, 1982. The purpose of this investigation was to evaluate two AFRSI rewaterproofing systems and to investigate films as a means of reducing blanket joint distortion. In addition, needle damage inflicted to the AFRSI during the sewing process was investigated to determine how it affected the life of the AFRSI material.

During earlier tests with the same test set-up, local flow perturbations and lack of uniformity were encountered. Oil flow visualization and pressure

INTRODUCTION (Concluded)

calibration tests were carried out in an attempt to eliminate the local flow perturbations and obtain a more two-dimensional flow field in the test section. Various separation wedge and tunnel wall slot configurations were tested at Mach numbers ranging from 0.65 to 0.82 and dynamic pressures of 138 to 1000 psf. A reasonable simulation of two-dimensional flow was achieved.

A total of 16 AFRSI specimens were tested: nine had blanket joints while the other seven were one-piece baseline configurations. Specimen testing was accomplished at a constant Mach number of 0.65 with dynamic pressures of 650 or 900 psf. Each condition was held until damage to the test article was observed or 55 minutes if no damage was incurred.

This report contains information on the conduct of the test, details of the model and instrumentation, a summary of the test schedule and conditions, plotted and tabulated pressure data, and photographs of the AFRSI specimens tested.

NOMENCLATURE

<u>SYMBOL</u>	<u>MNEMONIC</u>	<u>DEFINITION</u>
CONF		Test Configuration
C_p	CP	Pressure coefficient, data
HW		Wall position
IML		Inner Moldline
M	MACH	Freestream Mach number
OML		Outer Moldline
P_∞	P	Freestream static pressure, psia
P_l	PL	Local static pressure, psia
P_t	PT	Freestream total pressure, psia
q	Q	Freestream dynamic pressure, psf
Re	RE or RN	Freestream Reynolds number, per ft
T_s	TS	Freestream static temperature, °R
T_t	TT or T_{TF}	Freestream total temperature, °R or °F
V_∞	V	Freestream velocity, ft/sec
X	X	Longitudinal distance positive, inches aft of panel centerline
Y	Y	Lateral distance positive, inches right of panel centerline
ρ	RHO or RO	Freestream density, slugs/ft ³
PRMS	PRMS	RMS value of the variations from the mean value of the loca pressure, psi
WH		Wedge height, inches
WL		Wedge length, inches
WX		Wedge direction position, inches

REMARKS

During run numbers 10, 30, 40, 41, 42, 43, and 50, the tunnel data acquisition and Scanivalves showed some anomalies. Attempts to clear the problem were not successful. Since the oil flow test could be achieved without the pressure data, testing was resumed without any further delay. Computer and Scanivalve problems were solved after run 43.1.

During the initial pretest calibration, 22 Kulites were available of which three were found to be defective. These were Kulite numbers 17, 22, and 204. These Kulites were replaced with Kulite numbers 19 and 21. A total of 18 Kulites were used to obtain the fluctuating acoustic data during the calibration runs.

Data from a previous test (OS-301) in the ARC 2x2-foot TWT showed a lack of flow symmetry and regions of concentrated turbulence over the AFRSI test panels. In response to these conditions, visualization tests were conducted during Test OS-301 which showed a cross flow on the panels. This cross flow was apparently caused by air from the plenum chamber being drawn into the test section by the action of the low pressure field created by the presence of the separation wedge. For this reason, thorough oil flow and calibration runs were conducted during Test OS-310 and a satisfactory screening environment was achieved by mechanically backing all wall slots.

CONFIGURATIONS INVESTIGATED

The configurations used in this test did not duplicate any geometric surface of the Space Shuttle orbiter. A test article holding fixture, used during previous tests, was mounted in the tunnel's movable wall. The fixture, Model 115-0, was modified so that it would place the test articles in the center of the test section. During Test OS-310, the tunnel's movable wall was kept in the flush position (HWe0). The porosity of two of the tunnel surfaces was controllable. The other two had no provisions for any porosity. Four wedges were used to disturb the tunnel flow. All wedges had a 45-degree ramp to the flow. Three different wedge heights were used, 0.5, 1.0, and 1.5 inches. One wedge had a length of 23.6 inches, all the others were 20.75 inches long. The wedges were positioned at either $X = -11.9$ inches or $X = -16.4$ inches.

A dummy panel with grid marking was used during the oil flow portion of Test OS-310. Another dummy panel with instrumentation installed was used to calibrate the pressure distribution in the area of the test articles.

Sixteen test articles were used during this test. Each had an exposed surface of 15.5 x 12.5 inches and was mounted flush to the tunnel wall in the holding fixture. A description of each panel is presented in Table III.

INSTRUMENTATION

Data for Test OS-310 consisted of time averaged and fluctuating pressure measurements. The 32 static pressure orifices in the fixture were used during the entire test. Fifteen additional orifices were used with the calibration panel.

Twelve Kulite transducers in the fixture were also used during the entire test. The calibration panel contained 22 additional Kulite transducers.

The locations of all this instrumentation are shown in Figure 1.

TEST FACILITY

The ARC 2x2-foot wind tunnel was used for these tests. The tunnel is of the continuous flow type with variable porosity test section walls surrounded by a plenum chamber. Mach number is continuously variable over the range from 0.6 to 1.4 and dynamic pressure is continuously variable over the range from 200 to 1500 psf.

The tunnel can be operated so that one section of the side wall moves up to 1.4 inches into the airstream. The upstream edge of the movable wall is a sharp edged splitter plate which scoops off all or part of the tunnel sidewall boundary layer. It is possible to position the wall to achieve a boundary layer thickness from 0.25 to 1.0-inch in the panel test region.

TEST PROCEDURE

The test was conducted in three parts. First, a study was made, using oil, to define the surface flow pattern. The tunnel's wall porosity, Mach, and dynamic pressure were varied. The flow separator wedge height, length, and X-station were also varied.

After a usable flow field was found, an instrumented calibration panel was installed in the tunnel. The time-averaged pressures and the acoustic pressures were recorded for various tunnel and wedge conditions. When the proper environments had been defined, the test articles were inserted into the fixture and run. A detailed run schedule is presented in Table II.

DATA REDUCTION

Standard tunnel equations were used to compute all tunnel conditions.

The time-averaged pressure data was recorded and reduced to standard coefficient form by the facility using:

$$C_p = (P_L - P_\infty) \times 144/q$$

Plots of this data are presented in Figures 4 through 8. This data is tabulated in Appendix A.

Fluctuating acoustic pressure data was recorded on magnetic tape, then played back so that the Vibration and Acoustics group could analyze the data. The data was converted to dB's using:

$$dB = 10 \log_{10} \left(\frac{P_{RMS} \times 10^9}{2.9007} \right)^2$$

Representative data are presented in Figures 9 and 10.

REFERENCES

1. STS82-0762, "Pretest Information for AFRSI Rewaterproofing Screening Test OS-310 in the Ames Research Center (ARC) 2x2-foot Transonic Wind Tunnel" (October 1982)
2. V&A-280-301-83-021, "Wind Tunnel Environments Obtained for AFRSI Rewaterproofing Screening Test OS-310 Conducted in the ARC 2x2-foot Transonic Wind Tunnel" (March 22, 1983)

TABLE I

TEST CONDITIONS

Number	Reynolds Number (Per Ft x 10 ⁻⁶)	Dynamic Pressure PSF	Stagnation Temperature Deg F
0.3	2.17	140	80
0.4	2.67	225	80
0.5	3.15	325	80
0.6	3.53	425	80
0.6	4.77	575	80
0.6	6.02	725	80
0.6	7.05	850	80
0.6	8.30	1000	80
0.65	3.73	480	80
0.65	5.05	650	80
0.65	6.22	800	80
0.65	7.00	900	80
0.65	7.77	1000	80
0.7	3.96	540	80
0.7	5.13	700	80
0.7	5.87	800	80
0.7	6.60	900	80
0.75	4.18	600	80
0.75	4.52	650	80
0.75	5.40	775	80
0.75	6.96	1000	80
0.8	4.25	640	80
0.85	4.20	660	80
0.85	6.37	1000	80

ALES 2x2

7	13	19	25	31	37	43	49	55	61	67	73
MW = Wall Height, WHT = $y = 1.5"$ flow separator $x = 1.0"$ flow separator $z = 0.5"$ flow separator											
*Tunnel Floor & Ceiling Tape 50% Span Tunnel Tape 50% Span Top and Bottom Plus Porosity Bars Top and Bottom Closed.											

TEST: OS-310

AES 2x2

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DATA SET/RUN NUMBER COLLATION SUMMARY

DATE:

date	run no.	CONFIGURATION	WHI	H ₂ O			PSF	TEMP	wedge in.		remarks
				Mach	P _t	P _s			WHT	WLT WX	
	64-6	OIL FLOW + KVLUTES	0	.606	30.02	23.42	135.9	60.3	Y	23.6 -16.4	Porosity bars closed.
	65-1		0	.607	30.30	23.50	133.6	65.7	Y	23.6 -16.4	
	66-1		0	.611	30.56	23.28	137.1	70.9	Y	23.6 -16.4	
	68-1		0	.604	30.64	23.40	135.5	77.3	Y	23.6 -16.4	
	69-1		0	.605	30.35	23.95	139.9	82.7	Y	23.6 -16.4	
	70-2		0	.657	30.05	23.47	140.2	69.9	Y	23.6 -16.4	
	71-1		0	.653	30.67	23.55	145.3	75.4	Y	23.6 -16.4	
	72-1		0	.654	30.50	23.70	140.0	81.3	Y	23.6 -16.4	
	73-1	Y	0	.651	30.31	23.60	140.1	85.3	Y	23.6 -16.4	
	78-3	CALIBRATION PANEL	0	.651	30.09	23.62	135.3	64.8	Y	23.6 -16.4	
	79-1		0	.658	30.00	23.67	140.8	68.4	Y	23.6 -16.4	
	80-1		0	.652	30.04	23.61	139.6	76.5	Y	23.6 -16.4	
	81-1		0	.651	30.97	23.36	133.8	81.5	Y	23.6 -16.4	
	82-1	Y	0	.653	30.95	23.50	139.3	83.0	Y	23.6 -16.4	Y

1 7 13 19 25 31 37 43 49 55 61 67 73 75 76

WHI = Wall Height

WHT = y = 1.5" flow separator

x = 1.0" flow separator

z = 0.5" flow separator

Project 560-1-22

AES 2x2

TEST: OS-310		DATA SET/RUN NUMBER COLLATION SUMMARY										DATE:	
date	run no.	CONFIGURATION	hw	sw	blch	Hg		PSF	time	wedge in.		remarks	
						Pt	Ps			WHT	WLT WX		
	83-1	CALIBRATION PANEL	0		235	30.03	19.20	647.2	79.7	X	20.8	-16.4	Tunnel blockage
	84-1		0		750	30.06	20.71	576.0	78.4	X	20.8	-16.4	dropped 0.1 of a Mach
	85-2		0		752	40.00	22.56	771.4	82.6	X	20.8	-16.4	Porosity bars closed.
	86-2		0		750	53.50	36.16	1008	87.8	X	20.8	-16.4	
	87-3		0		849	28.91	17.30	144.2	78.7	Z	20.8	-16.4	
	88-2		0		851	40.94	27.97	1003	85.9	Z	20.8	-16.4	
	89-1	Y	0		848	45.21	28.25	1004	89.4	Z	20.8	-16.4	Y
	100-10	TEST PANEL #2	0		652	46.32	31.05	633.7	86.4	Y	23.6	-16.4	(control panel)
	101	#2	0		652	43.85	42.12	990	86.5	Y	23.6	-16.4	Porosity bars closed
	102-18	#1	0		652	57.22	42.13	901.8	87.8	Y	23.6	-16.4	
	103-6	#1-C	0		650	57.21	43.11	901.3	88.7	Y	23.6	-16.4	
	104-5	#11	0		653	57.07	42.84	904.5	82.8	Y	23.6	-16.4	
	105-1	#12	0		651	57.19	43.02	902.1	84.8	Y	23.6	-16.4	
	106*	#1-C	0		645	51.33	45.00	900	76.4	Y	23.6	-16.4	
	107-1	Y #13	0		652	57.33	43.08	902.1	83.2	Y	23.6	-16.4	Y

Run 106, 3 min. from air on to shutdown. Not on condition. Panel #1-C was repaired and coated.

Note: Time-cumulative minutes on-condition.

x = 1.0" flow separator

z = 0.5" flow separator

Project 560-1-22

AIES 2x2

TEST: OS-310		DATA SET/RUN NUMBER COLLATION SUMMARY										DATE:			
date	run no.	CONFIGURATION	hw	sw	fact	Hg		PSF	temp	time	wedge ~ in.		remarks		
						Pt	P _s				WHT	WLT			
	108-4	TEST PANEL #2-C	0			654	57.15	42.87	900.9	90.5	8	Y	23.6	-16.4	Porosity bars closed
	109-17	#8	0			650	35.64	31.09	690.5	82.2	37	Y	23.6	-16.4	
	110-4	#14	0			652	52.09	42.89	903.5	83.8	10	Y	23.6	-16.4	
	111-3	#16	0			654	57.35	42.96	909	84.0	5.5	Y	23.6	-16.4	
	112-12	#2-C	0			650	57.16	43.02	901	94.9	28	Y	23.6	-16.4	
	113-10	#15	0			651	57.14	43.0	902.7	94.9	21.5	Y	23.6	-16.4	
	114-7	#3	0			651	41.27	31.04	651.4	85.2	14	Y	23.6	-16.4	
	115-6	#4	0			652	41.27	31.02	653.4	80.3	56	Y	23.6	-16.4	
	116-2	#5	0			652	41.35	31.07	654.1	78.0	26	Y	23.6	-16.4	
	117-2	#6	0			651	41.37	31.11	653	70.2	14	Y	23.6	-16.4	
	118-2	#7	0			654	41.95	31.09	652.7	71.0	10.5	Y	23.6	-16.4	Y

TEST RUN NUMBERS

7 13 19 25 31 37 43 49 55 61 67 73 79

HW = Wall Height
 WHT = y = 1.5" flow separator
 x = 1.0" flow separator
 z = 0.5" flow separator

TABLE III

<u>Date</u>	<u>T/A</u>	<u>Needle Damage</u>	<u>Joint</u>	<u>Rewater-proofing</u>	<u>Thermal # of Cycles</u>	<u>Test Condition</u>	<u>Time Min. On-condition</u>	<u>Notes</u>
11-16-82	2	Not per spec Moderate	Yes	No	No	M=0.65 Q=650 psf	55	Some thread failure
11-17-82	2	Not per spec Moderate	Yes	No	No	M=0.65 Q=950 psf	9	Fabric frays along stitch-line almost to failure (fwd and aft areas)
11-17-82	1	Not per spec Moderate	No	No	No	M=0.65 Q=905 psf	21	Fabric failure (aft corner)
11-17-82	1-C	Minimal	No	No	No	M=0.65 Q=901 psf	9	premature shutdown due to fabric frays along T.E. Fabric at T.E. pulling out from frame. Will coat damage areas, then put back into tunnel.
11-17-82	11	Not per spec Moderate	Yes	Z6079 + Acrylic Film	400; 1500 (1)	M=0.652 Q=901 psf	2	Fabric/thread failure (fwd center)
11-17-82	12	Yes	Yes	Z6079 + Acrylic Film	600; 1500 (1)	M=0.651 Q=902 psf	2	Fabric failure along stitch-line (total aft end)
11-18-82	1-C	Minimal	No	No	No	M=0.645 Q=900 psf	0	Damaged area from previous run, failed before obtaining tunnel conditions. 3 min. from air on to shutdown.

TABLE III (Continued)

Date	I/A	Needle Damage	Joint	Rewater-proofing	Thermal # of Cycles	Test Condition	Time Min. On-condition	Notes
11-18-82	13	Minimal	No	Z6079 + Acrylic Film	800; 1500 (5)	M=0.650 Q=900 psf	5	Pad puffed significantly prior to failure, due to major thread damage. (Total aft end)
11-18-82	2-C	Minimal	Yes	No	No	M=0.655 Q=910 psf	8	Shutdown prematurely due to fabric fray. Will coat damage area, then retest.
11-18-82	8	Not to spec Moderate	Yes	Z6079 + Acrylic Film	800; 1500 (5)	M=0.652 Q=655 psf	37	Failure initiation adjacent to stitch row significance puffing prior to failure. Pad had W/P exposure. (forward center)
11-19-82	14	Minimal	No	Z6079 + Acrylic Film	1000; 1500 (9)	M=0.650 Q=900 psf	10	Major thread breakage; puffing of pad prior to failure, fabric pulled out from TE frame contributing to failure.
11-19-82	16	Broken yarns Sidewall Minimal	Yes	No	No	M=0.650 Q=900 psf	5.5	Fabric failure did not occur on sidewall. Sidewall looks good. Failure occurred adjacent to stitchline. (Mid edge)
11-19-82	2-C	Slight	Yes	No	No	M=0.650 Q=901 psf	28	Fabric failure did not occur on sidewall. (Aft side & edge)
11-19-82	15	Moderate	Yes	No	No	M=0.654 Q=902 psf	22	Fabric failure adjacent to stitchline. (Aft center)

TABLE III (Concluded)

Date	T/A	Needle Damage	Joint	Rewater-proofing	Thermal # of Cycles	Test Condition	Time Min. On-condition	No. s
11-19-82	3	Yes	Yes	No	200; 1500 (1)	M=0.653 Q=652 psf	14	Thread breakage caused failure. (Aft center)
11-22-82	4	Yes	Yes	Silane Z6079	400; 1500 (1)	M=0.653 Q=654 psf	56	No mileage. Thread breakage and slight puffing.
11-22-82	5	Yes	Yes	Silane Z6079	600; 1500 (1)	M=0.654 Q=654 psf	26	Thread failure caused blanket failure. Significant puffing prior to failure. (Aft center)
11-22-82	6	Not per spec. Moderate	No	Silane Z6079	800; 1500 (5)	M=0.651 Q=653 psf	14	Thread breakage caused failure. I.E. Fabric on verge of pulling out from frame. (Aft corner)
11-23-82	7	Per spec. Minimal	No	Silane Z6079	1000; 1500 (7)	M=0.650 Q=653 psf	10.5	Thread breakage caused failure. (Trailing edge)

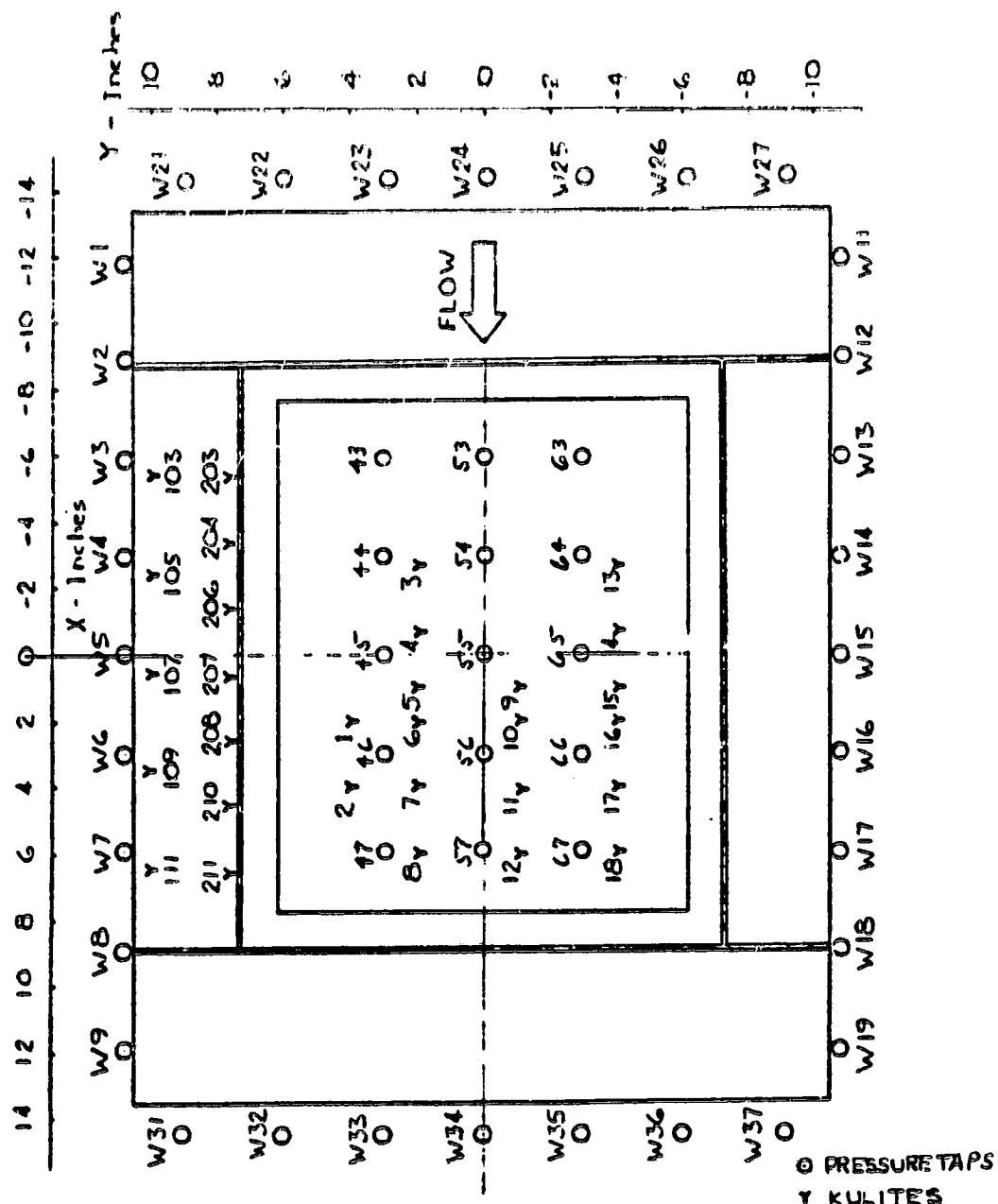


Figure 1. INSTRUMENTATION LOCATION

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Space Systems Group



Hawthorn
International



Figure 2.0

Run 10 $M = 0.81$ $P_T = 29.92$ in. Hg $q = 633$ psf
Tunnel floor and ceiling taped 50% span.
 $W_H = 1.5$ $W_L = 23.6$ $W_X = 16.4$



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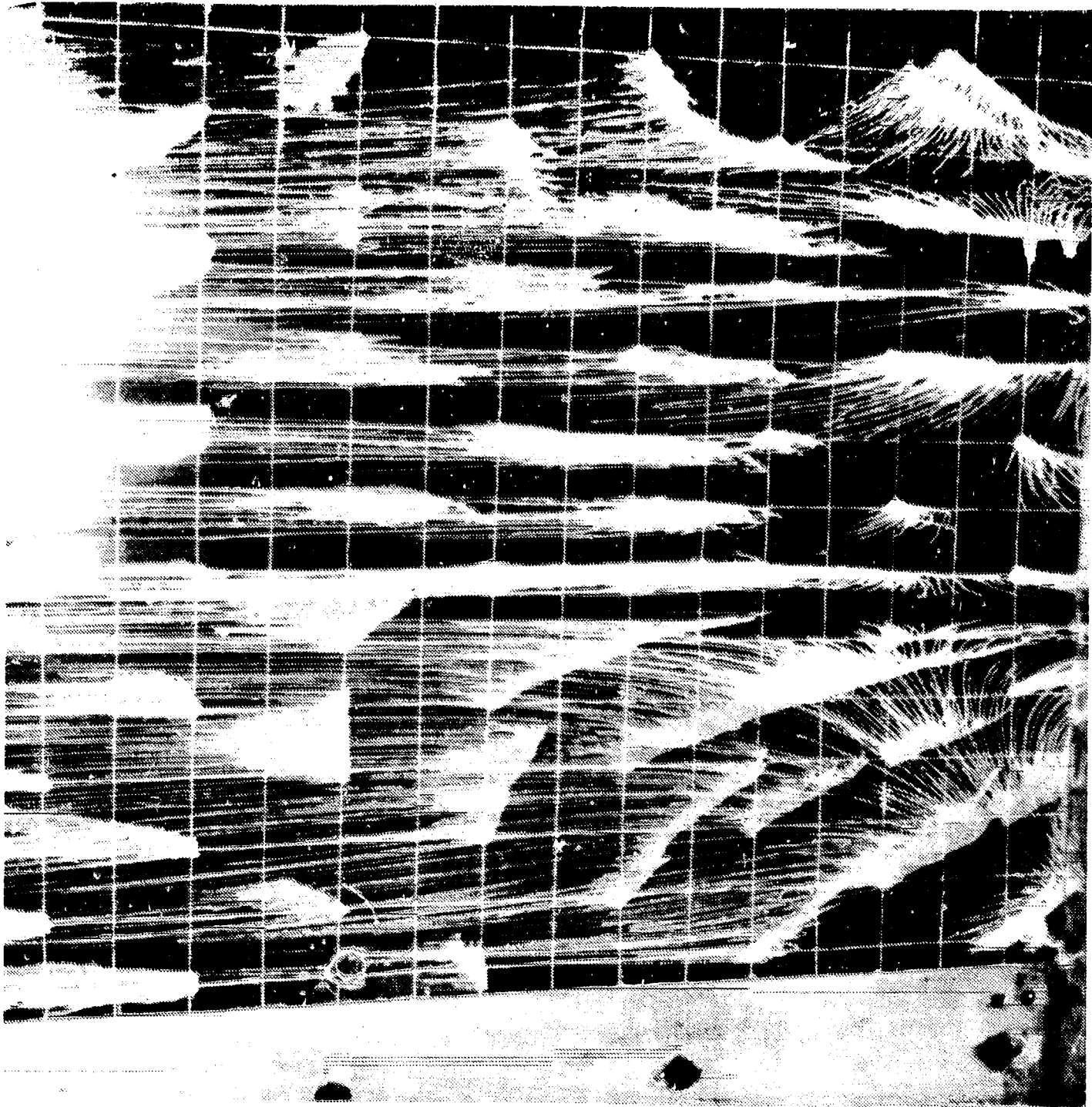


Figure 2.b

Run 30 $M=0.74$ $P_T=29.99$ $q=568$

Tunnel taped 50% span top and bottom;
porosity bars closed top and bottom.

$W_I=1.5$ $W_L=23.6$ $W_X=16.4$



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Figure 2.c

Run 41 M=0.75 P_T=34.63 q=115

Porosity bars closed top and bottom.

WI=1.5 WL=23.6 WX=-16.4



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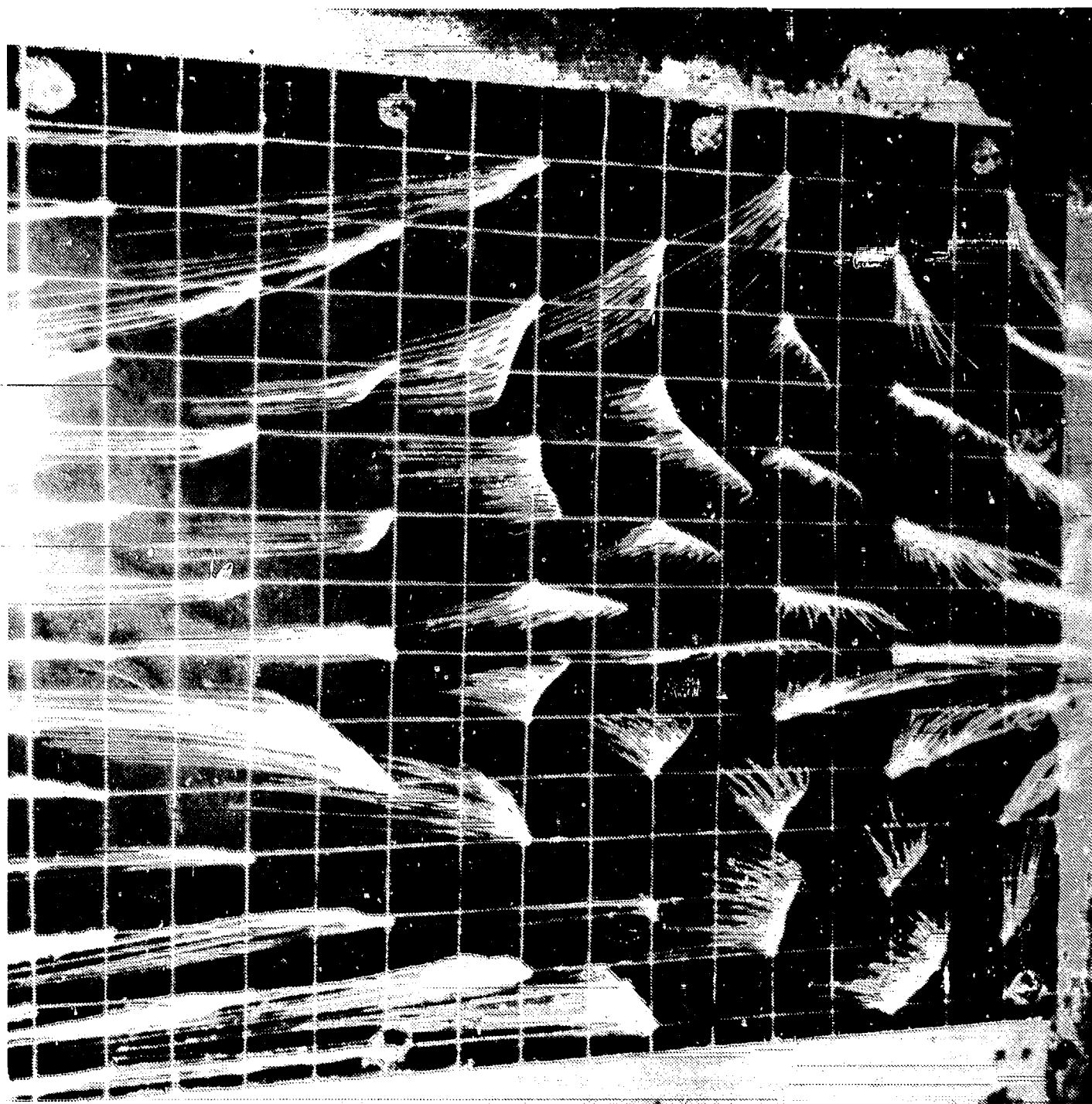


Figure 2.d Run 43 M=0.83 $P_T=34.97$ $q=106$
Porosity bars open 0.025 inch top and bottom.
WI=1.5 WL=23.C WX=-16.4

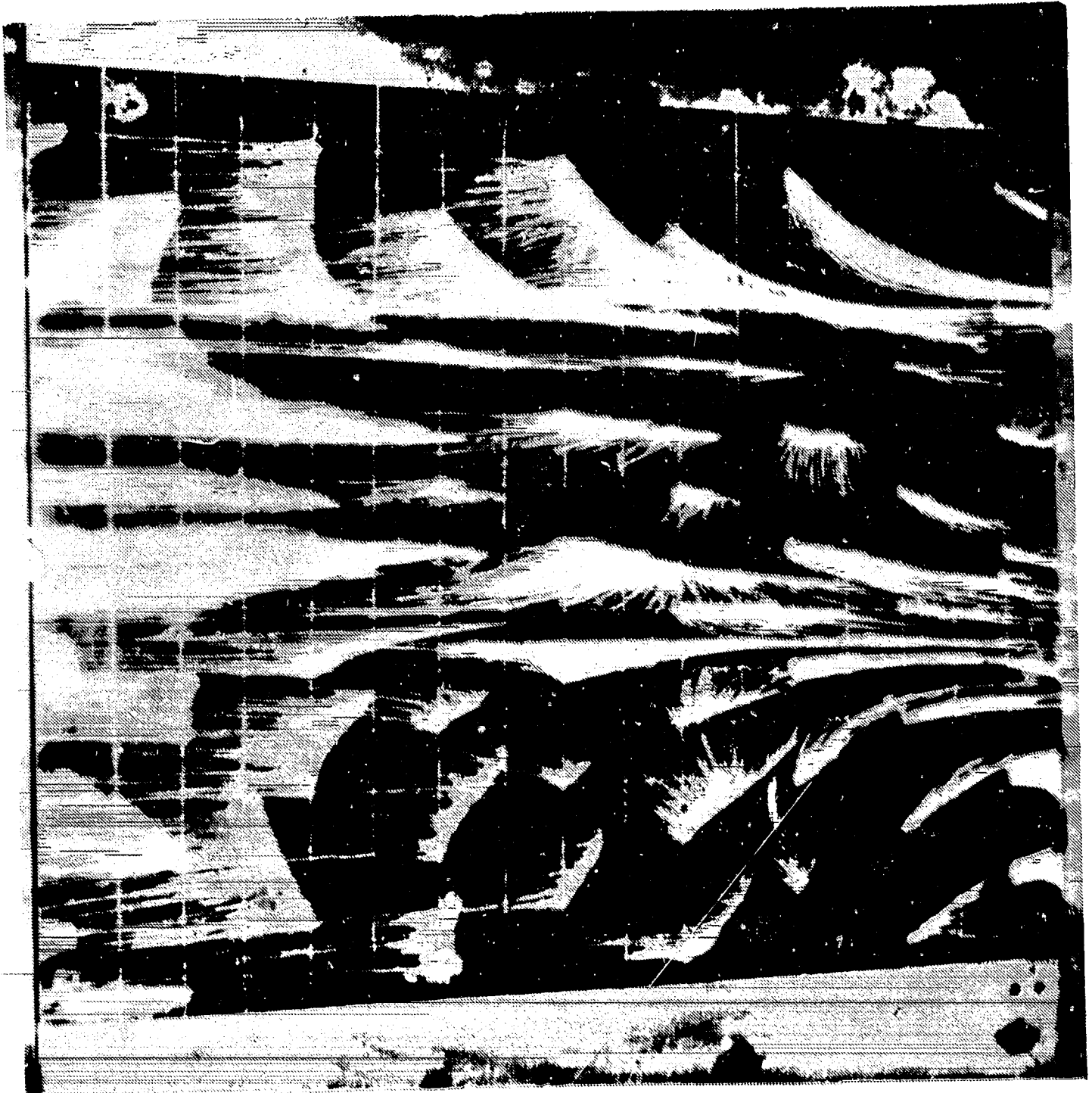
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Figure 2.c Run 51 $M=0.75$ $P_T=29.8$ $q=1000$
Run 52 $M=0.75$ $P_T=35.3$ $q=1010$

After Runs 51 and 52, porosity bars closed
top and bottom.

$Wt=1.5$ $WL=23.6$ $WX=11.9$

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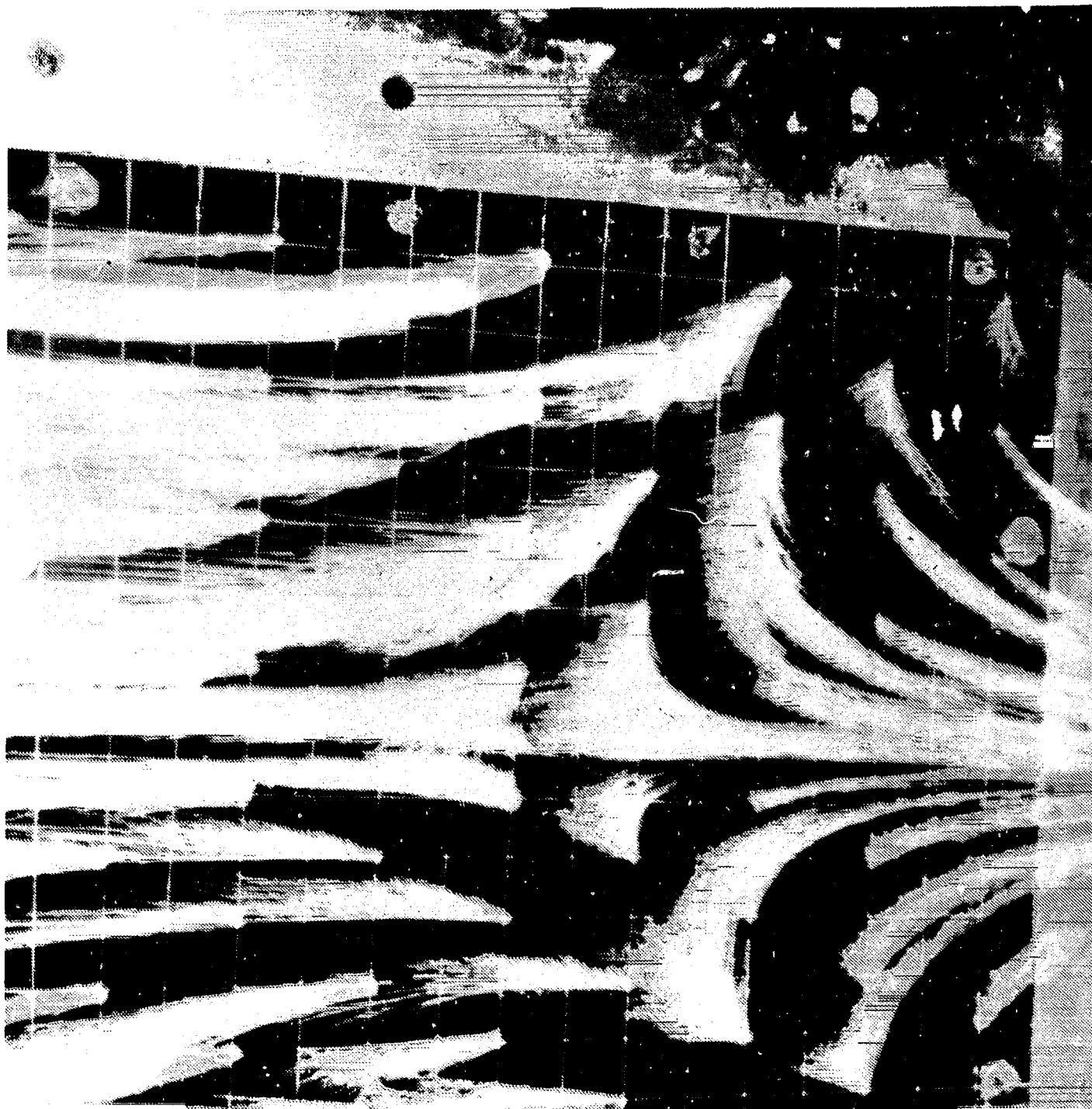


Figure 2.f Runs 54→62 $M=0.30→0.77$ $P_T=30→44$ $q=140→880$

Porosity bars closed top and bottom.

WH=1.5 WL=20.8 WX=16.4



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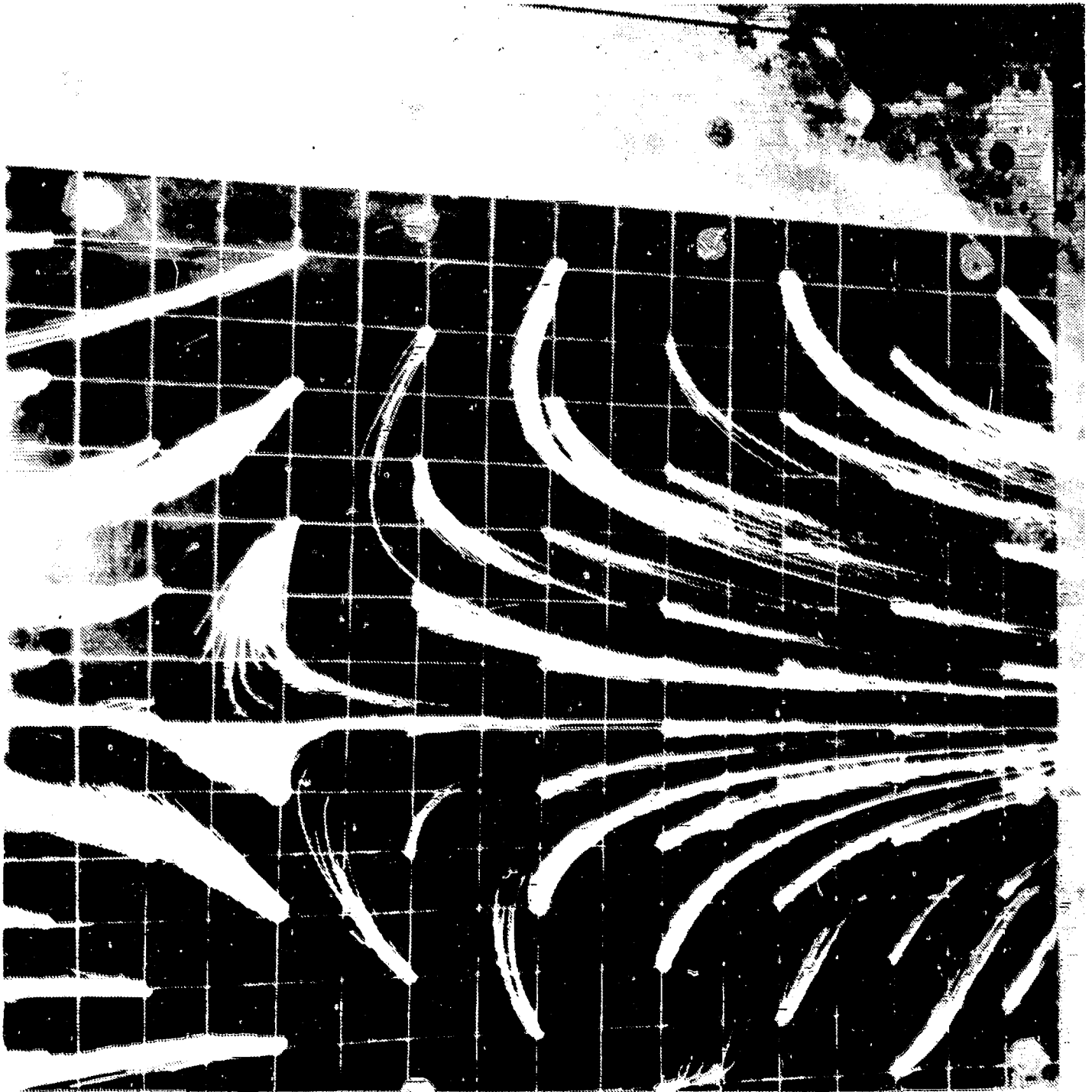


Figure 2.g Runs 64→69 $M=0.6$ $P_T=30→70$ $q=425→1000$
(No Run 67)

Porosity bars closed top and bottom.

WH=1.5 WL=23.6 WX=-16.4

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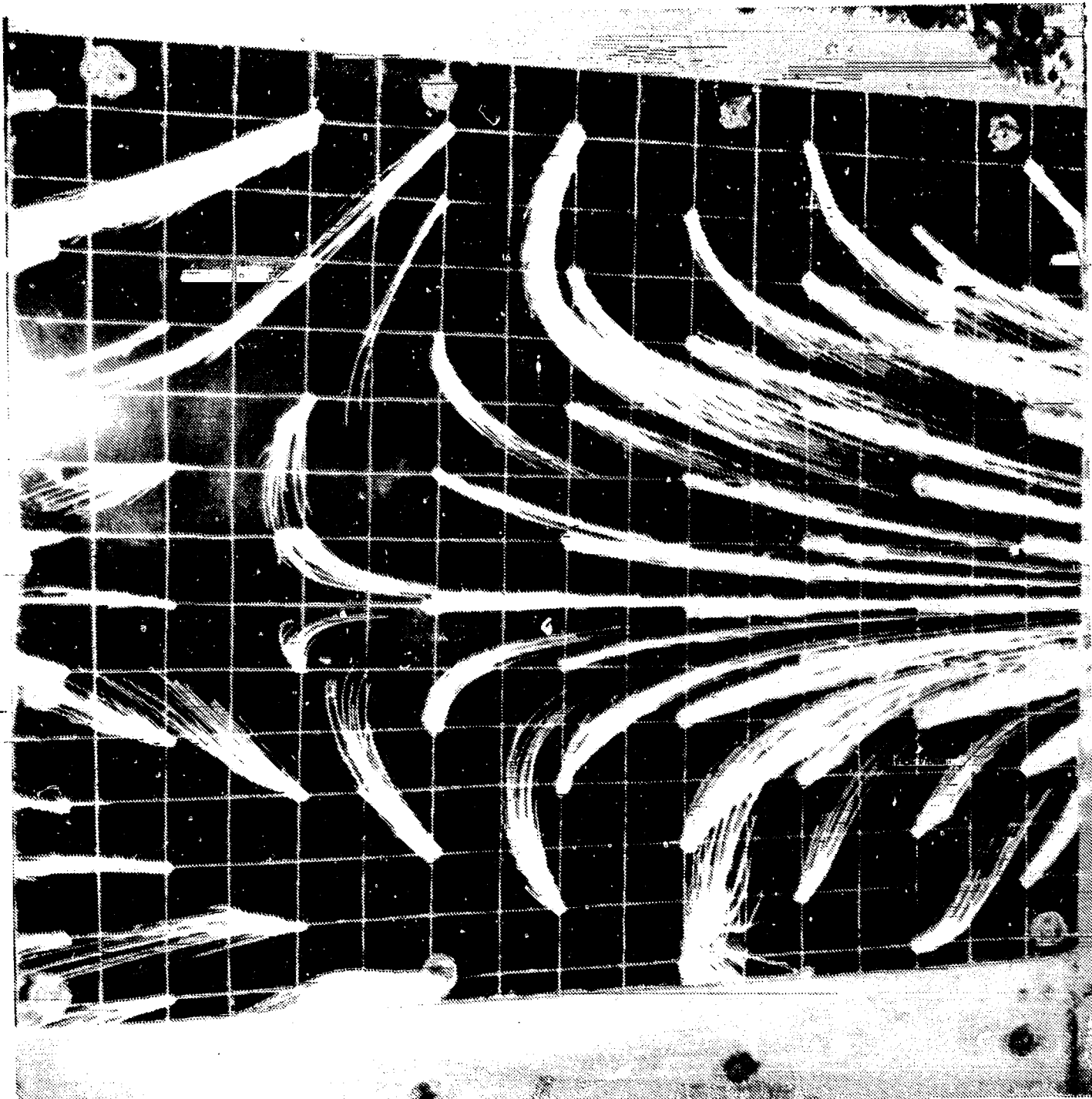
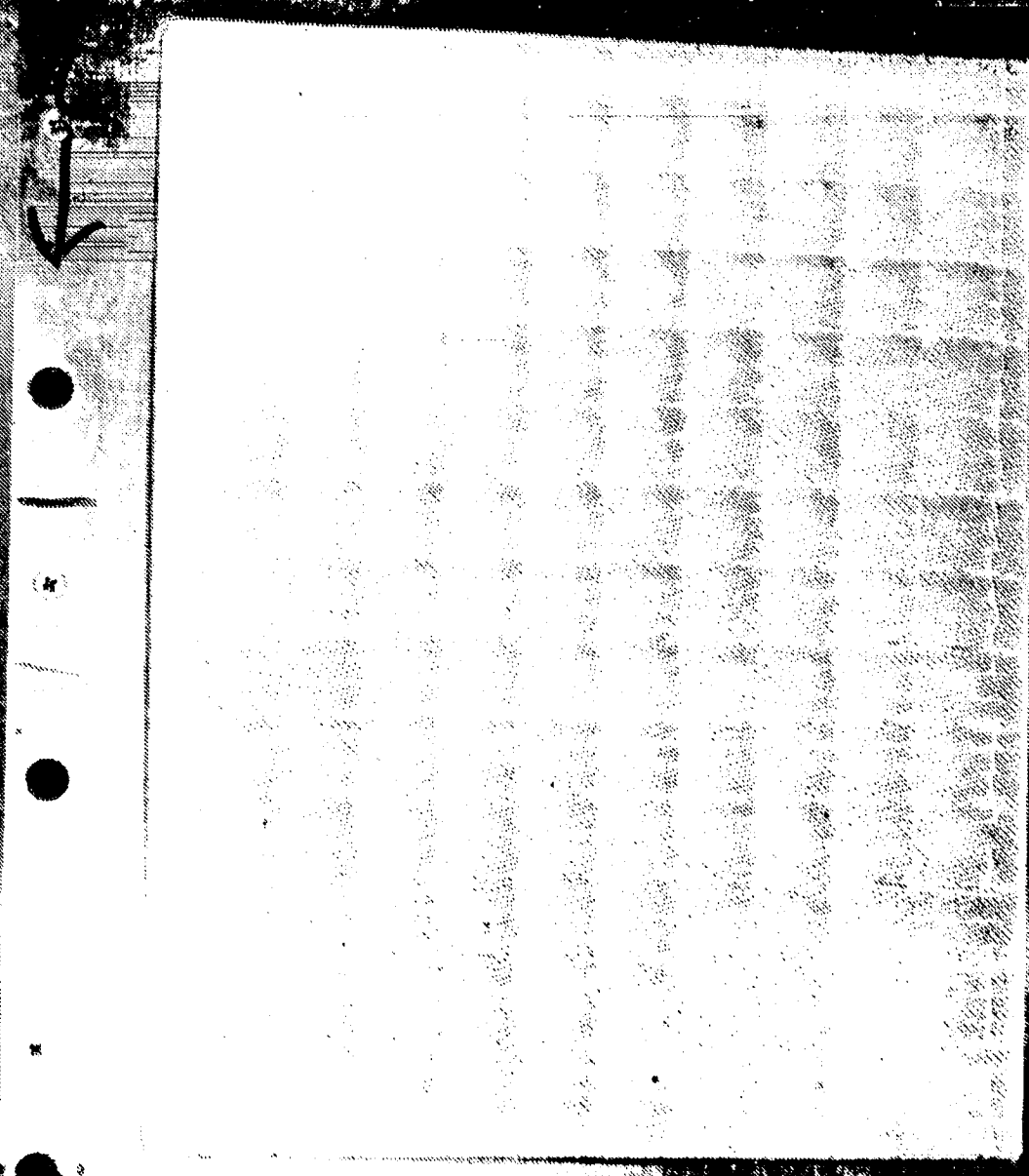


Figure 2.h Run 70 → 73 $M=0.65$ $P_T=30 \rightarrow 63$ $q=480$ 1000
Porosity bars closed top and bottom.
 $Wt=1.5$ $WL=23.6$ $WX=-16.4$



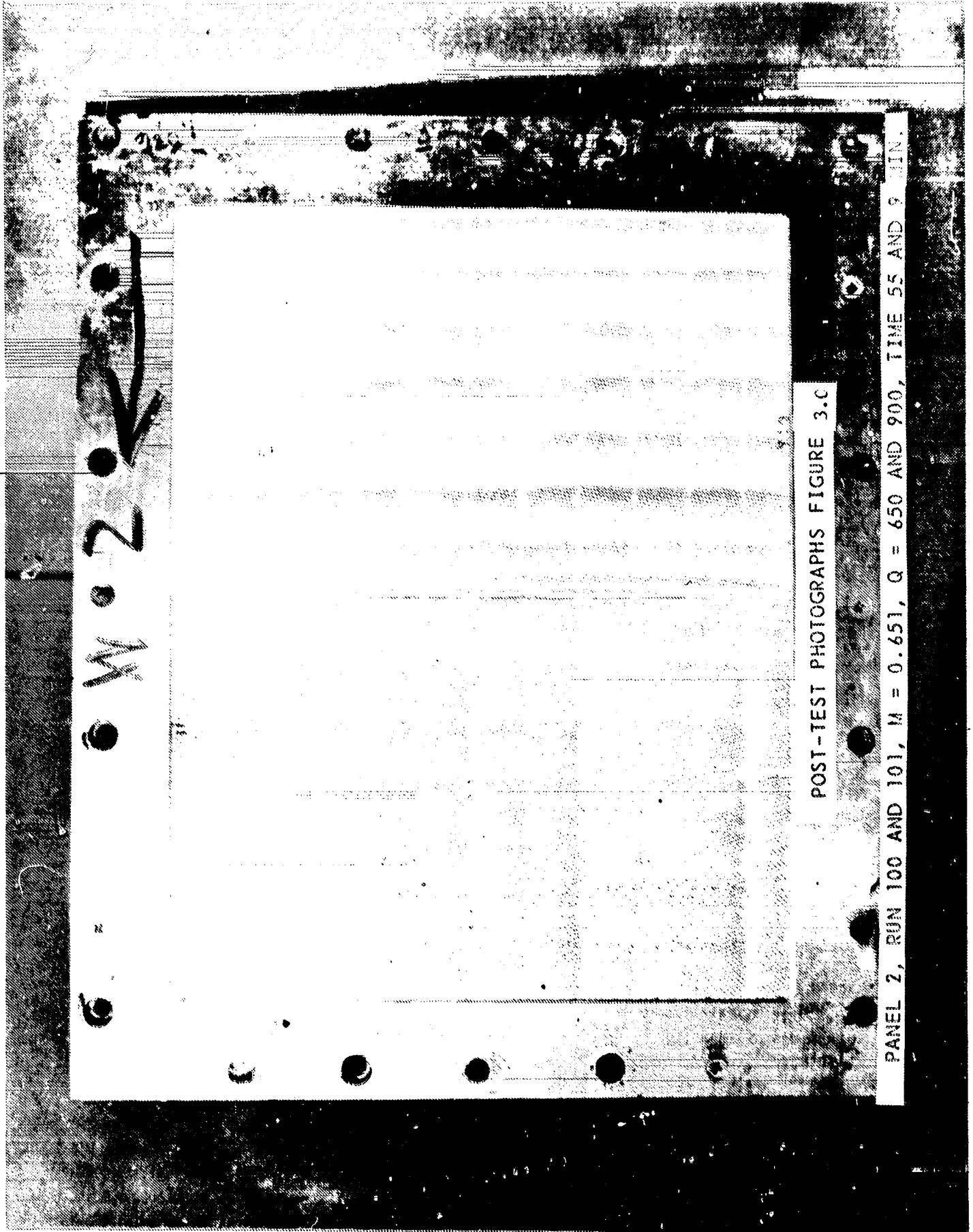
POST-TEST PHOTOGRAPHS FIGURE 3.A

PANEL 1, RUN 102, M = 0.652, Q = 905, TIME = 21 MIN.

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POST TEST PHOTOGRAPHS FIGURE 3.B

PANEL 1-C, RUN 106, $M = 0.643$, $Q = 900$, TIME = 12 MIN.



W. 2



POST-TEST PHOTOGRAPHS FIGURE 3.0

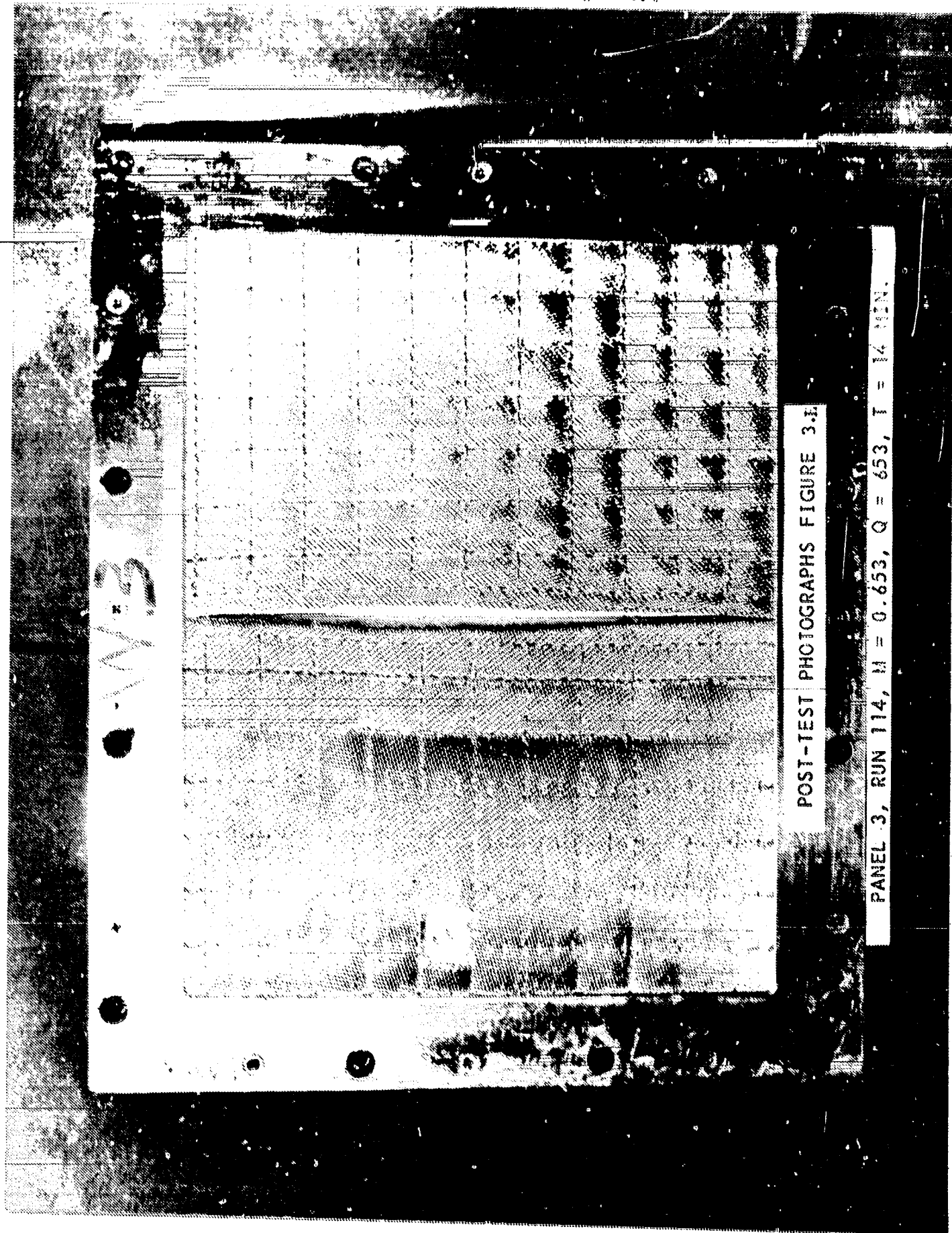
PANEL 2, RUN 100 AND 101, M = 0.651, Q = 650 AND 900, TIME 55 AND 9 MIN.

● 26 ●

POST-TEST PHOTOGRAPHS FIGURE 3.D

PANEL 2-C RUN 112, M = 0.650, Q = 901, T = 28 MIN.

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POST-TEST PHOTOGRAPHS FIGURE 3.1

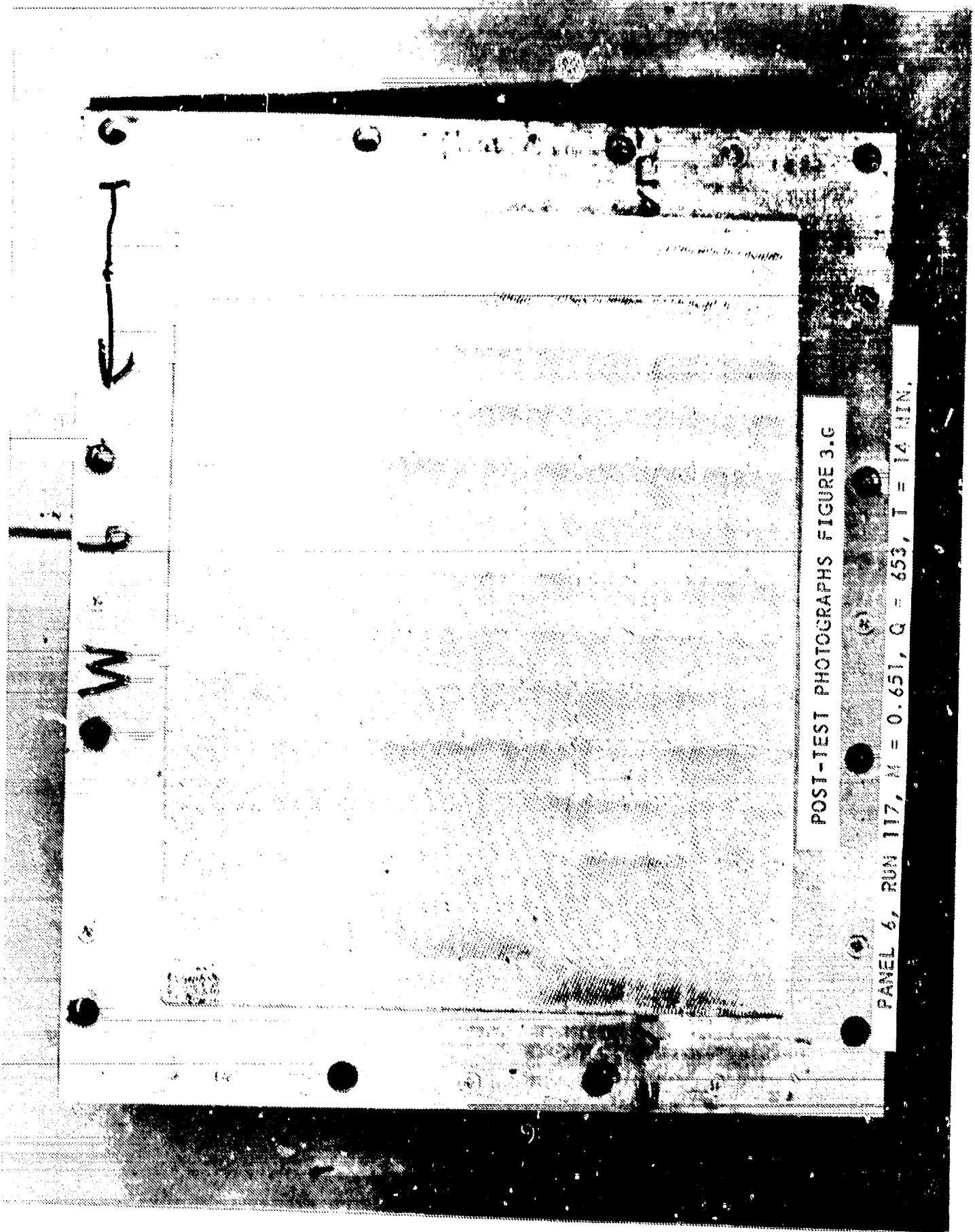
PANEL 3, RUN 114, M = 0.653, Q = 653, T = 14 MIN.

W-4

POST-TEST PHOTOGRAPHS FIGURE 3.1

PANEL 4, RUN 115, M = 0.653, Q = 654, T = 56 MI.

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POST-TEST PHOTOGRAPHS FIGURE 3.11

PANEL 7, RUN 118, M = 0.050, Q = 653, T = 10.5 MIN.

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POST-TEST PHOTOGRAPHS FIGURE 3.1

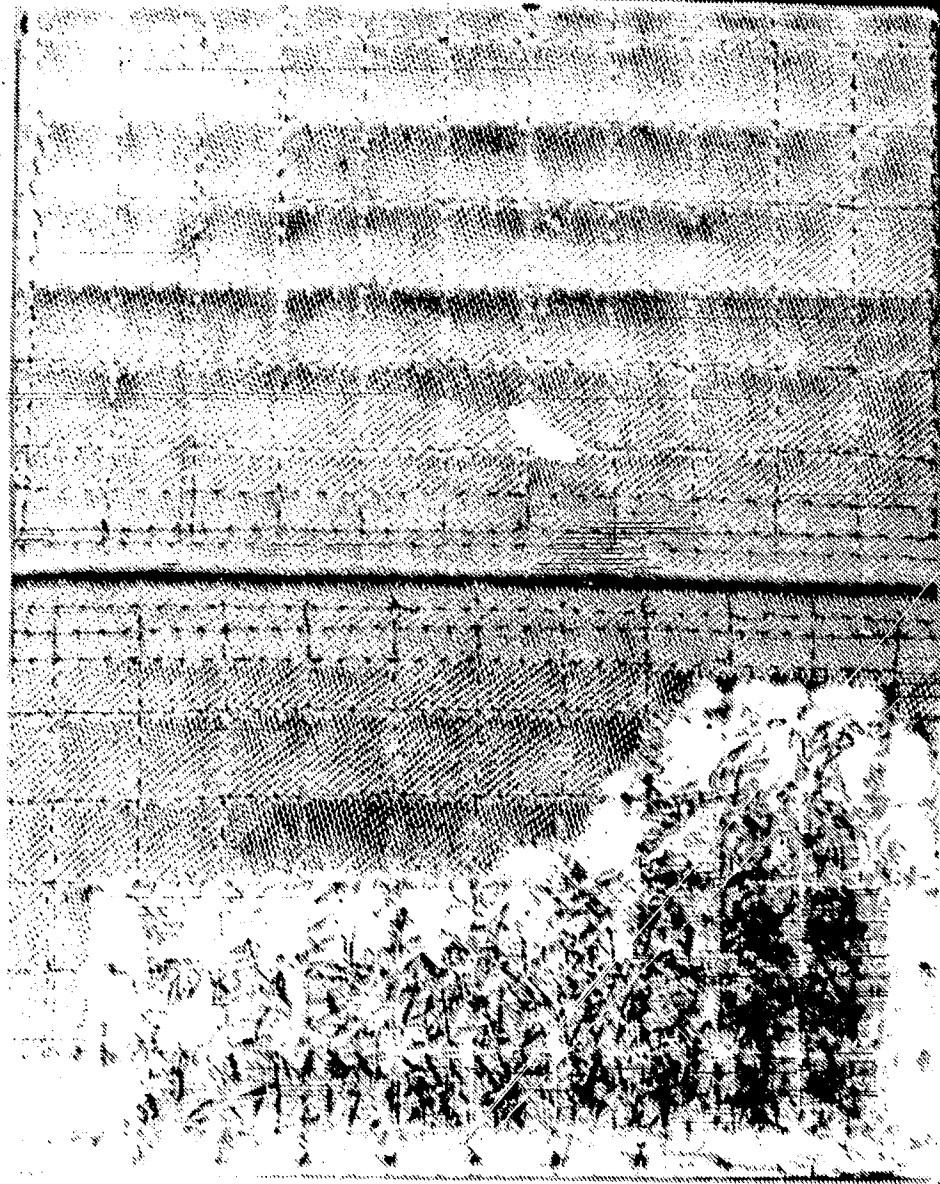
PANEL 8, RUN 109, H = 0.653, Q = 655, T = 37 MIN.

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POST-TEST PHOTOGRAPHS FIGURE 3.J

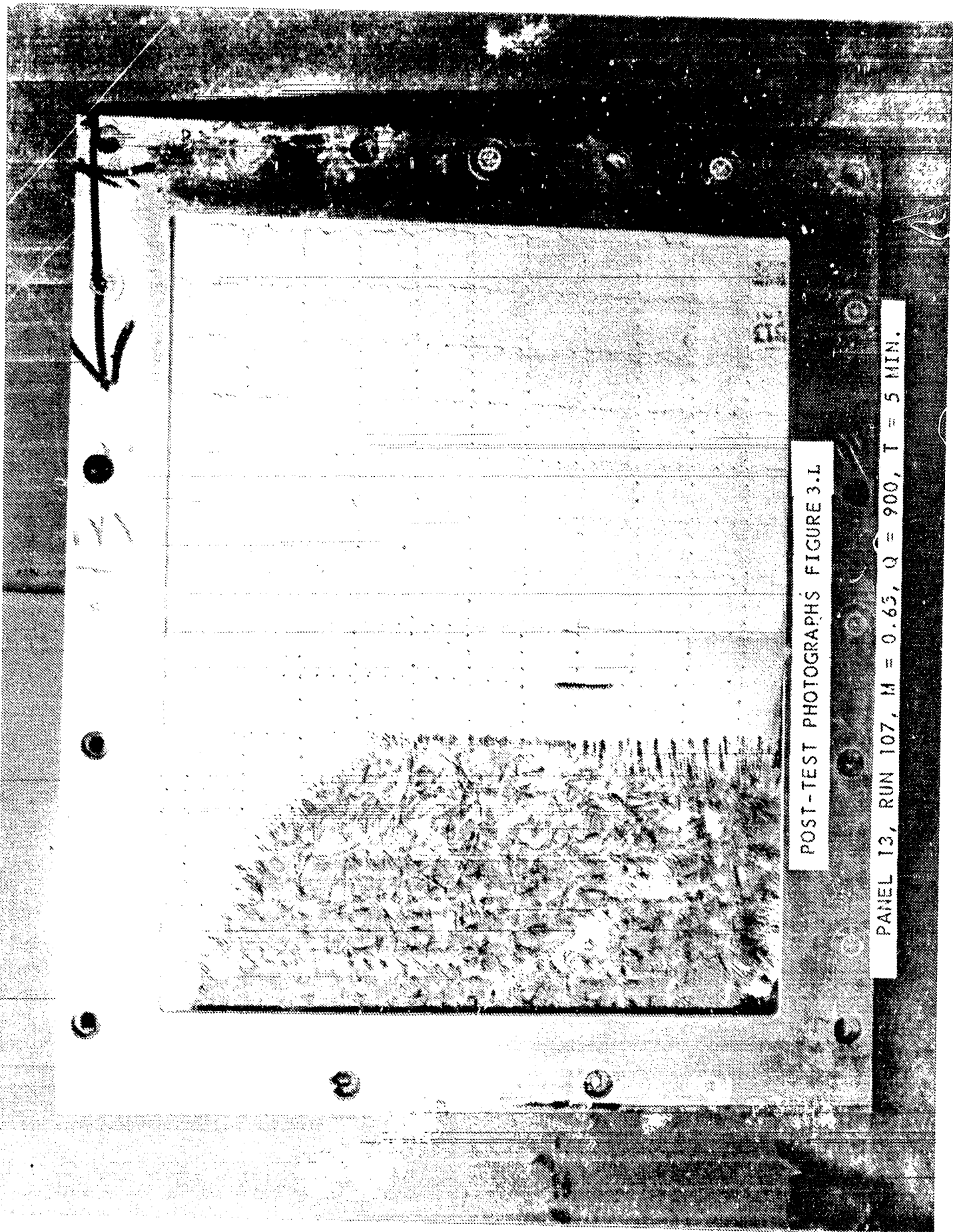
PANEL 11, RUN 104, $M = 0.652$, $Q = 902$, $T = 2$ MIN.

12



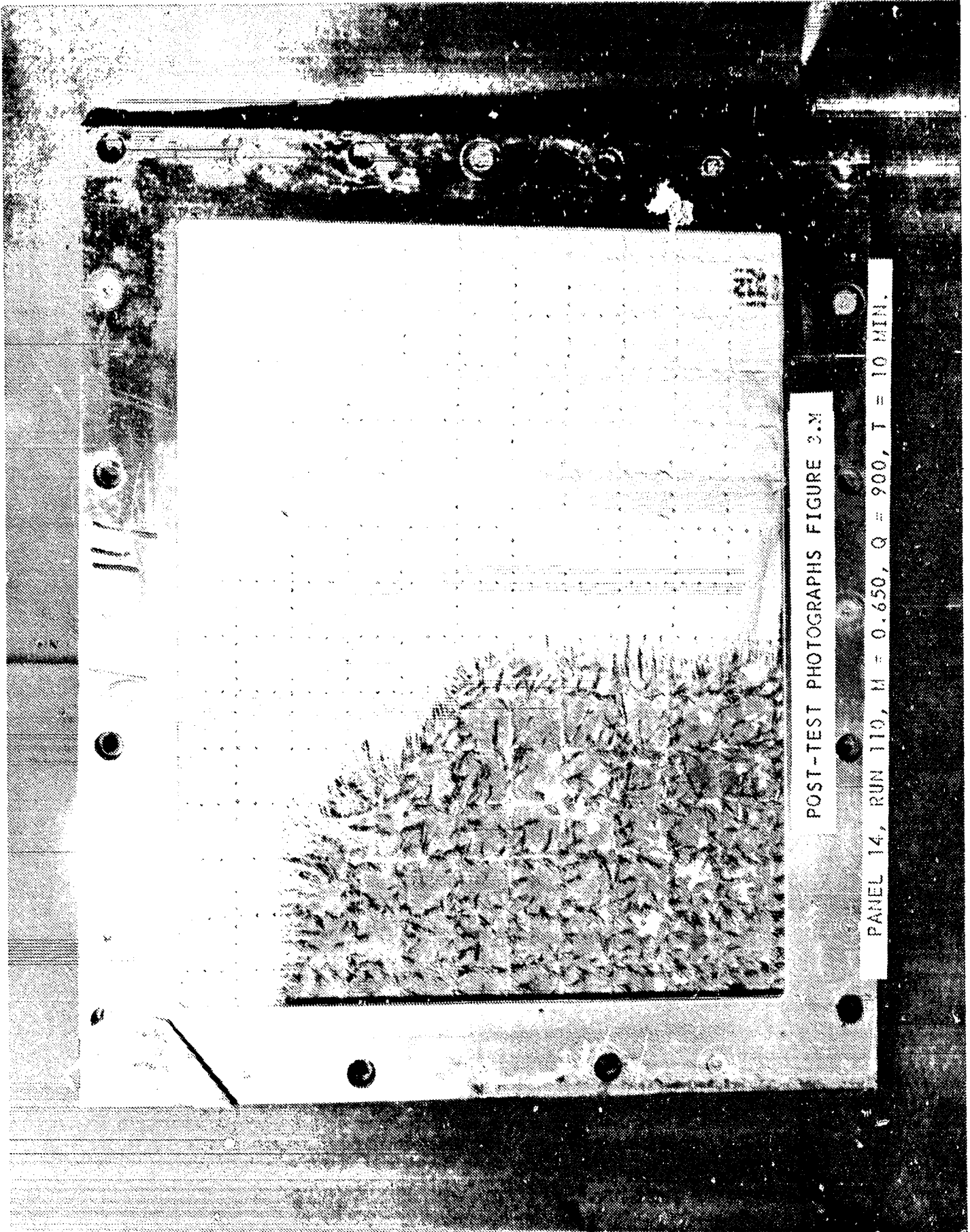
POST-TEST PHOTOGRAPHS FIGURE 3.K

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POST-TEST PHOTOGRAPHS FIGURE 3.1

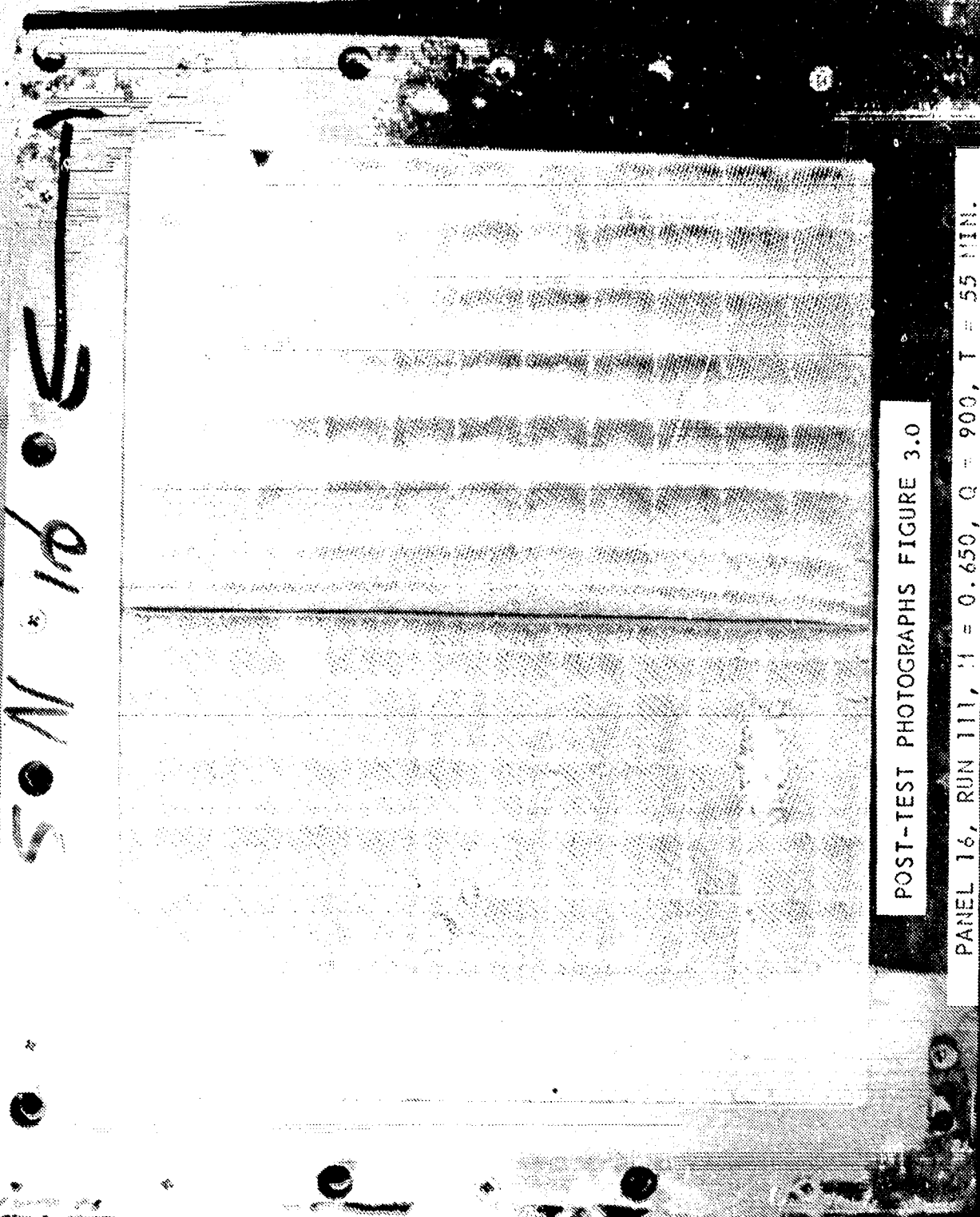
PANEL 13, RUN 107, $M = 0.65$, $Q = 900$, $T = 5$ MIN.



15

POST-TEST PHOTOGRAPHS FIGURE 3.N

PANEL 15, RUN 113, $N = 0.654$, $Q = 902$, $T = 21.5$ MIN.



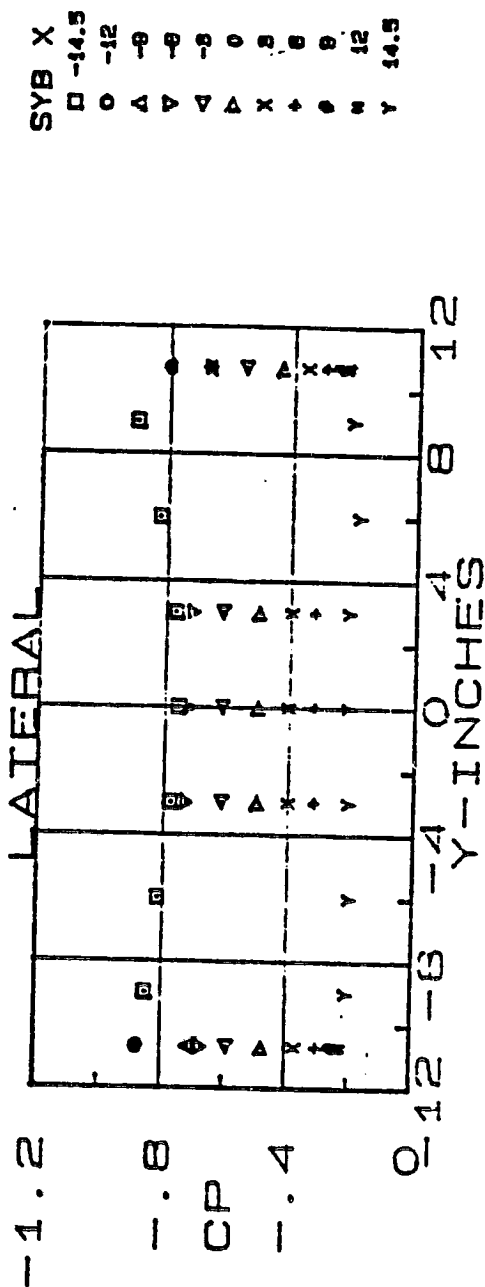
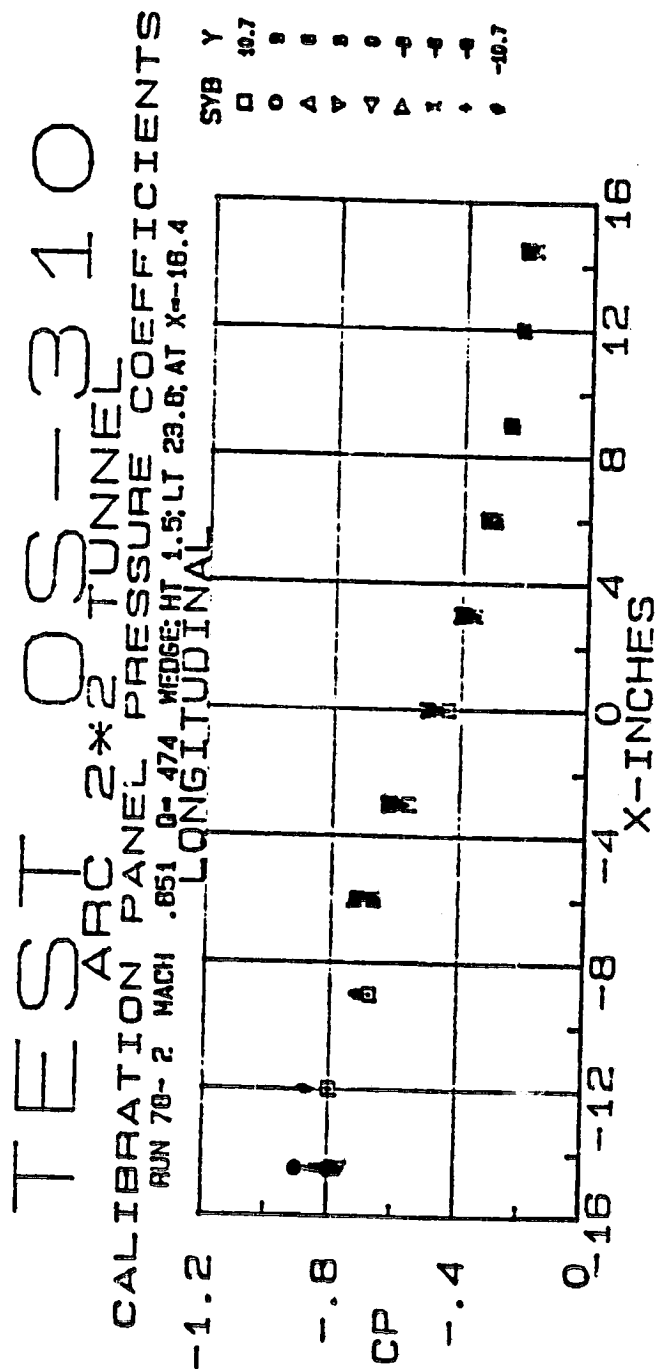


FIGURE 4.A

TEST ARC 2*2 TUNNEL CALIBRATION PANEL PRESSURE COEFFICIENTS RUN 79-1 MACH .653 Q-841 WEDGE HT 1.5; LT 23.0; AT X=-18.4

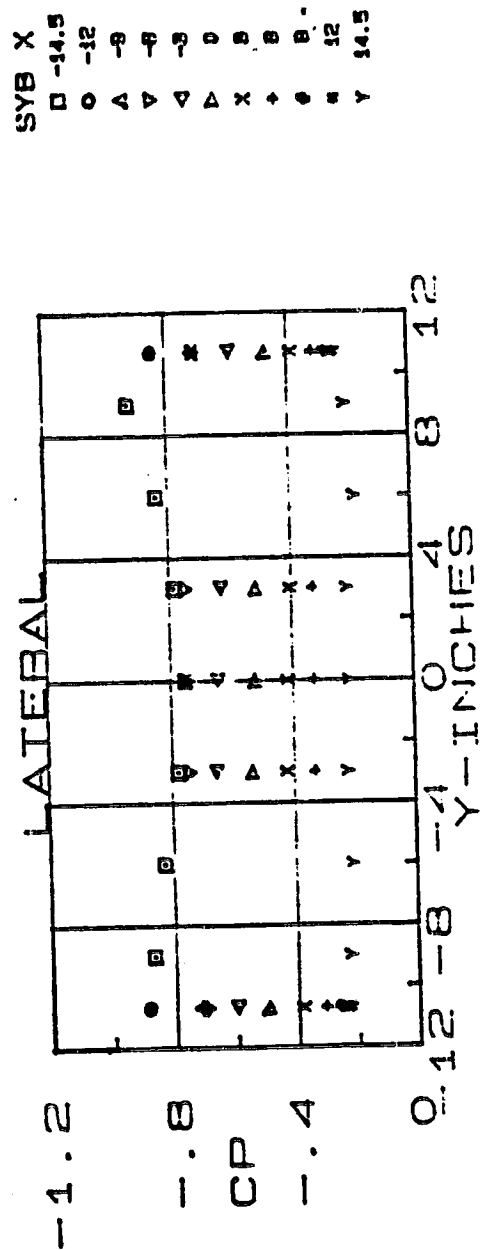
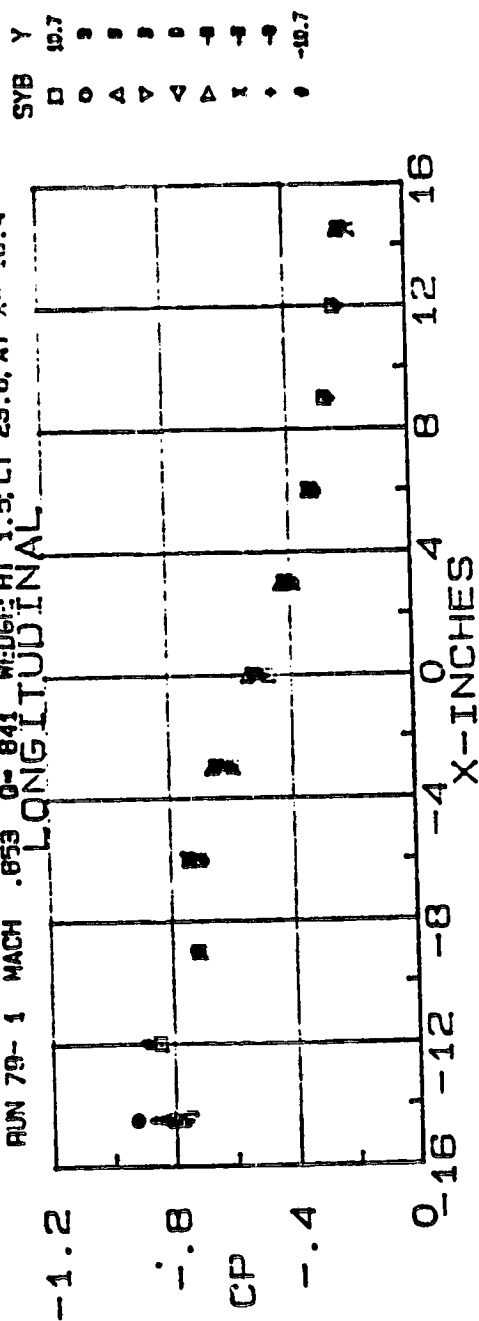


FIGURE 4.B

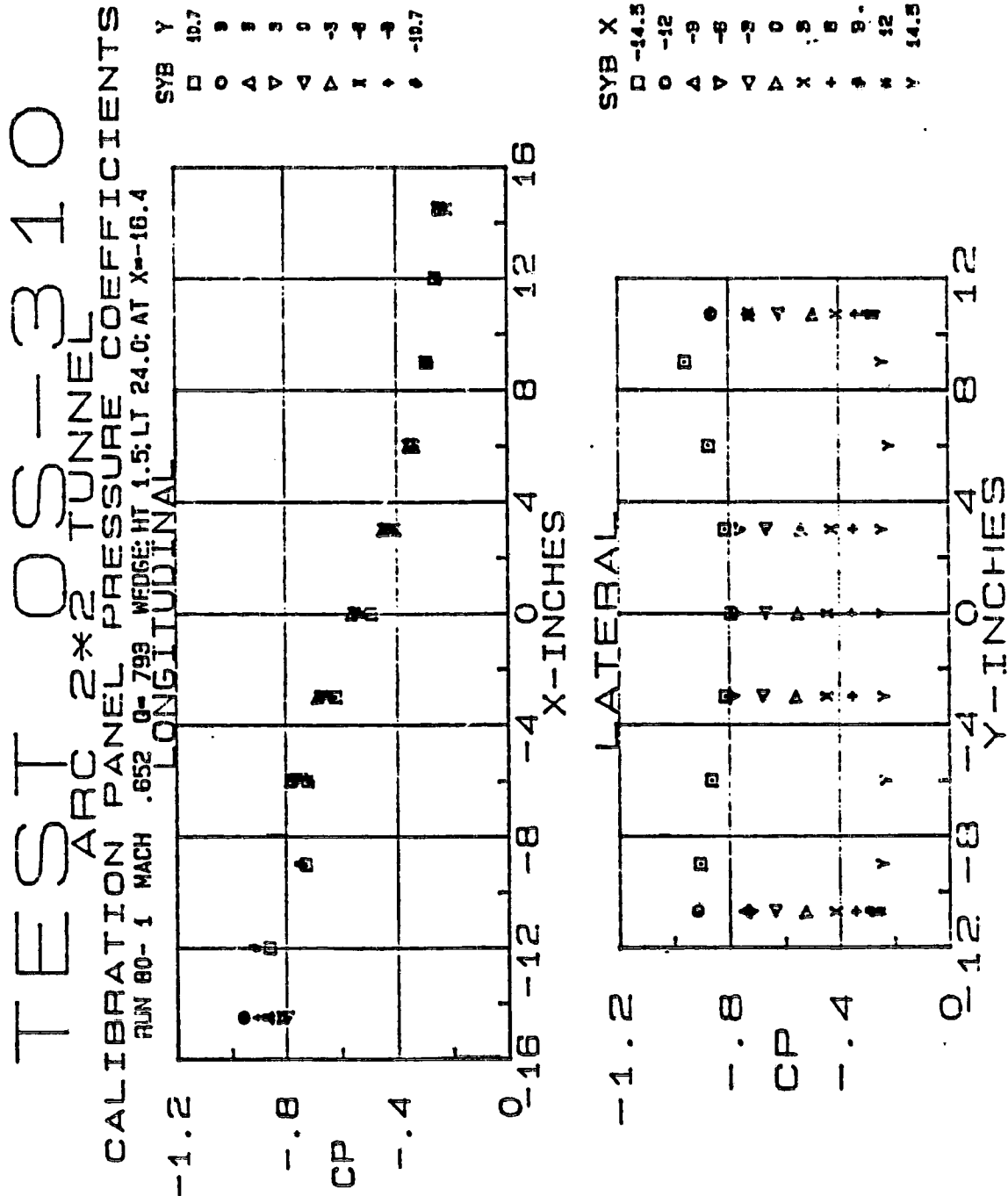


FIGURE 4.C

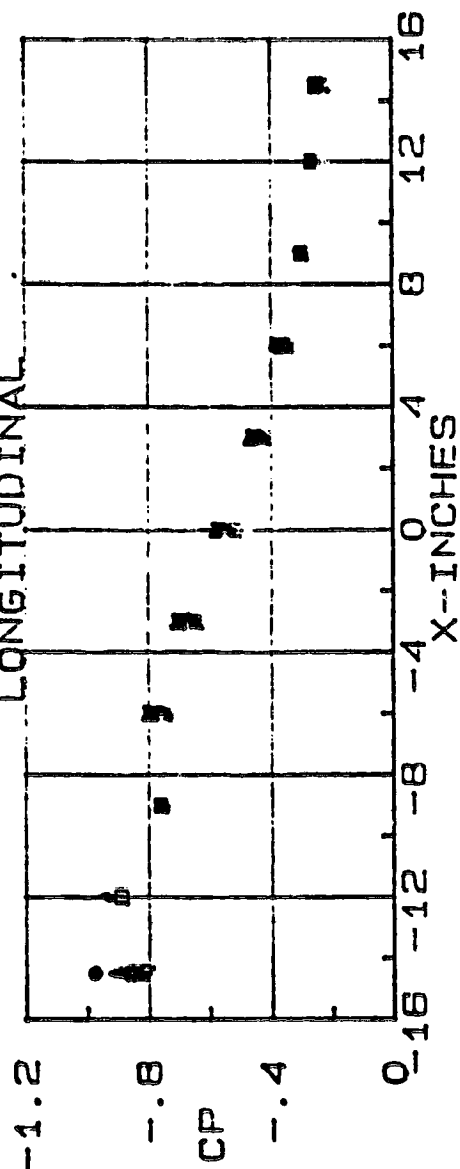
TEST OS-310

ARC 2*2 TUNNEL

CALIBRATION PANEL PRESSURE COEFFICIENTS

RUN 81-1 MACH .651 Q=993 WEPSE: HT 1.5; LI 23.6; AT X=-18.4

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SYB X
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 ○ -100

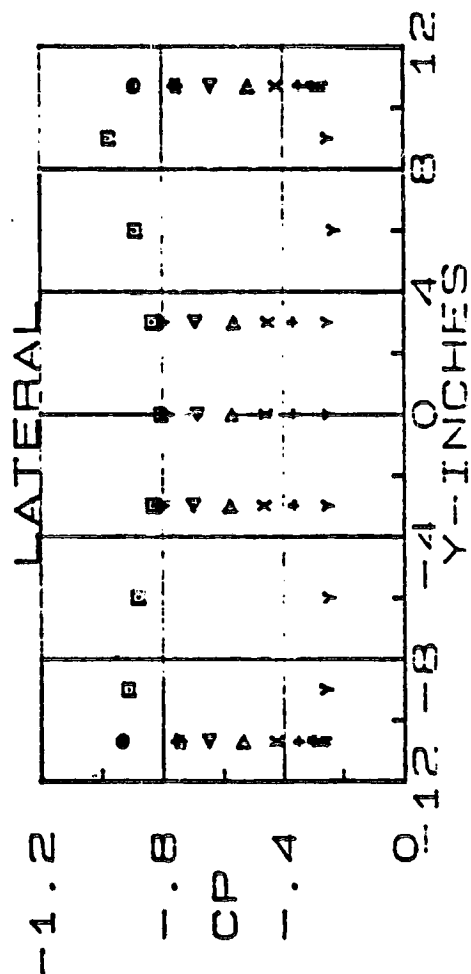


FIGURE 4.D

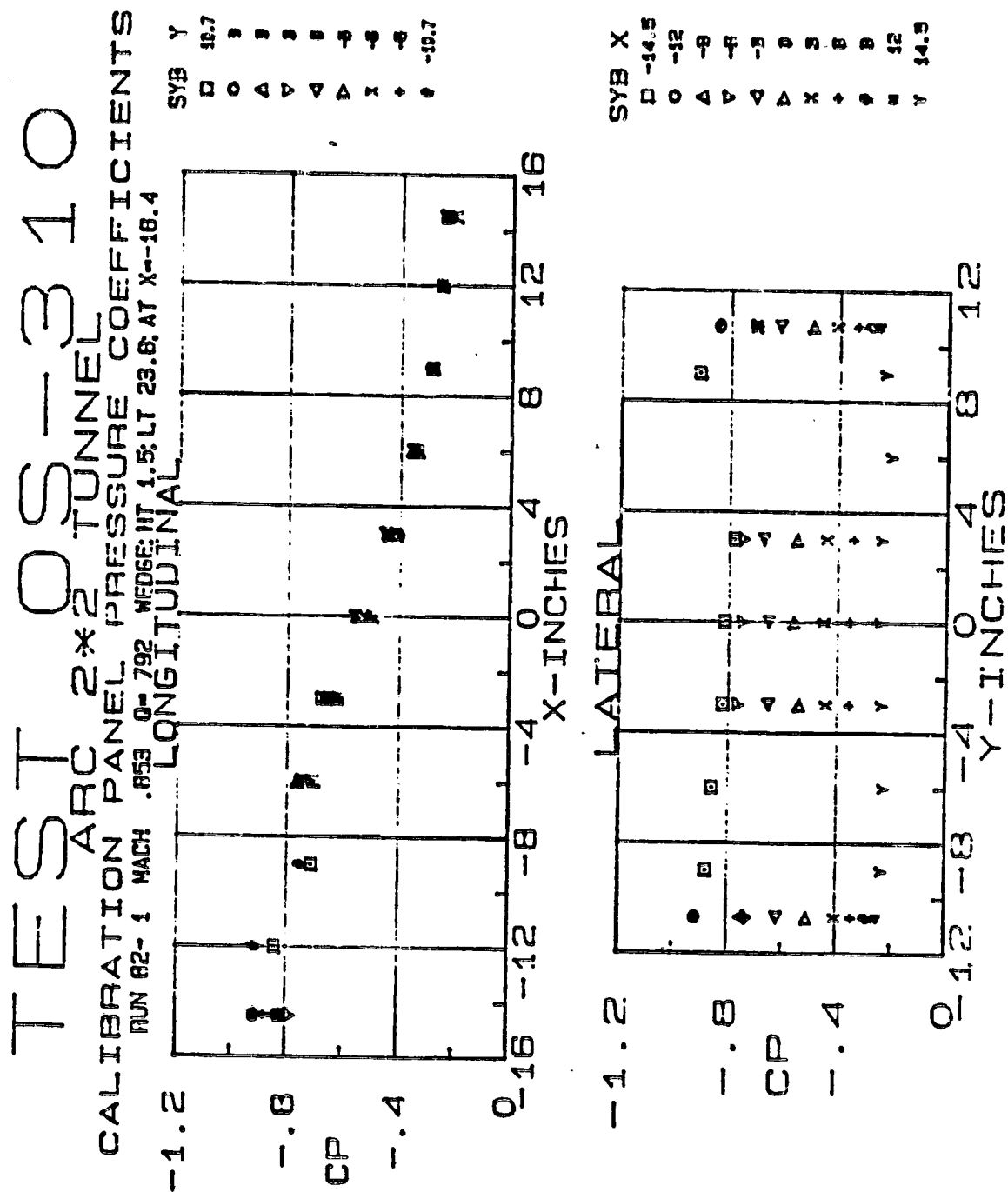


FIGURE 4.E

TEST OS-310

ARC 2x2 TUNNEL

CALIBRATION PANEL PRESSURE COEFFICIENTS

RUN 84-1 MACH .750 Q=578 WEDGE HT 1.0; LT 20.8; AT X=-18.4

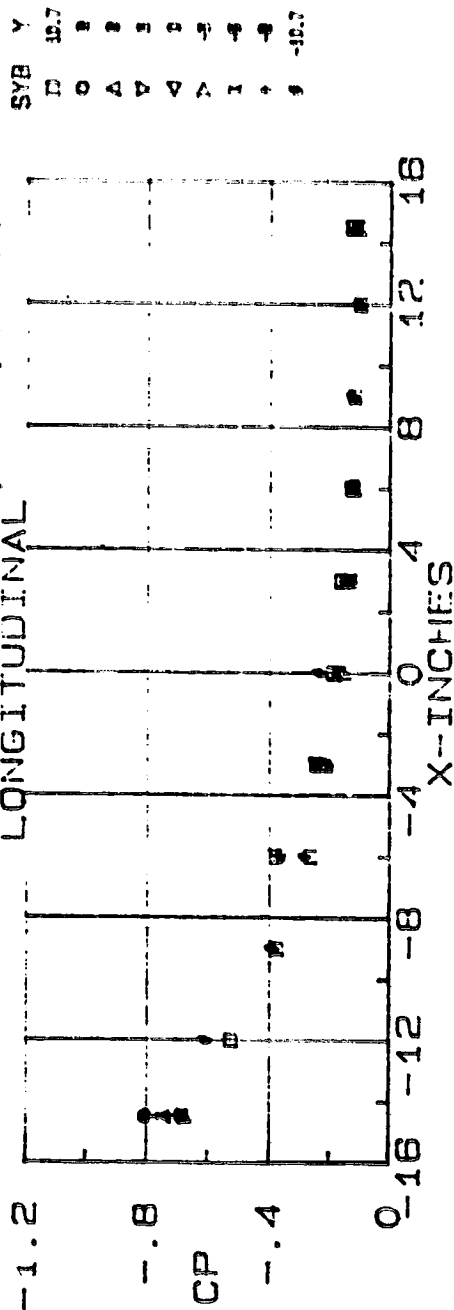
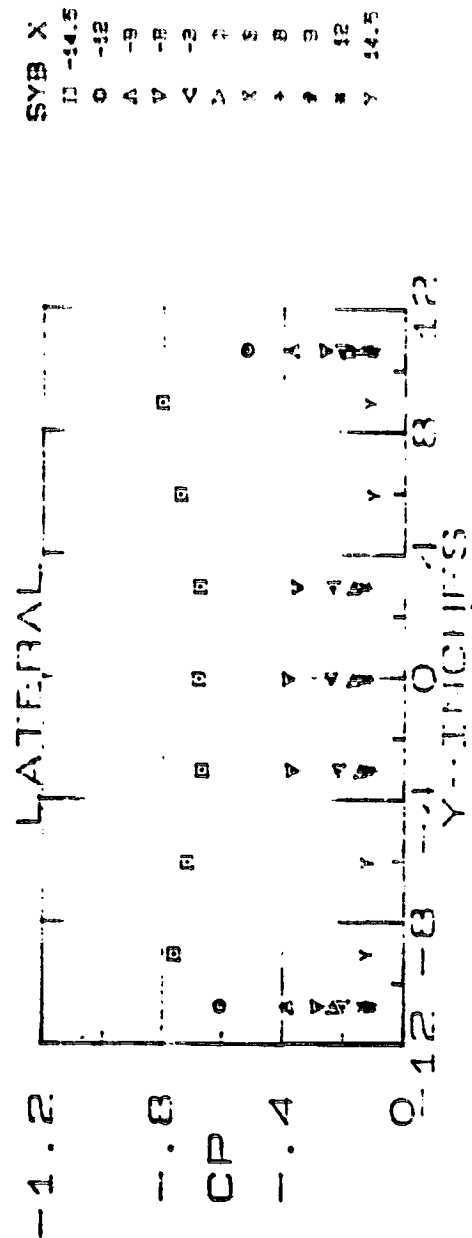


FIGURE 4.F



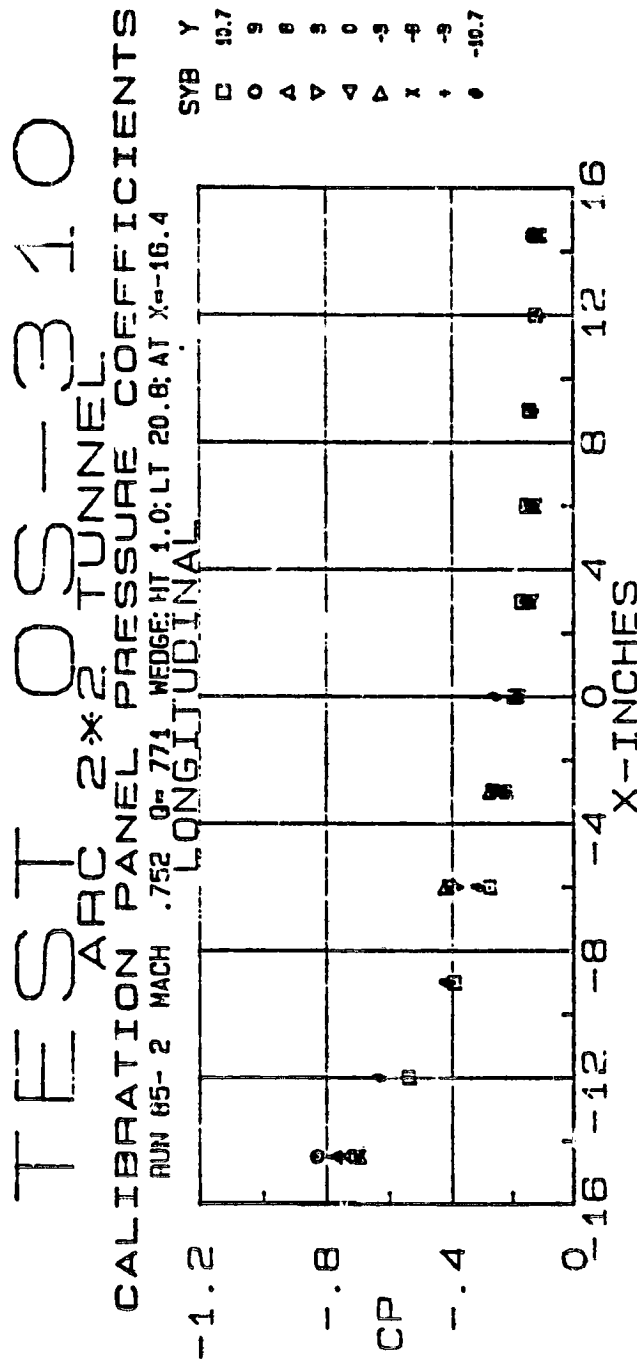
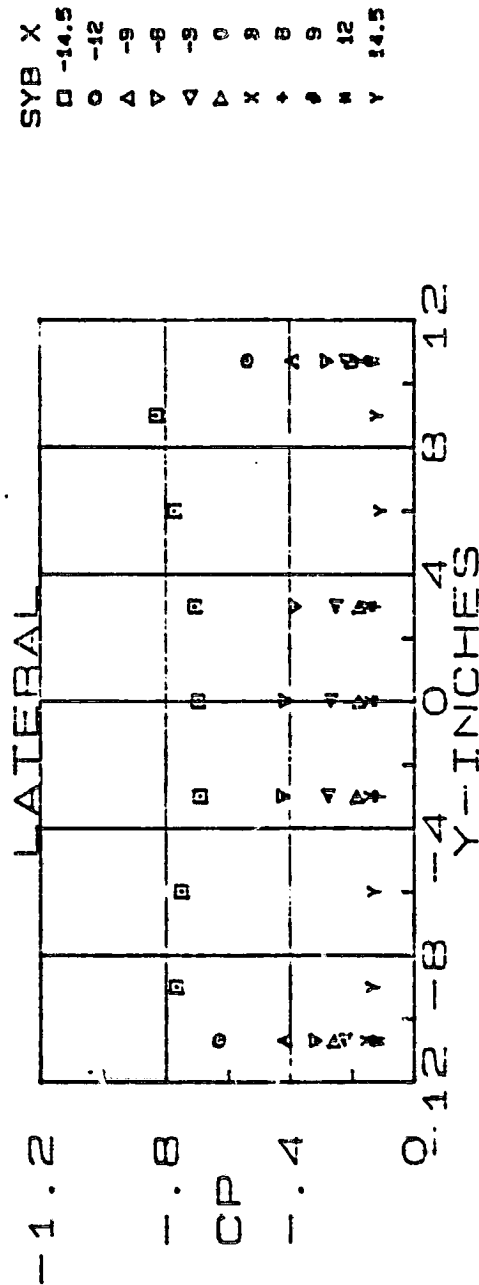


FIGURE 4.6



TEST OS-310

ARC 2*2 TUNNEL

CALIBRATION PANEL PRESSURE COEFFICIENTS
 RUN 86-2 MACH .750 Q=1005 WEDGE HIT 1.0: LT 20.8; AT X=-16.4

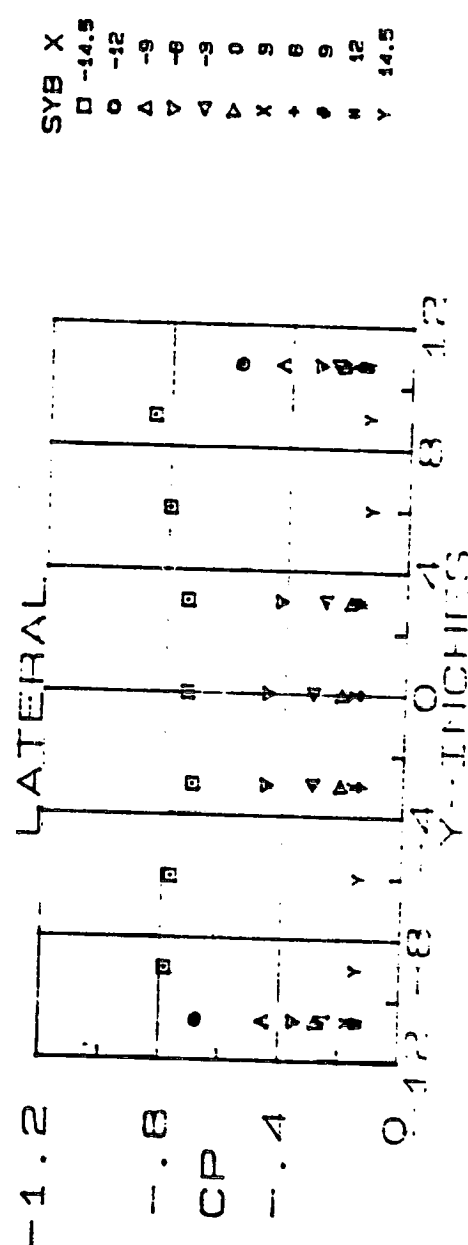
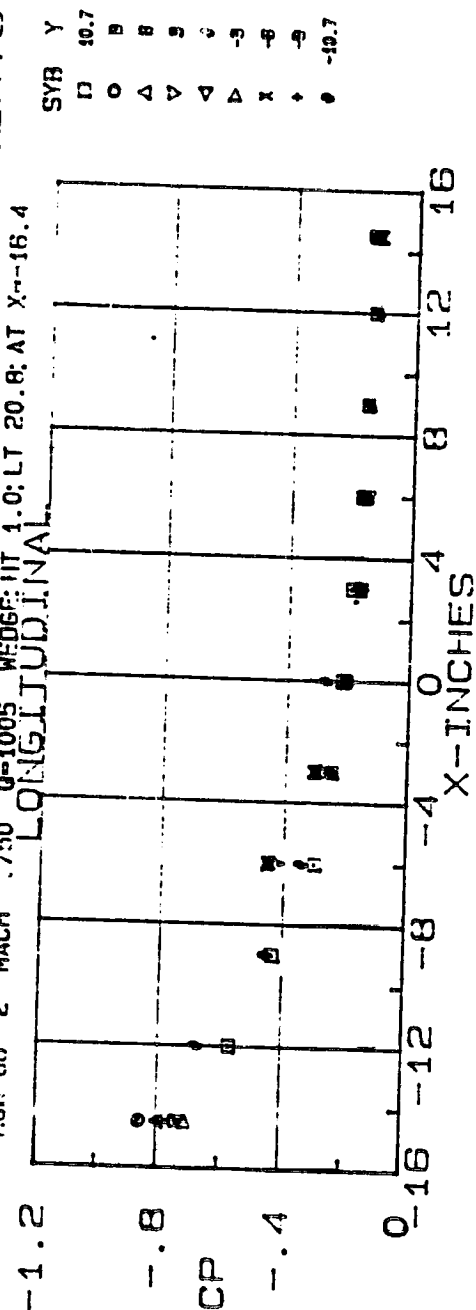


FIGURE 4.H

TEST OS-310

ARC 2*2 TUNNEL
CALIBRATION PANEL PRESSURE COEFFICIENTS
RUN 87-3 MACH .849 Q=860 WEDGE HT .5; LT 20.8; AT X=-16.4
LONGITUDINAL

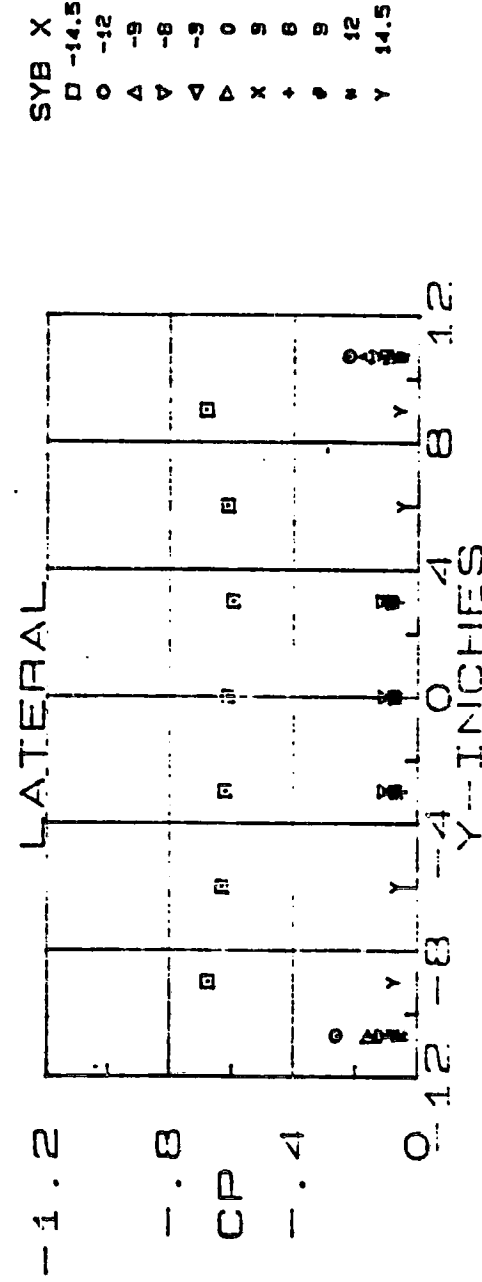
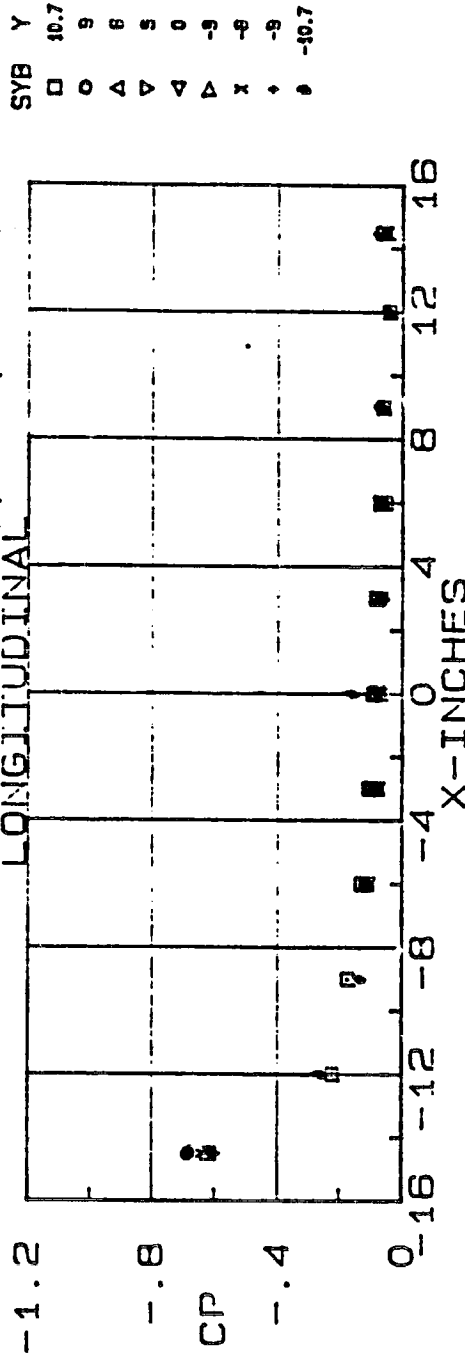


FIGURE 4.1

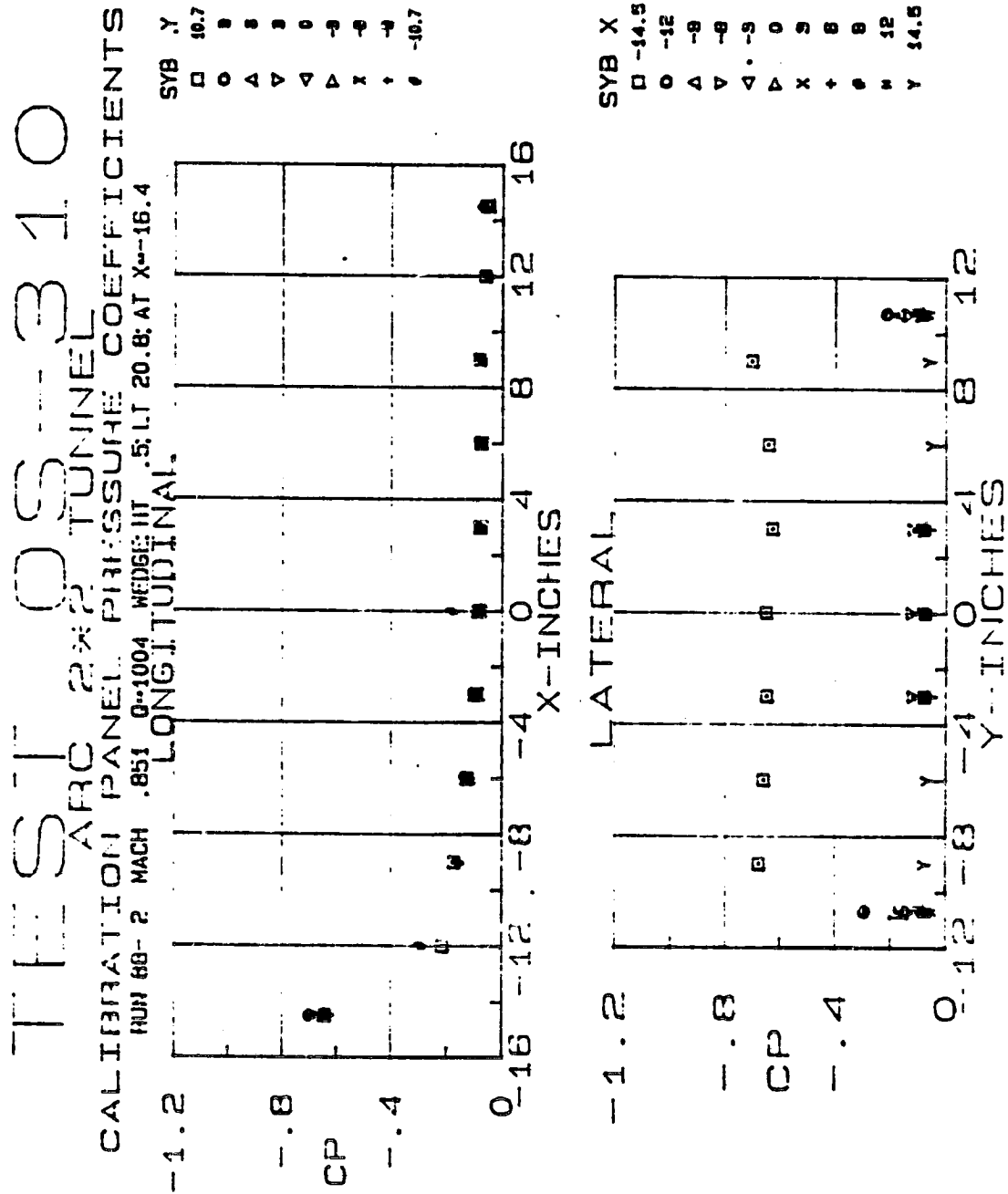


FIGURE 4.J

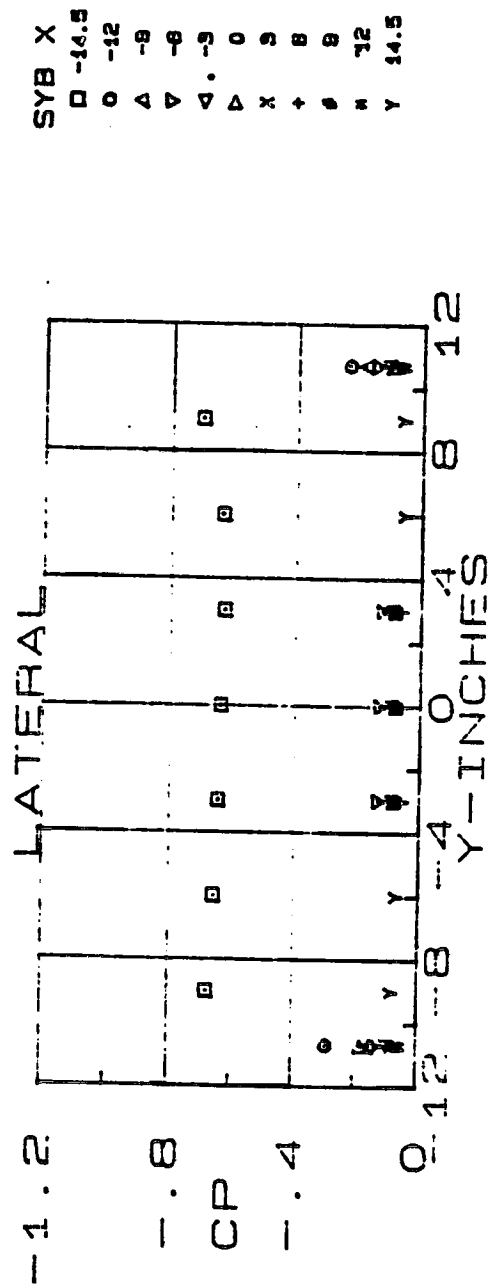
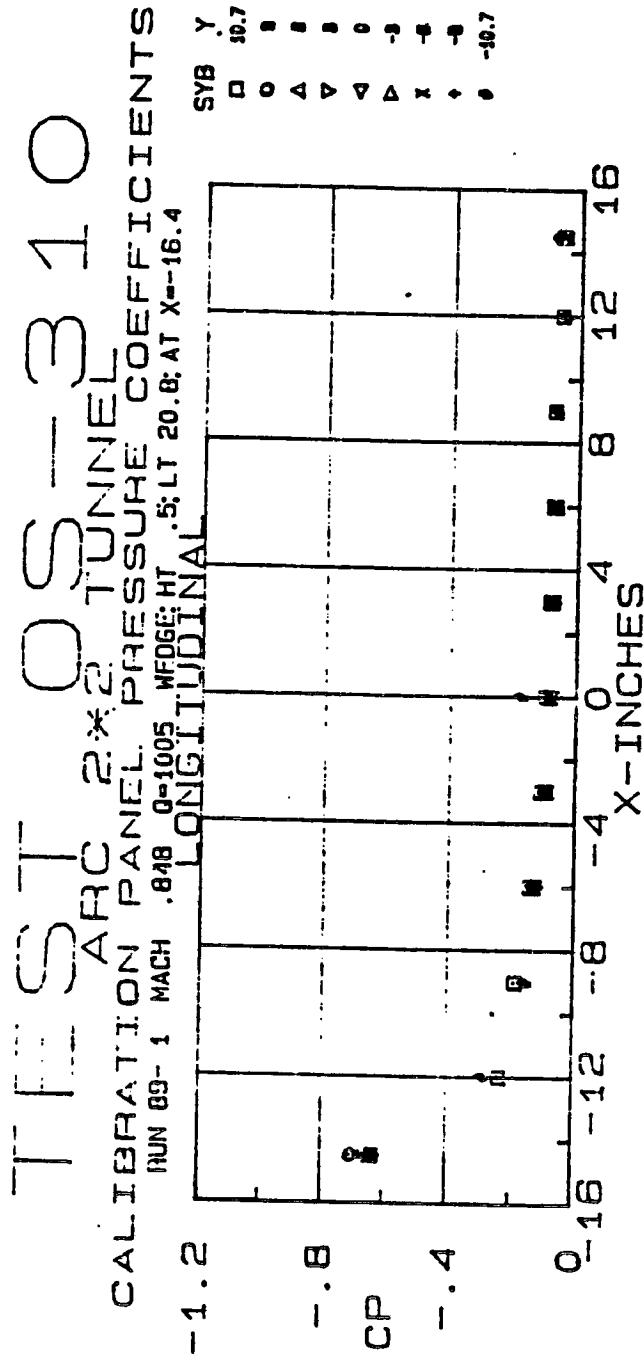


FIGURE 4.K

TEST OS-310 ARC 2-WALL TUNNEL PANEL PRESSURE COEFFICIENTS

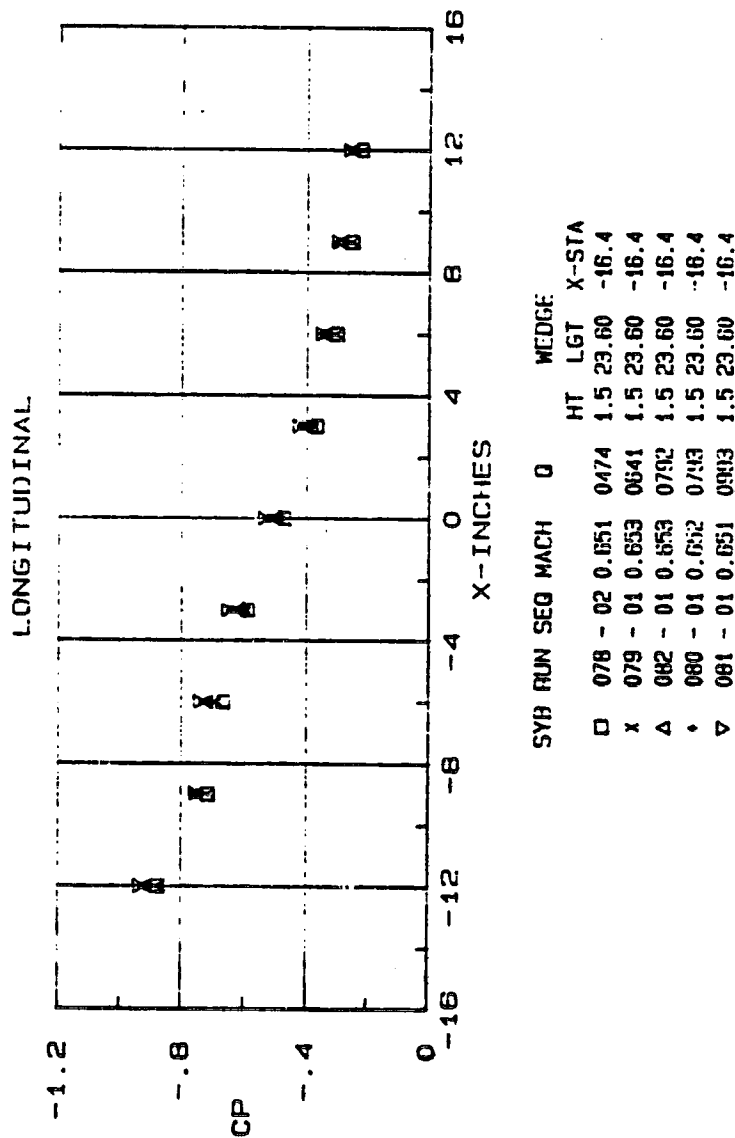


FIGURE 5.A

TEST OS-310 ARC 2x2 TUNNEL PANEL PRESSURE COEFFICIENTS

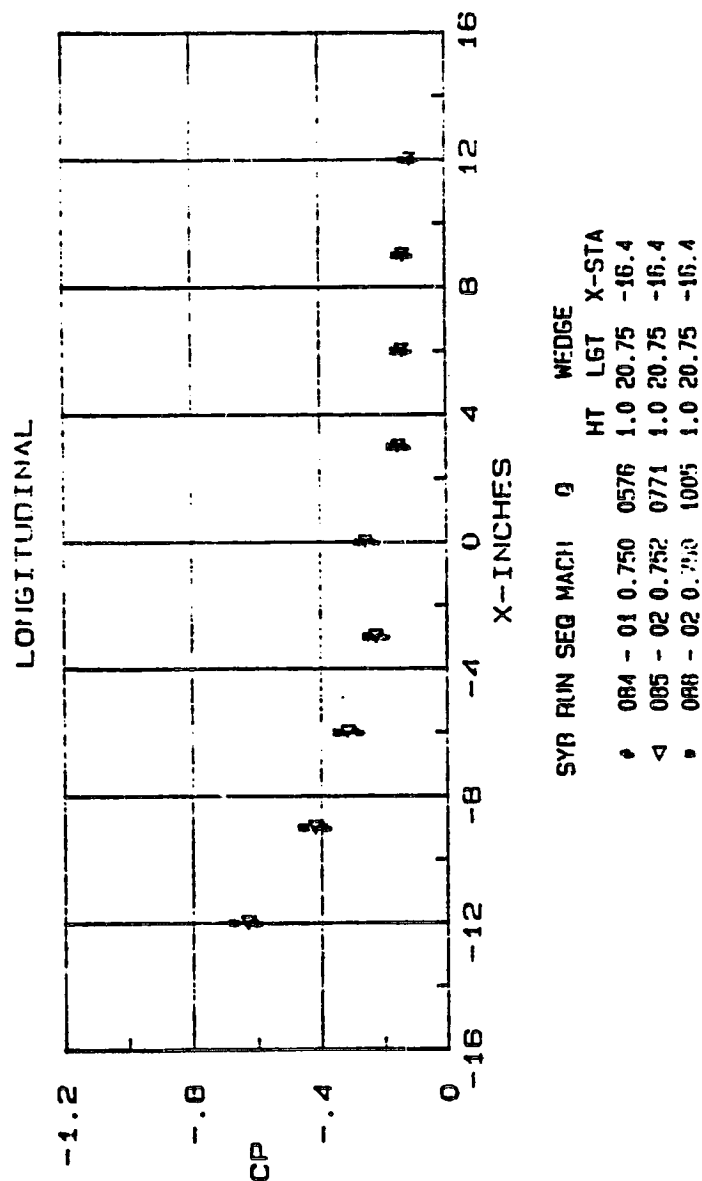
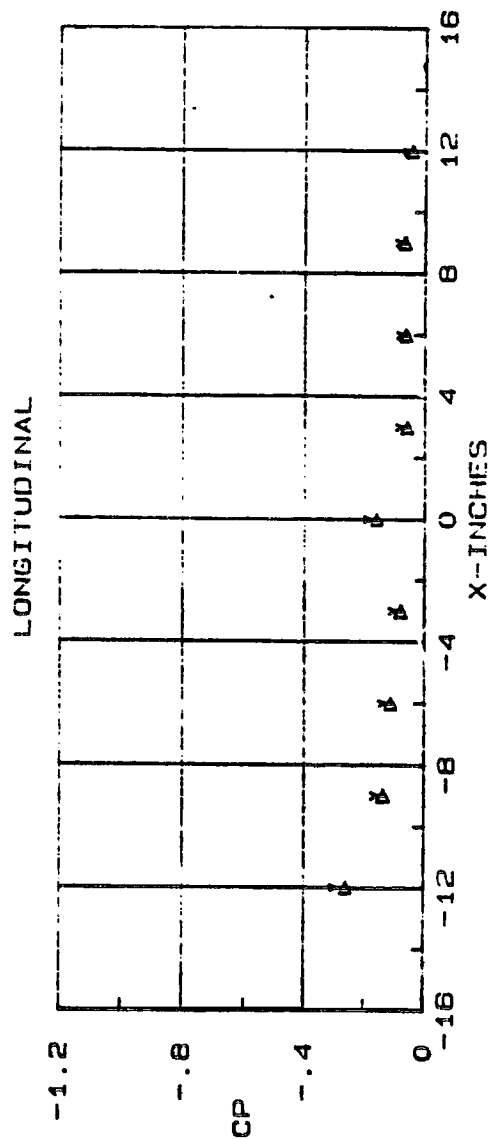


FIGURE 5.B

TEST OS-310

ARC 2x2 TUNNEL
PANEL PRESSURE COEFFICIENTS



SYB RUN	SEQ	MACH	Q	WEDGE	HT	LGT	X-STA
087	- 03	0.849	0568		0.5	20.75	-16.4
088	- 02	0.851	1004		0.5	20.75	-16.4

FIGURE 5.C

TEST OS-310 ARC 2x2 TUNNEL PANEL PRESSURE COEFFICIENTS

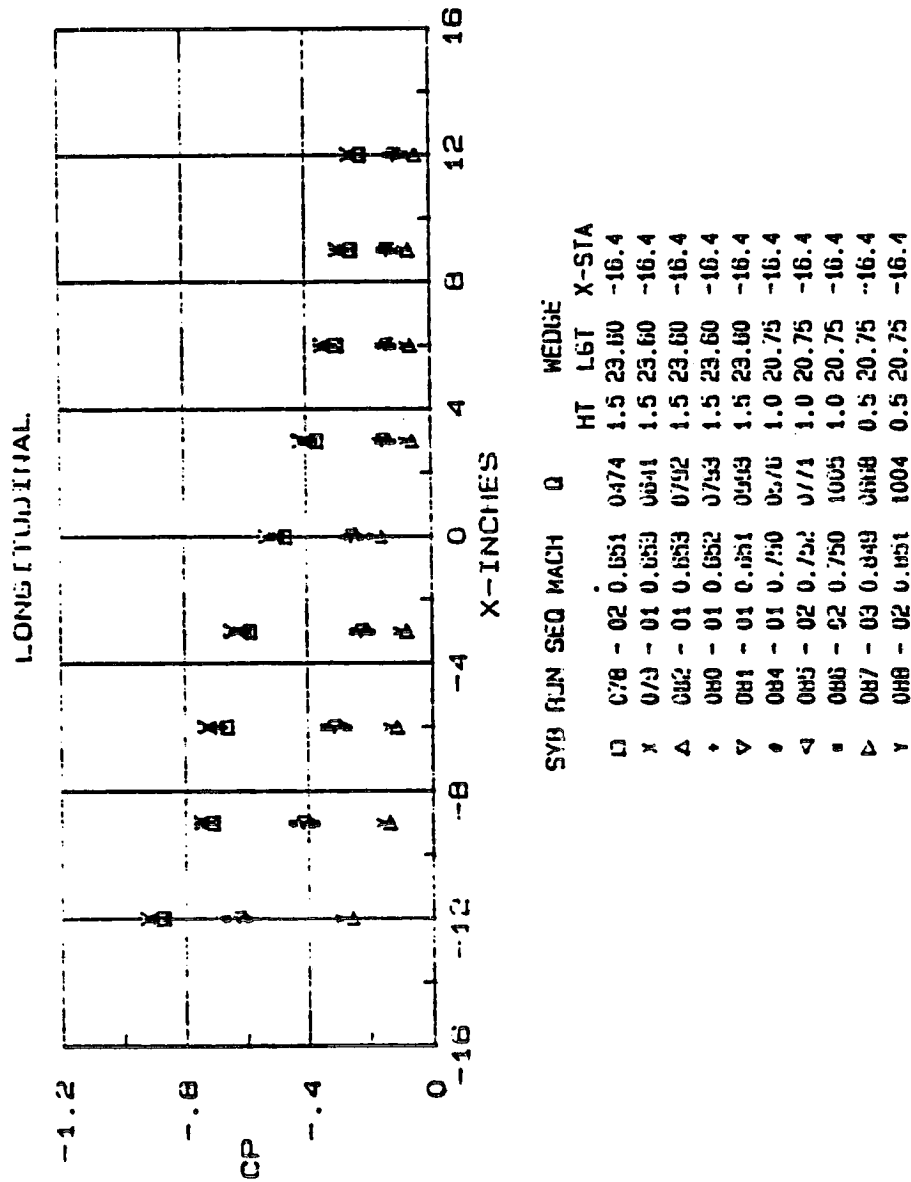


FIGURE 6.A

TEST OS-310 ARC 2x2 TUNNEL PANEL PRESSURE COEFFICIENTS

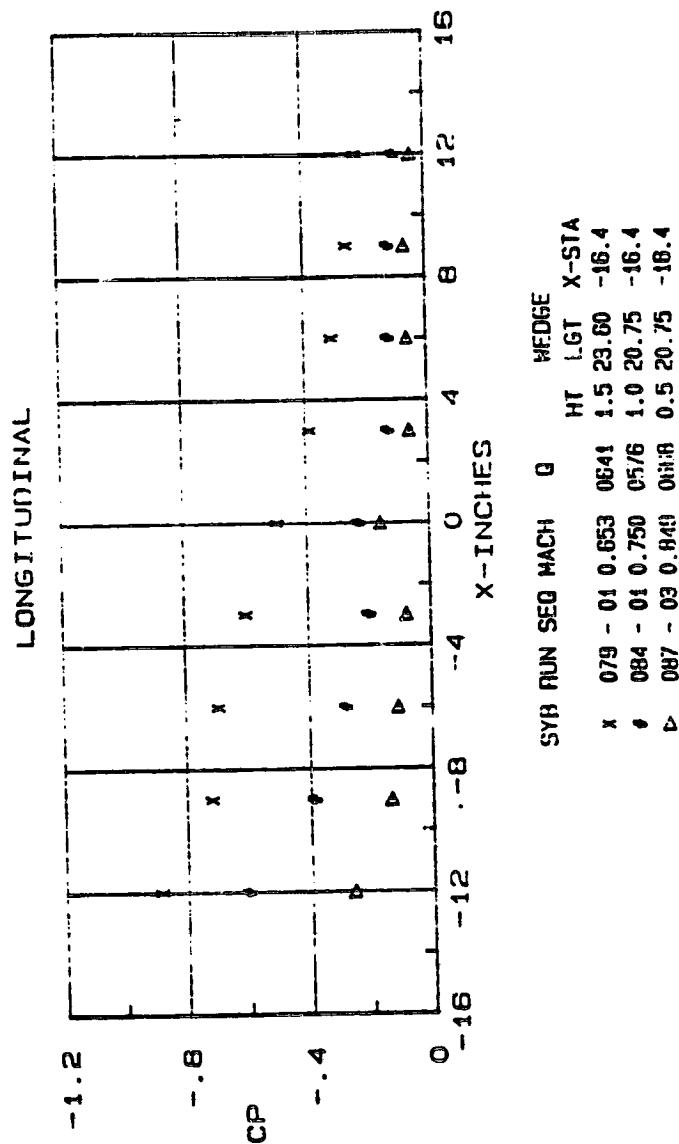


FIGURE 6.B

TEST OS-310 ARC 2x2 TUNNEL PANEL PRESSURE COEFFICIENTS

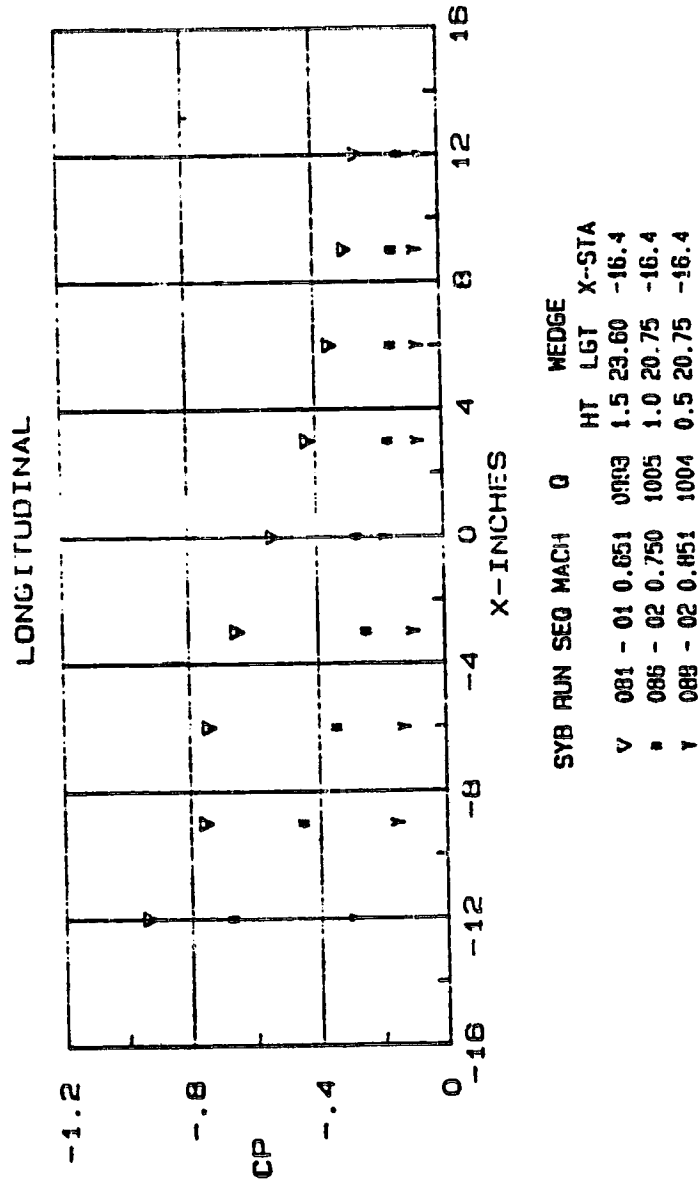
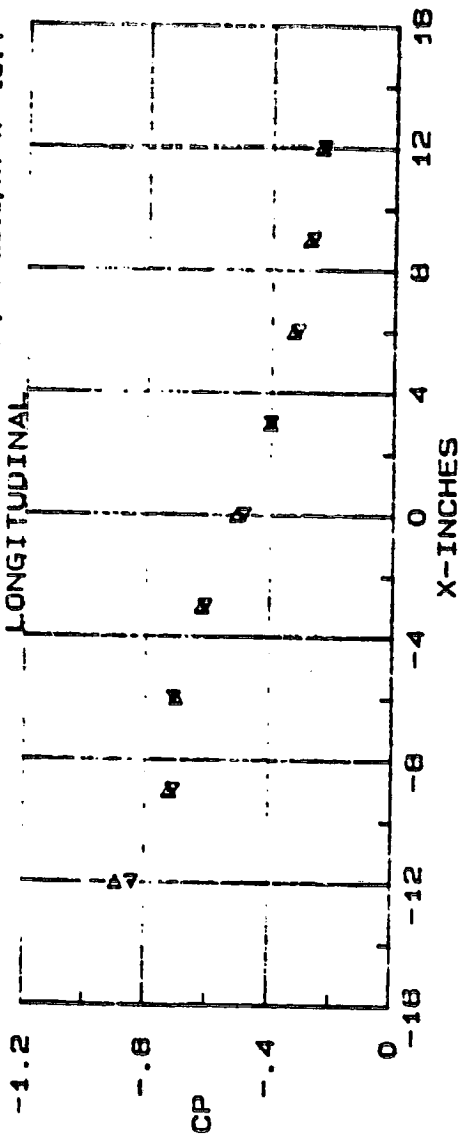


FIGURE 6.C

TEST OS-310

ARC 2*2 TUNNEL
 PANEL PRESSURE COEFFICIENTS
 RUN 100-10 MACH .652 Q= 654 WEDGE: WT 1.5; LT 23.6; AT X=-16.4

SYB Y
 < 30.7
 > -30.7



SYB X
 Δ -34.5
 ▽ 34.5

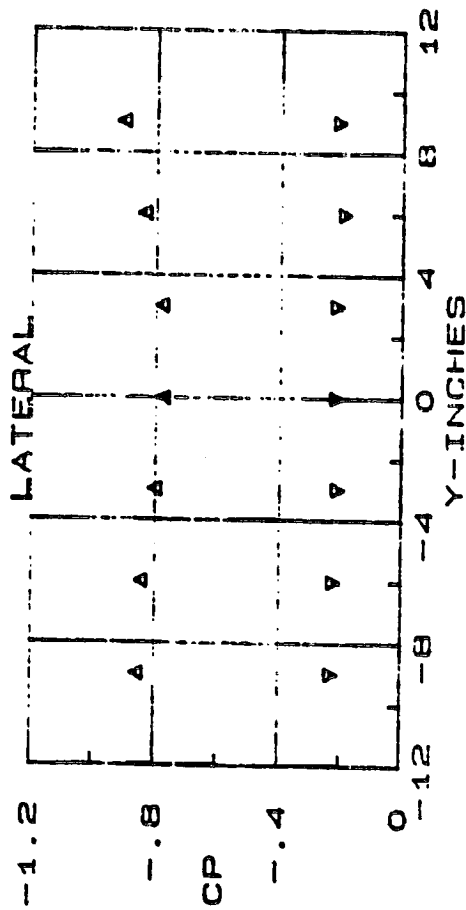
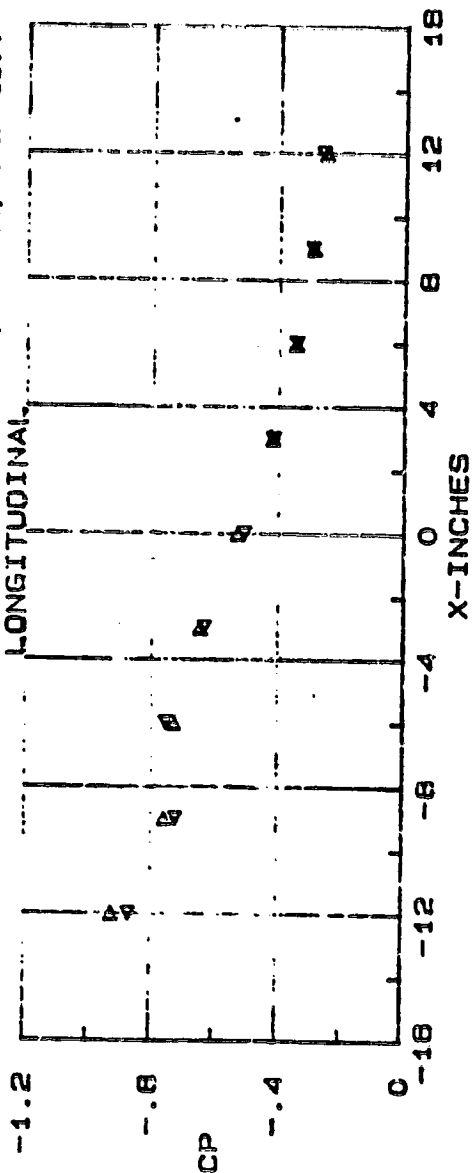


FIGURE 7.A

TEST OS-310

ARC 2*2 TUNNEL
PANEL PRESSURE COEFFICIENTS
RUN 102-18 MACH .650 Q= 902 WEDGE: HT 1.5: LT 23.0: AT X=-16.4



SYB X
△ -14.5
▽ 14.5

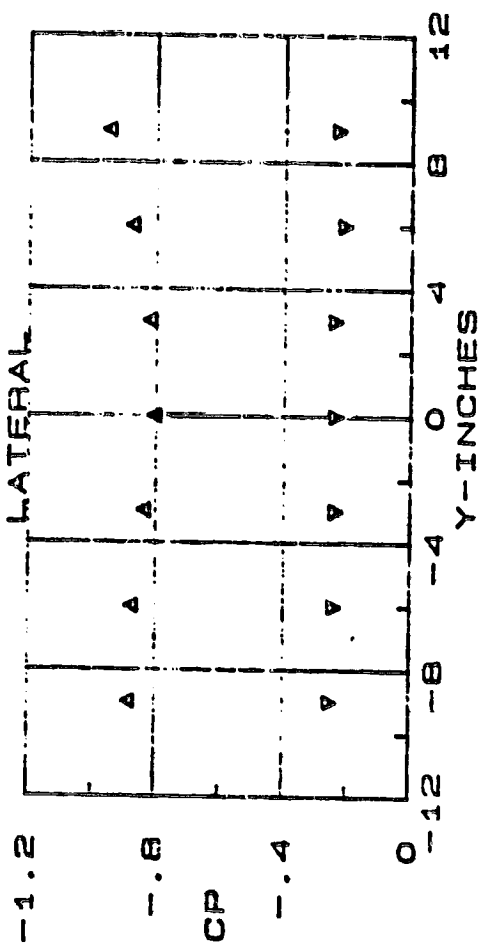
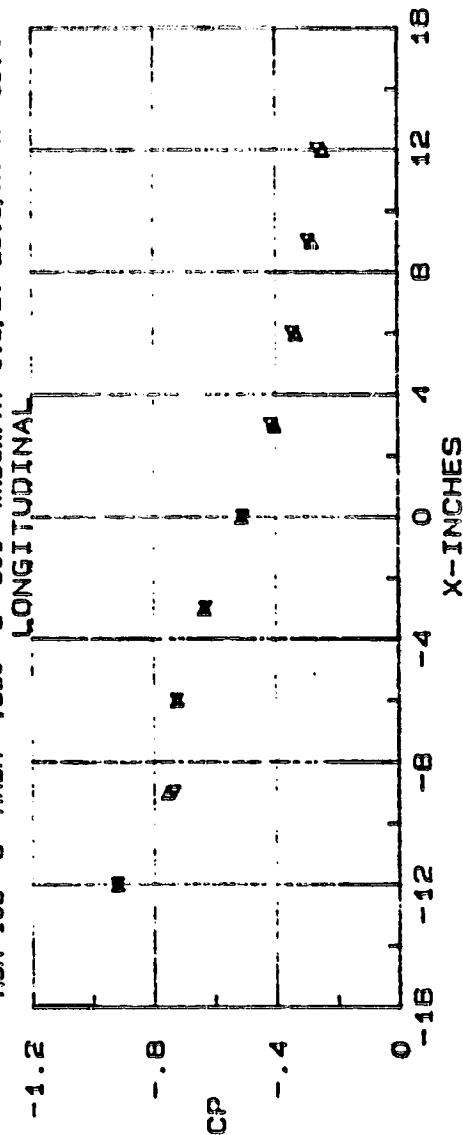


FIGURE 7.5

TEST OS-310

ARC 2*2 TUNNEL
PANEL PRESSURE COEFFICIENTS
RUN 103-6 MACH .650 Q-901 WEDGE: HT 1.5; LI 23.6; AT X=-16.4

SYB Y
△ 19.7
▽ -19.7



SYB X
△ -14.5
▽ 14.5

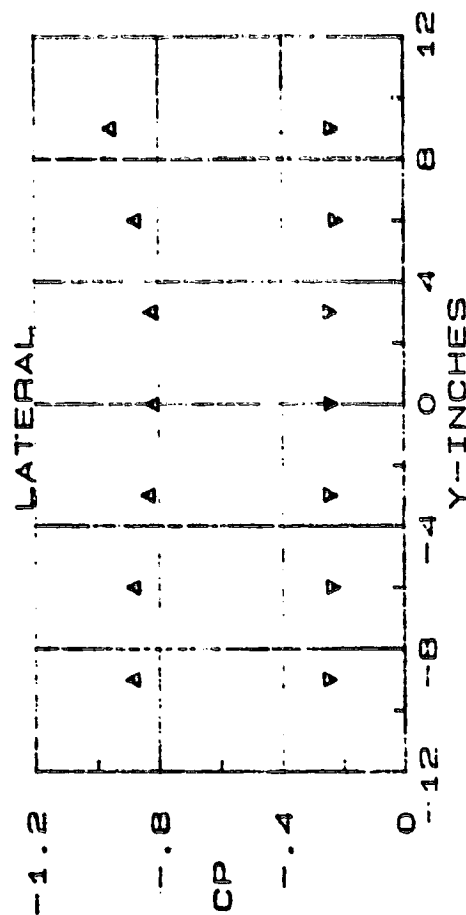


FIGURE 7.C

TEST OS-310

ARC 2x2 TUNNEL
 PANEL PRESSURE COEFFICIENTS
 RUN 104-5 MACH .653 Q= 905 WEDGE: HT 1.5; LT 23.8; AT X=-16.4

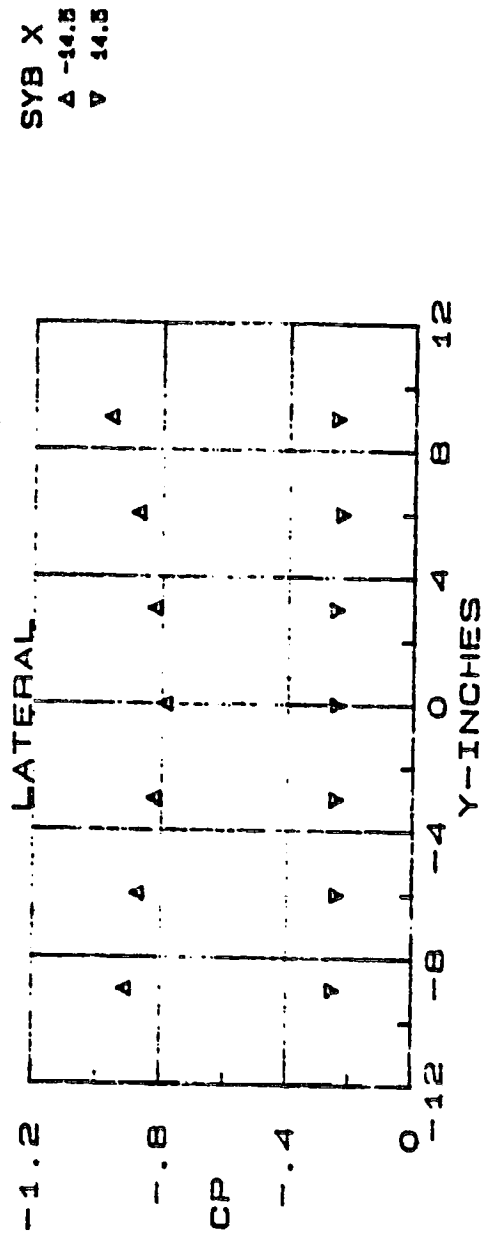
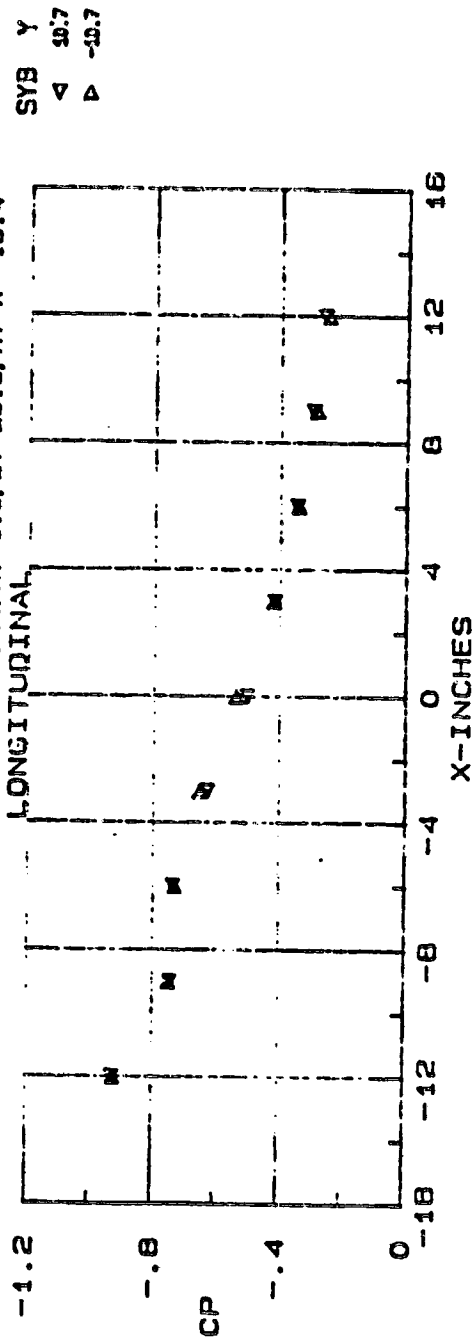


FIGURE 7.D

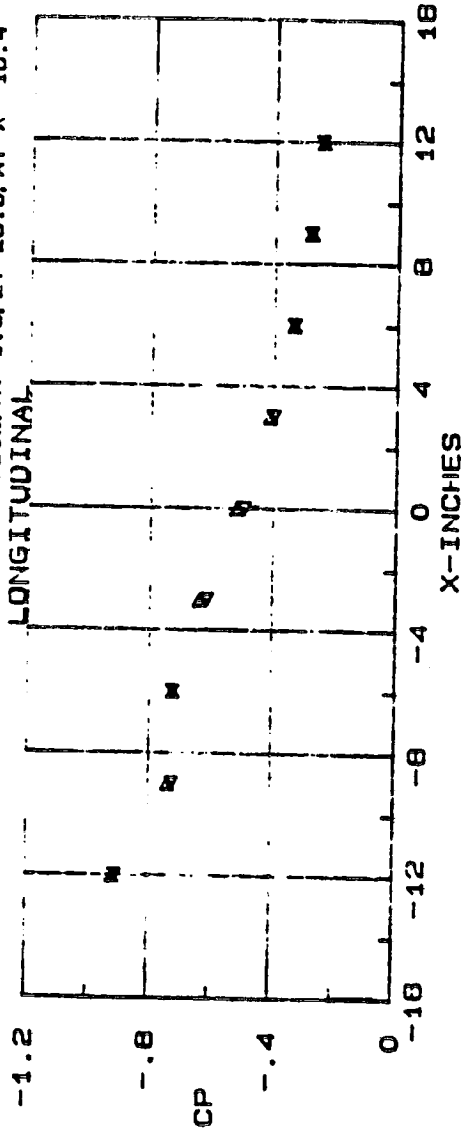
TEST OS-310

ARC 2*2 TUNNEL

PANEL PRESSURE COEFFICIENTS

RUN 105-1 MACH .651 Q= 902 WFUDGE: HT 1.5; LT 23.6; AT X=-16.4

SYB Y
 < 10.7
 > -10.7



SYB X
 < -14.8
 > 14.5

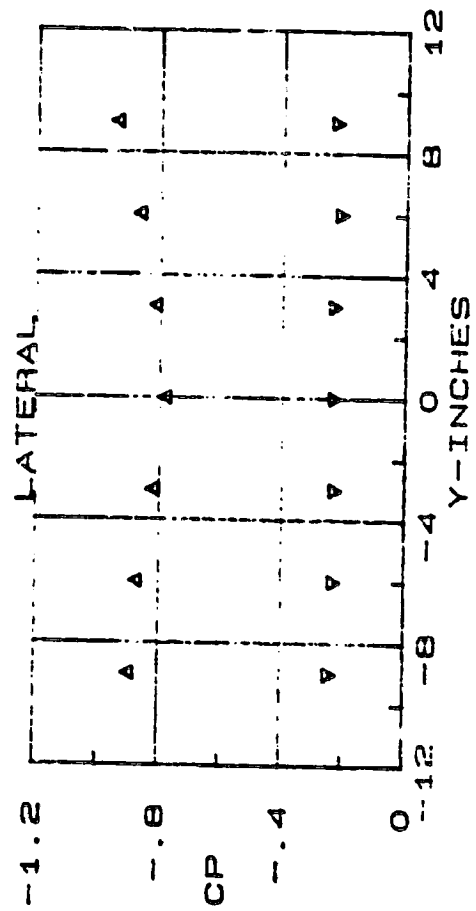
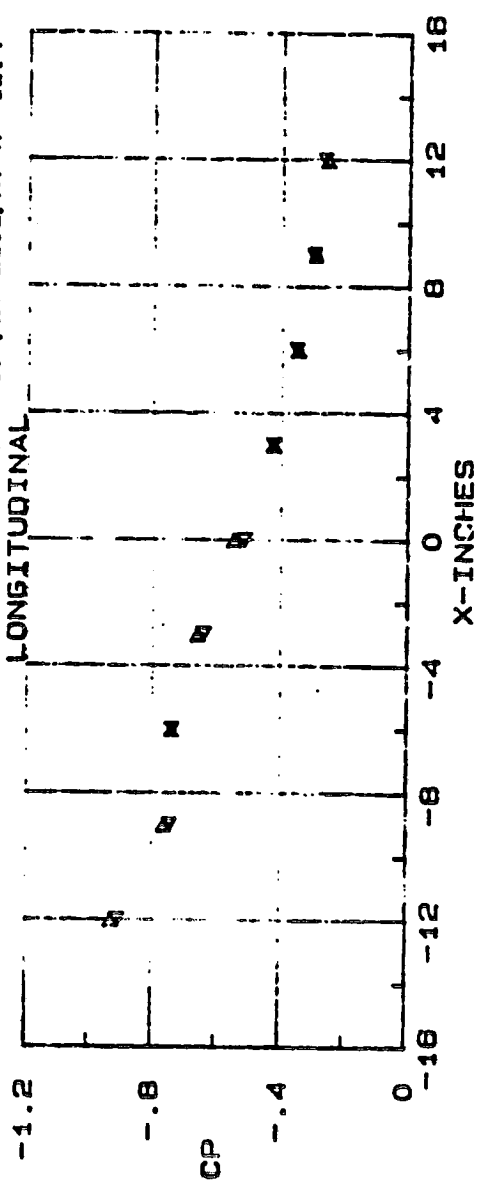


FIGURE 7.E

TEST OS-310

ARC 2*2 TUNNEL
 PANEL PRESSURE COEFFICIENTS
 RUN 107-1 MACH .652 Q=907 WEDGE: HT 1.5; LT 23.6; AT X=-18.4

SYB Y
 Δ 10.7
 ▽ -10.7



SYB X
 Δ -14.8
 ▽ 14.8

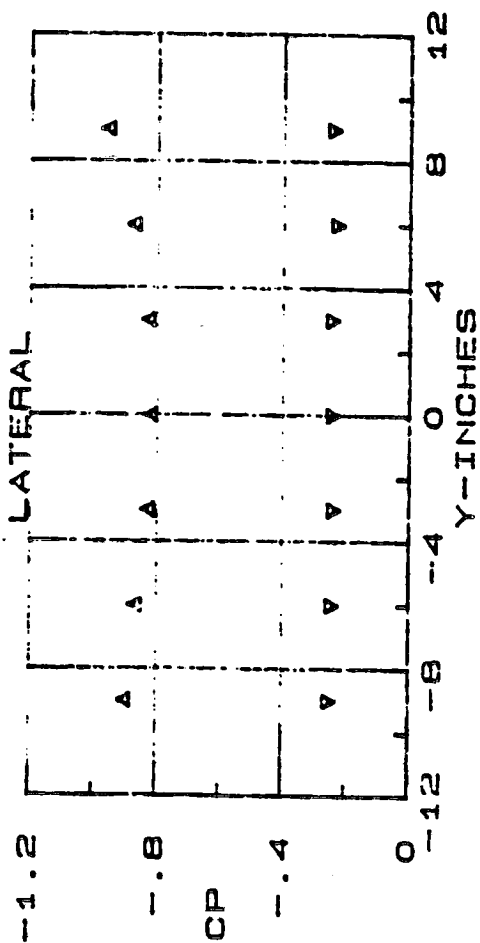


FIGURE 7.F

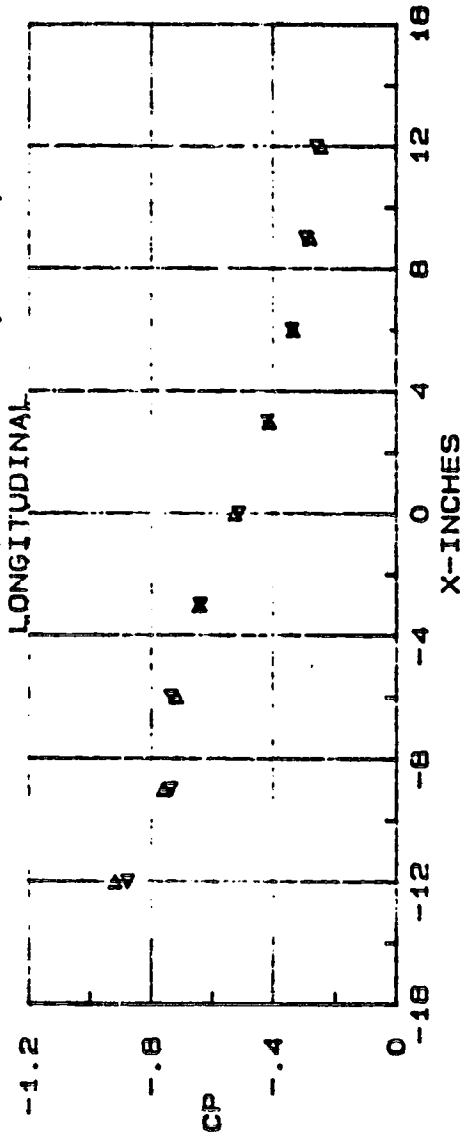
TEST OS-310

ARC 2*2 TUNNEL

PANEL PRESSURE COEFFICIENTS

RUN 108- 4 MACH .654 Q= 900 WEDGE: HT 1.5; LT 23.6; AT X=-18.4

SYB Y
 < 19.7
 > -19.7



SYB X
 Δ -14.8
 ▽ 14.8

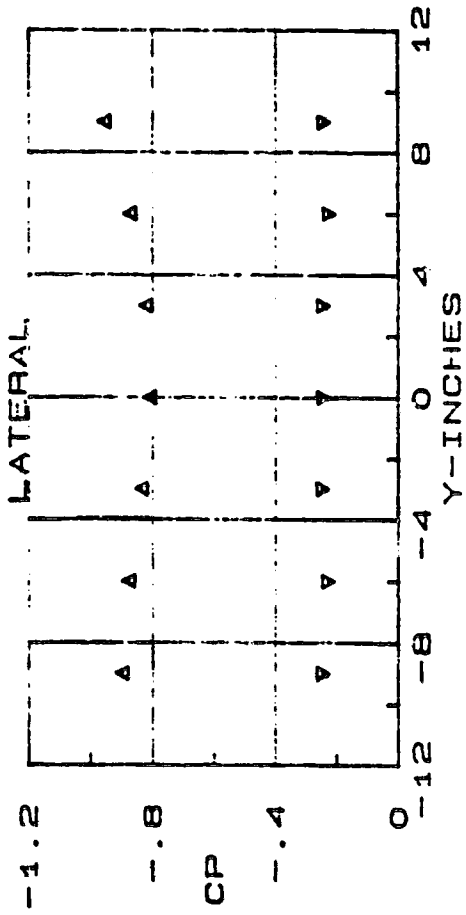
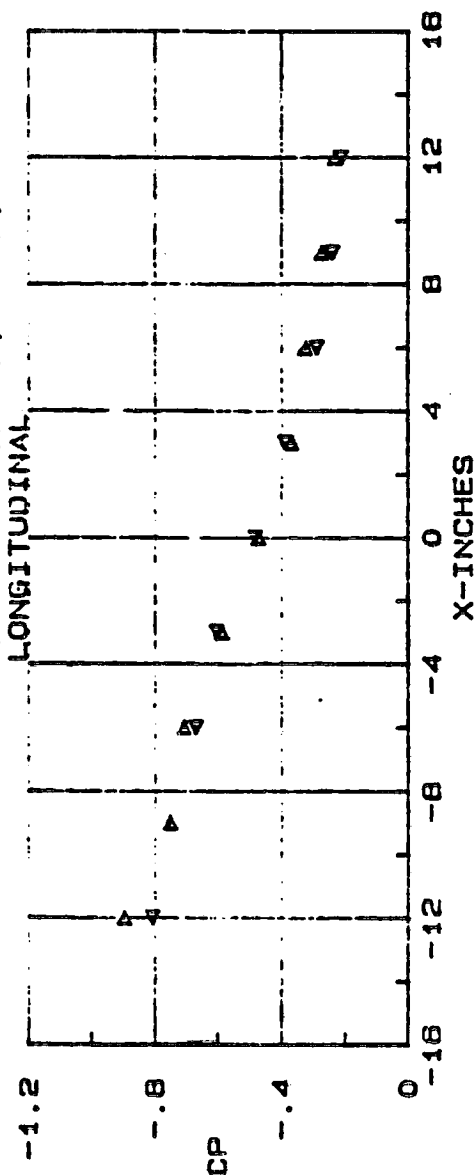


FIGURE 7.3

TEST OS-310

ARC 2x2 TUNNEL
 PANEL PRESSURE COEFFICIENTS
 RUN 109-17 MACH .850 Q= .851 WEDGE: HT 1.5; LT 23.6; AT X=-18.4

SYB Y
 ▲ 10.7
 ▼ -10.7



SYB X
 ▲ -14.5
 ▼ 14.5

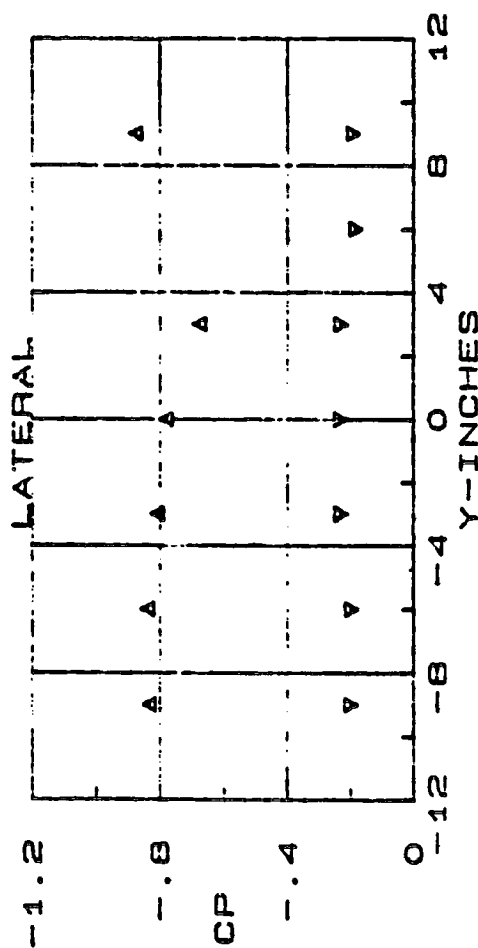
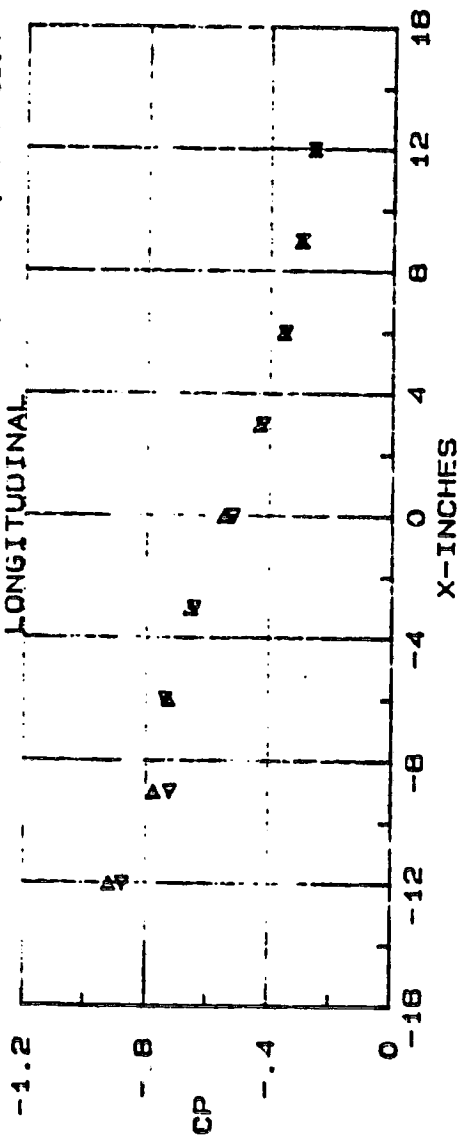


FIGURE 7.H

TEST OS-310

ARC 2x2 TUNNEL
PANEL PRESSURE COEFFICIENTS
RUN 110-4 MACH .652 Q=904 WEDGE HT 1.5; LT 23.6; AT X=18.4

SYB Y
△ 19.7
▽ 19.7



SYB X
△ 14.8
▽ 14.8

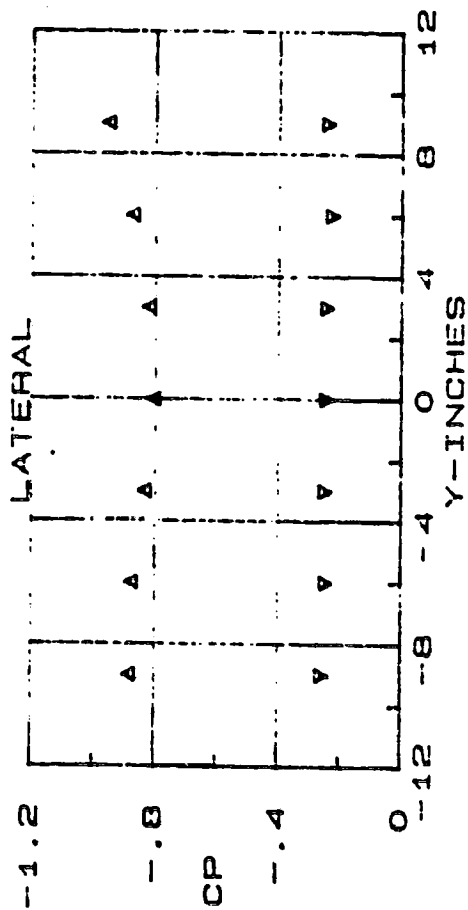


FIGURE 7.1

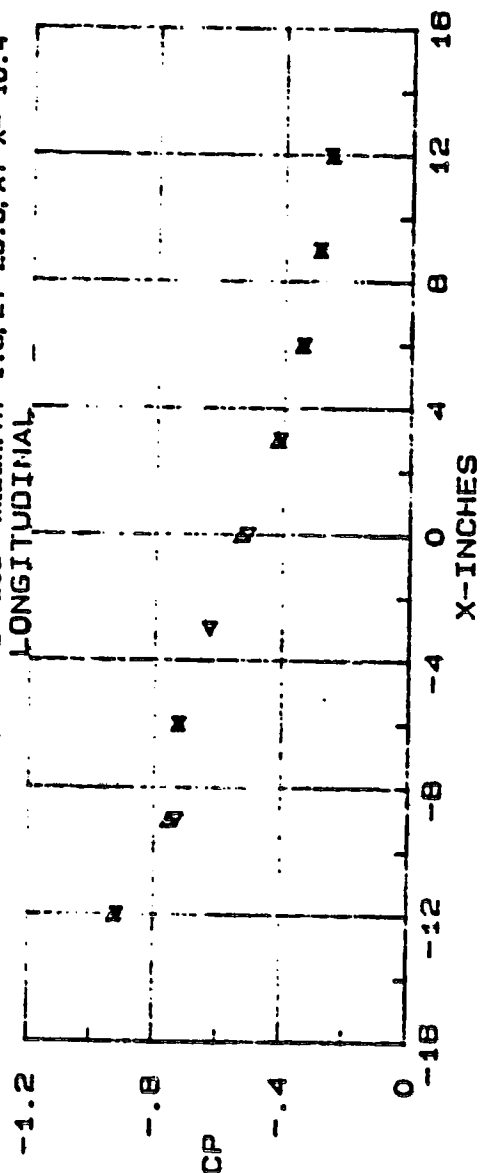
TEST OS-310

ARC 2x2 TUNNEL

PANEL PRESSURE COEFFICIENTS

RUN 111-3 MACH .654 Q-909 WEDGE: HT 1.5; LT 23.8; AT X=-16.4

LONGITUDINAL



LATERAL

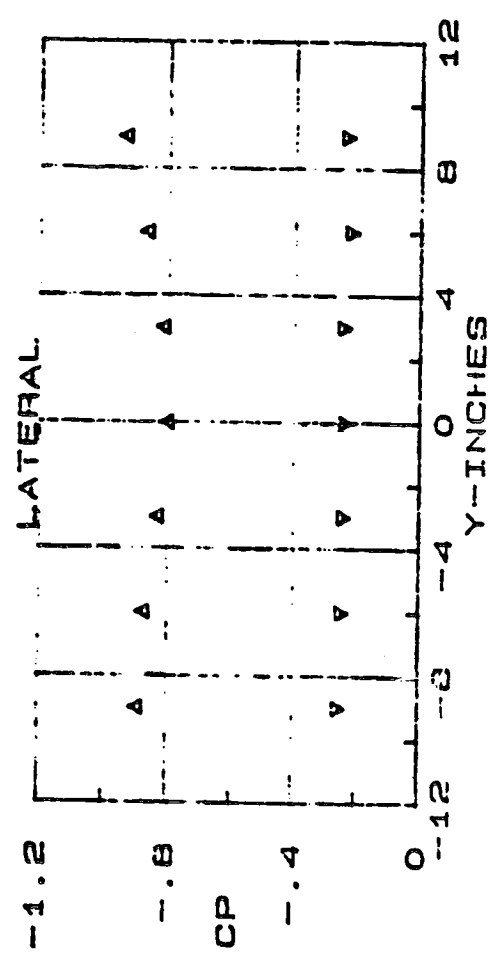


FIGURE 7.J

TEST RESULTS-310

ARC 2x2 TUNNEL
 PANEL PRESSURE COEFFICIENTS
 RUN 112-12 MACH .650 Q= 901 WEDGE: HT 1.5; LT 23.8; AT X=-16.4

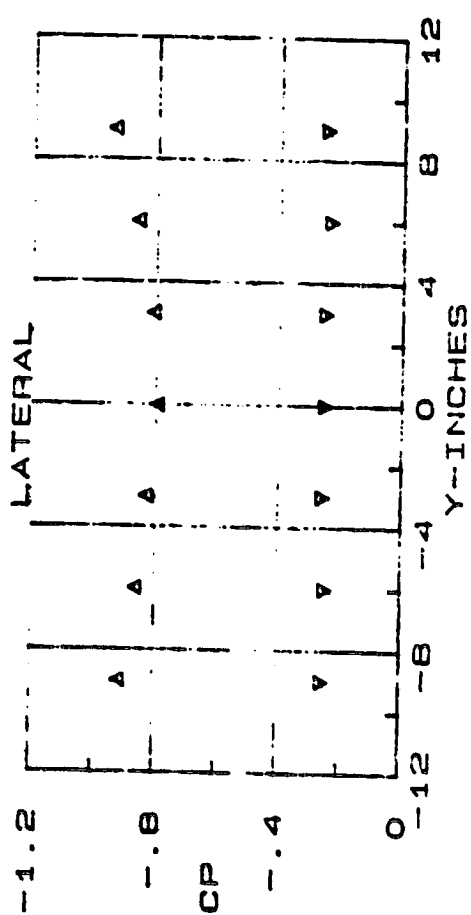
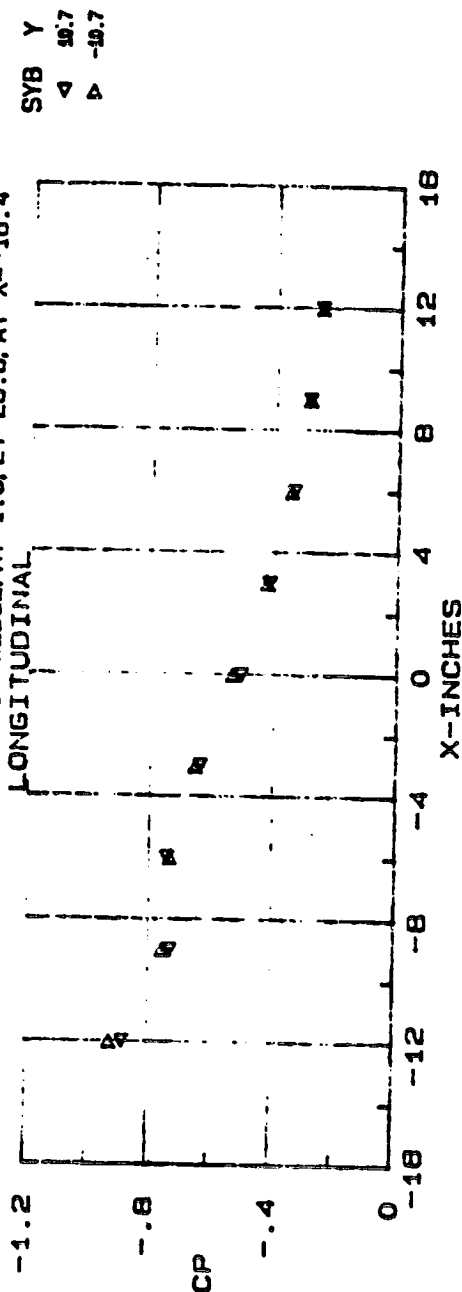
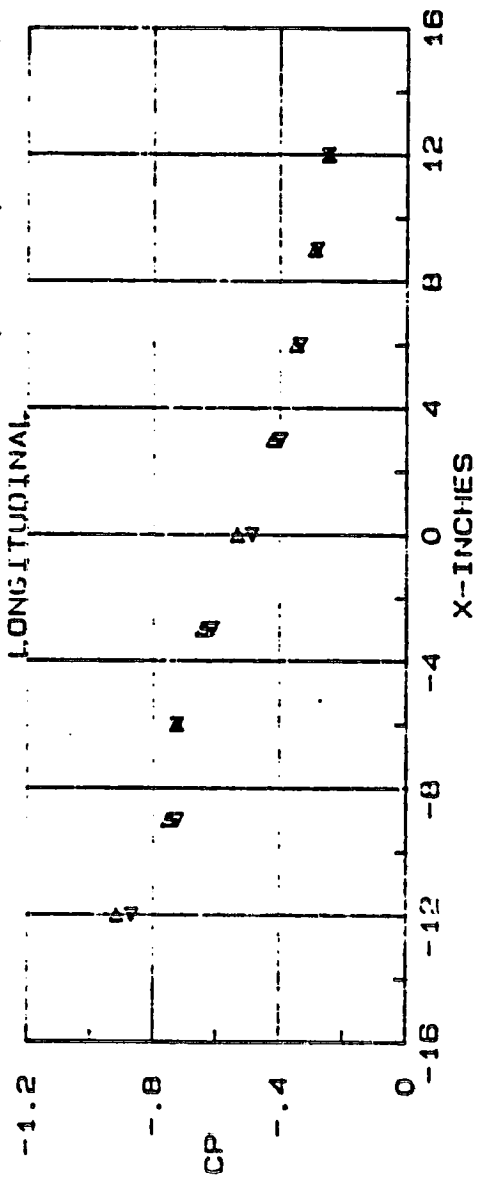


FIGURE 7.K

TLS-310

ARC 2X2 TUNNEL
 PANEL PRESSURE COEFFICIENTS
 RUN 113-10 MACH .651 Q= 903 WEDGE: HT 1.5; LT 23.6; AT X=-16.4

SYB Y
 Δ 10.7
 ▽ -10.7



SYB X
 Δ -14.5
 ▽ 14.5

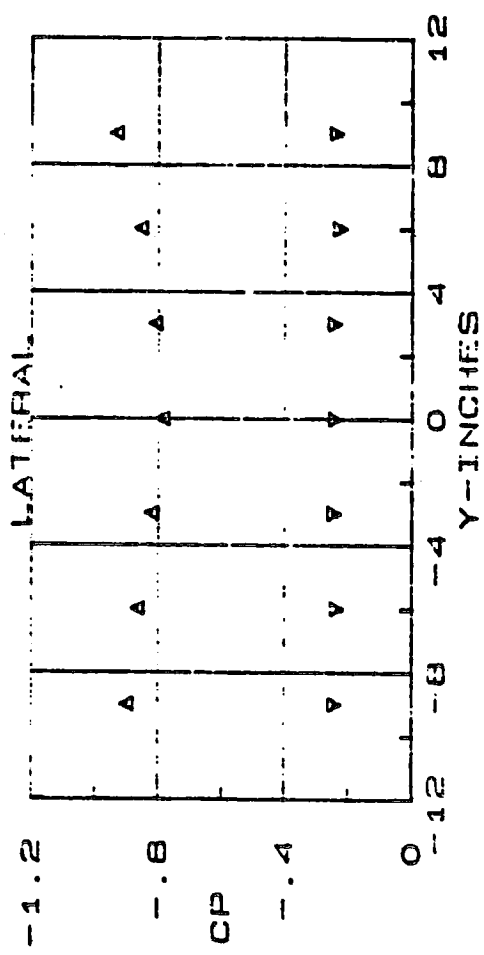


FIGURE 7.L

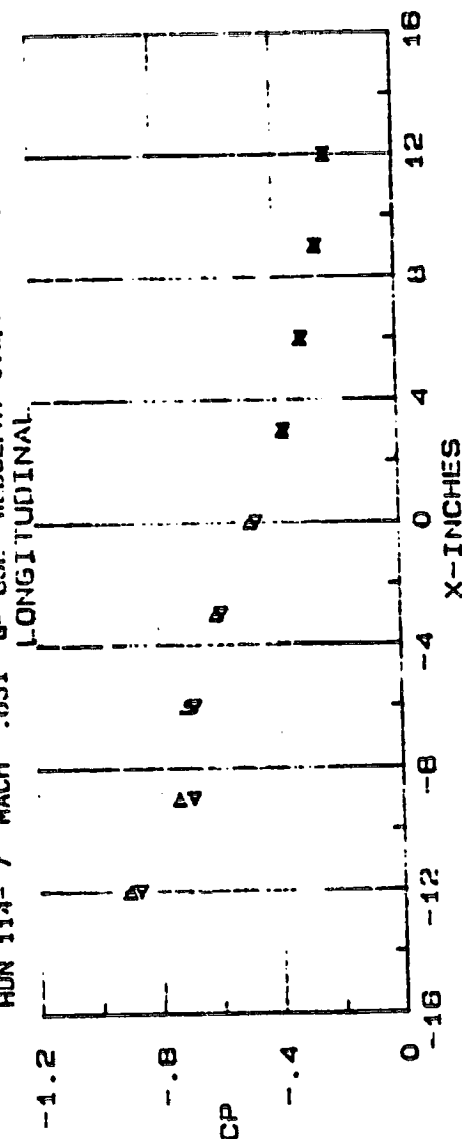
TEST RESULTS 310

ARC 2x2 TUNNEL

PANEL PRESSURE COEFFICIENTS

RUN 114-7 MACH .651 $Q = 652$ WEDGE HT 1.5; LT 23.6; AT X=18.4

SYB Y
 Δ 19.7
 ∇ -19.7



SYB X
 Δ -14.5
 ∇ 14.5

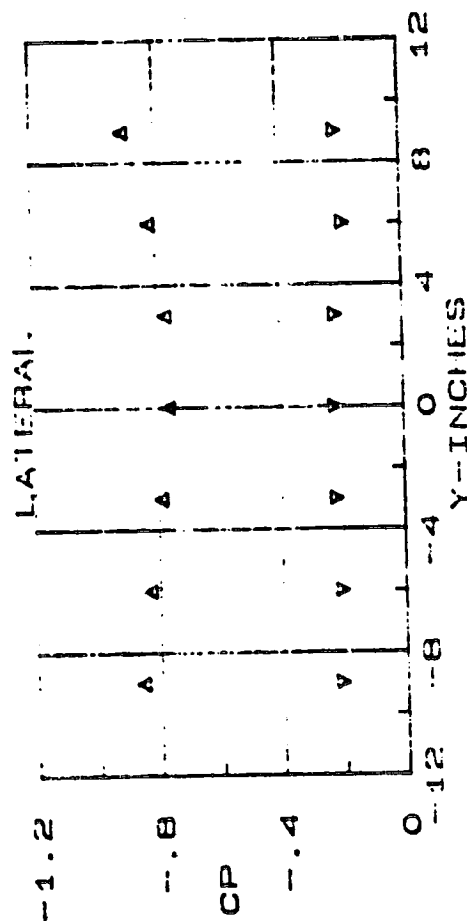
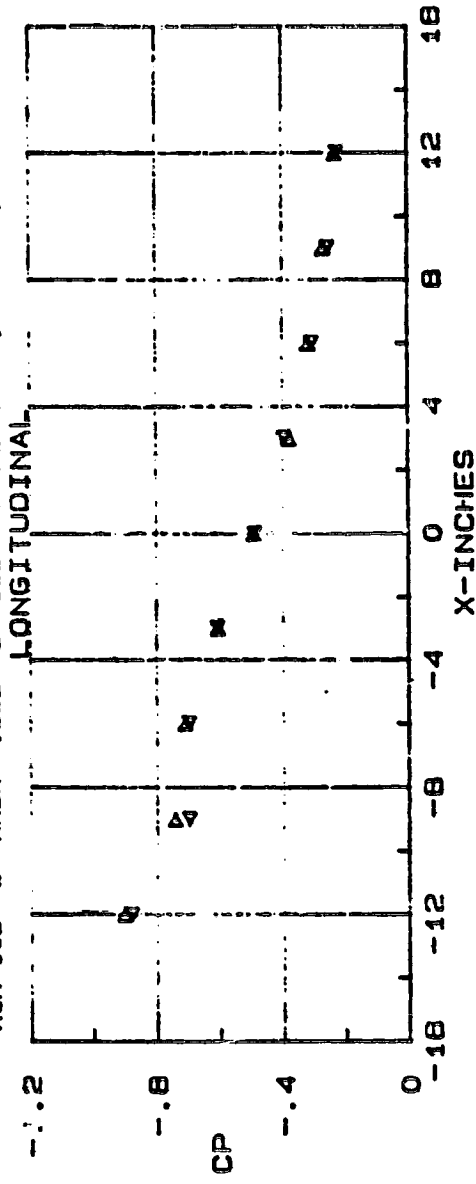


FIGURE 7.M

TEST OS-310

ARC 2*2 TUNNEL
 PANEL PRESSURE COEFFICIENTS
 RUN 115-6 MACH .652 G-653 WEDGE HT 1.5; LT 23.6; AT X=-16.4

SYB Y
 Δ 19.7
 ▽ -19.7



SYB X
 Δ -14.5
 ▽ 14.5

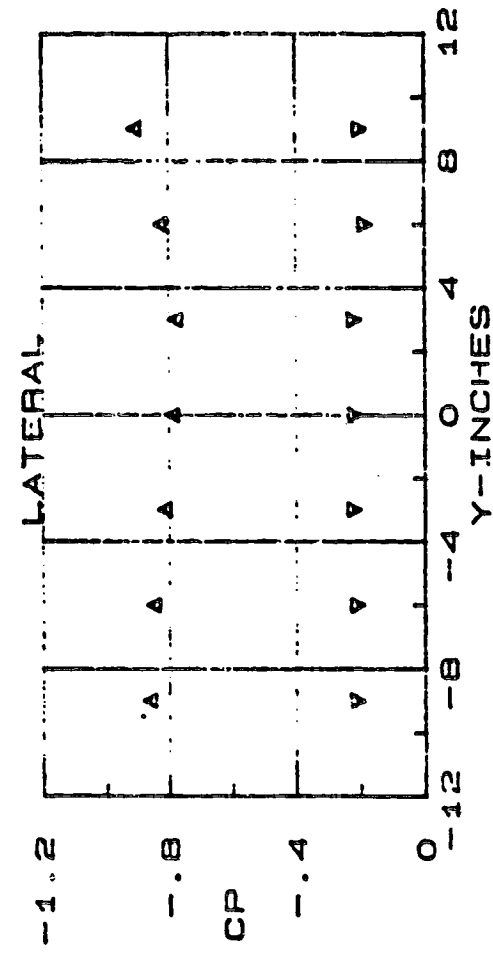
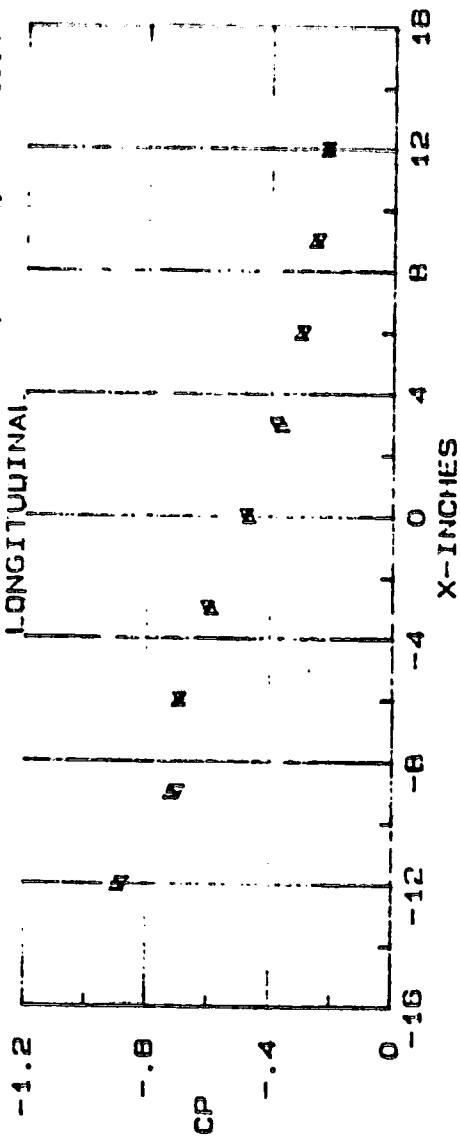


FIGURE 7.N

TEST 03-310

ARC 2*2 TUNNEL
 PANEL PRESSURE COEFFICIENTS
 RUN 116-2 MACH .652 Q= 655 WEDGE HT 1.5; LT 23.6; AT X=-16.4

SYB Y
 Δ 10.7
 ▽ -10.7



SYB X
 Δ -14.5
 ▽ 14.5

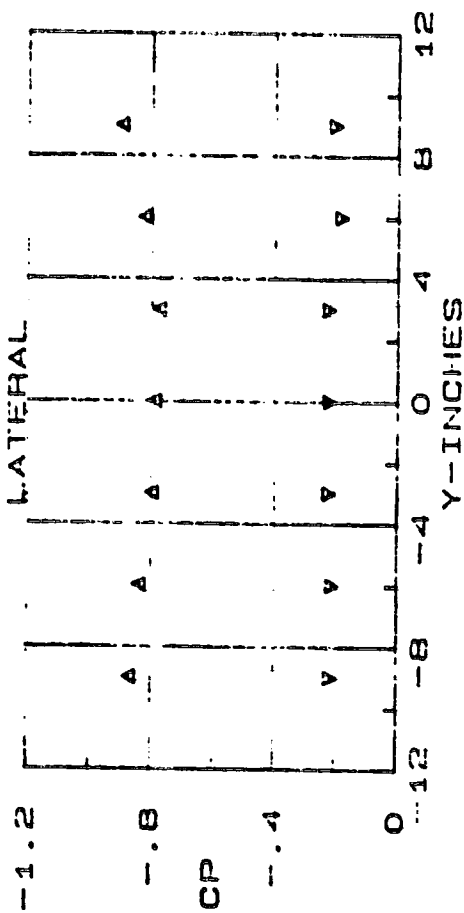
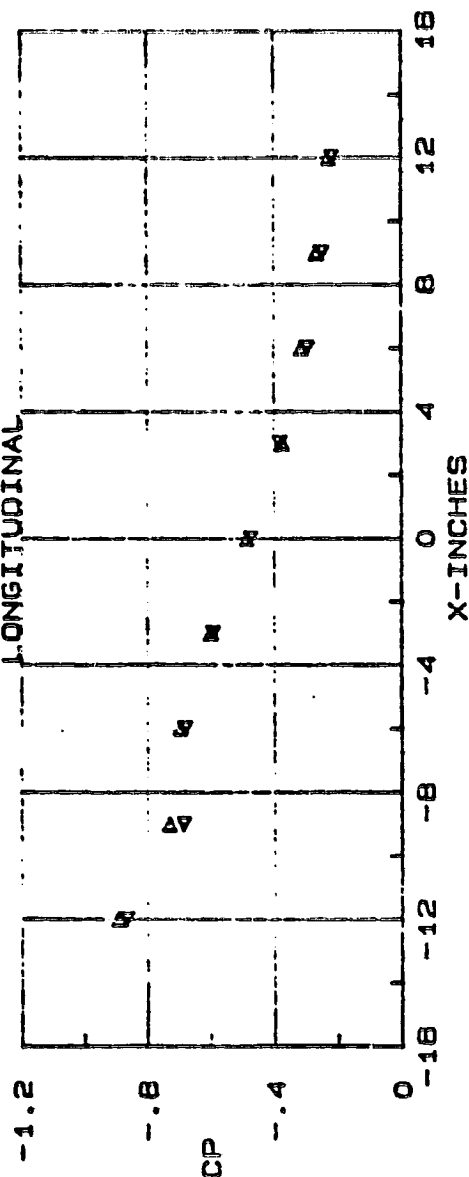


FIGURE 7.0

TEST OS-310

ARC 2*2 TUNNEL
 PANEL PRESSURE COEFFICIENTS
 RUN 117-2 MACH .651 Q= 853 WEDGE: HT 1.5; LT 23.6; AT X=-18.4

SYB Y
 < 13.7
 > -13.7



SYB X
 Δ -14.5
 ▽ 14.5

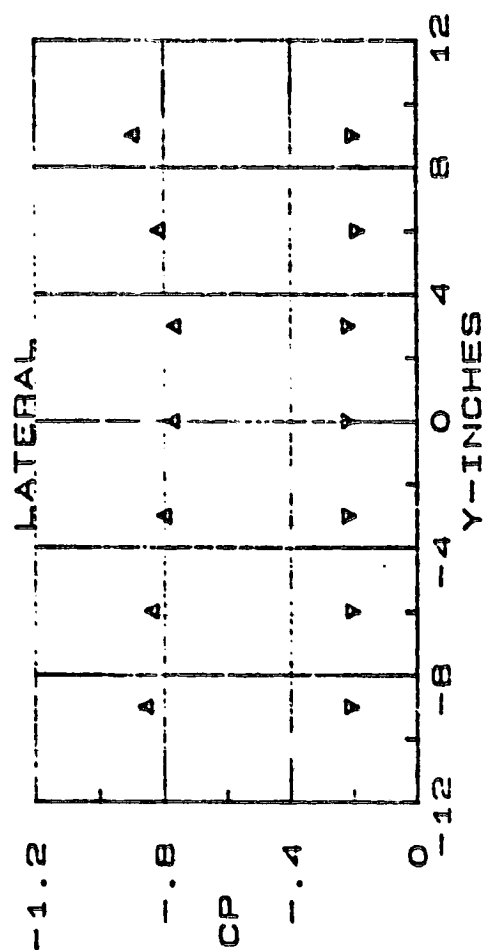


FIGURE 7.P

TEST RESULTS-310

ARC 2x2 TUNNEL
 PANEL PRESSURE COEFFICIENTS
 RUN 116-2 MACH .654 Q= 859 WEDGE: HT 1.5; LT 23.6; AT X=-18.4

SYB Y
 Δ 19.7
 ▽ -19.7

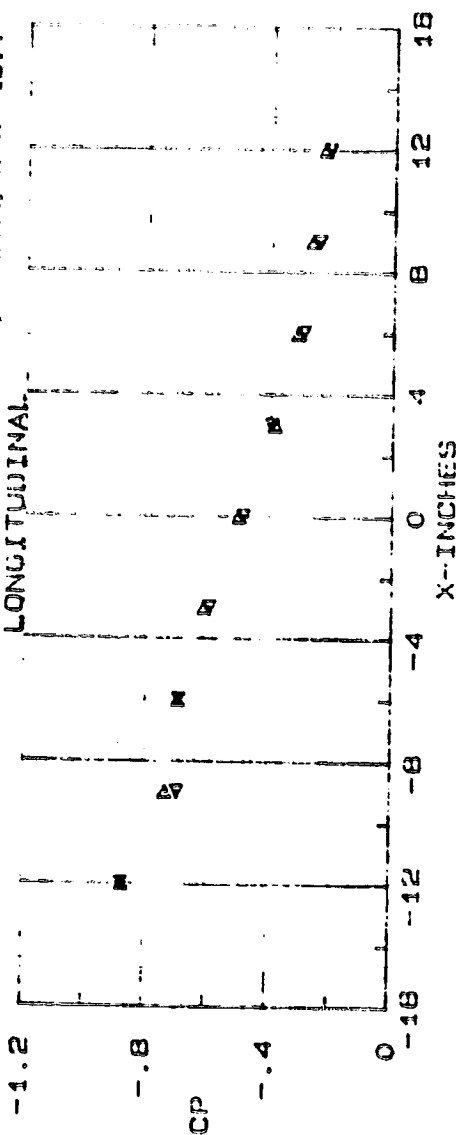
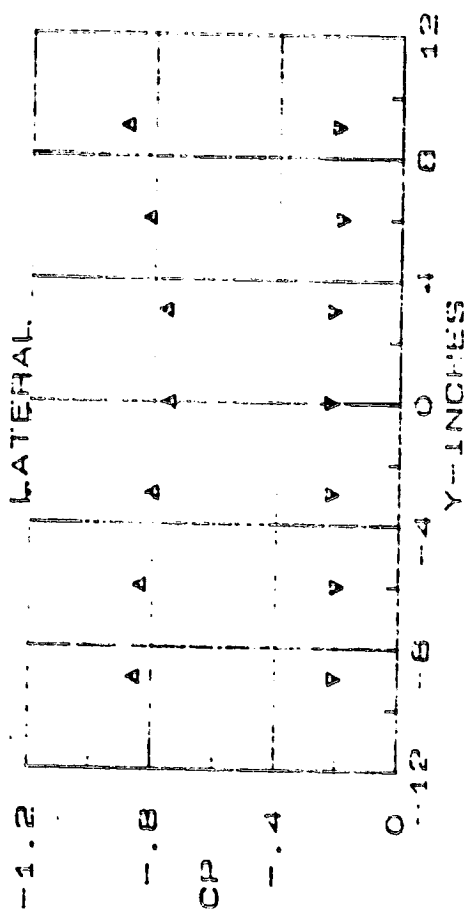
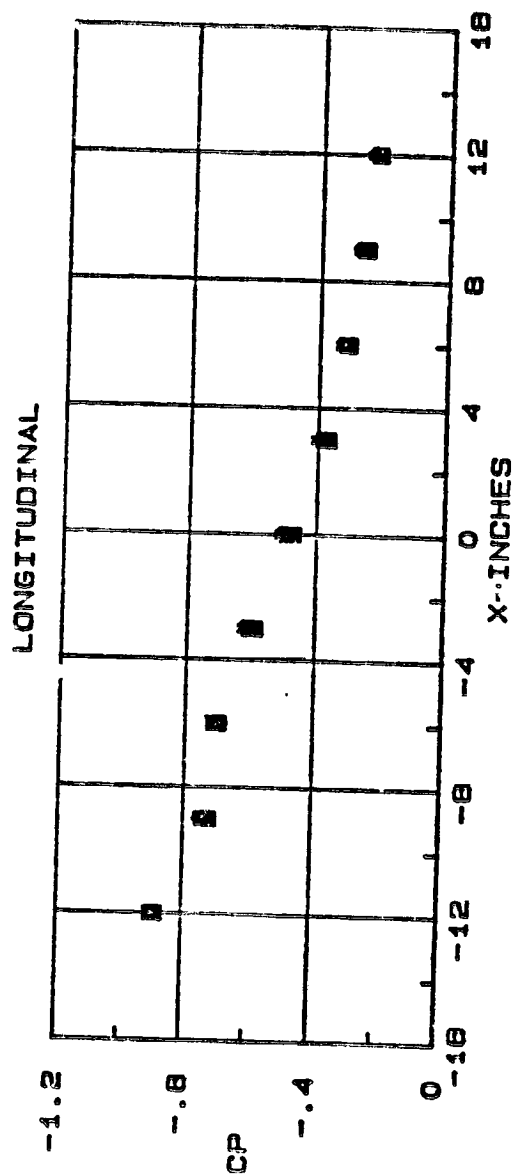


FIGURE 7.Q

SYB X
 Δ -14.5
 ▽ 14.5



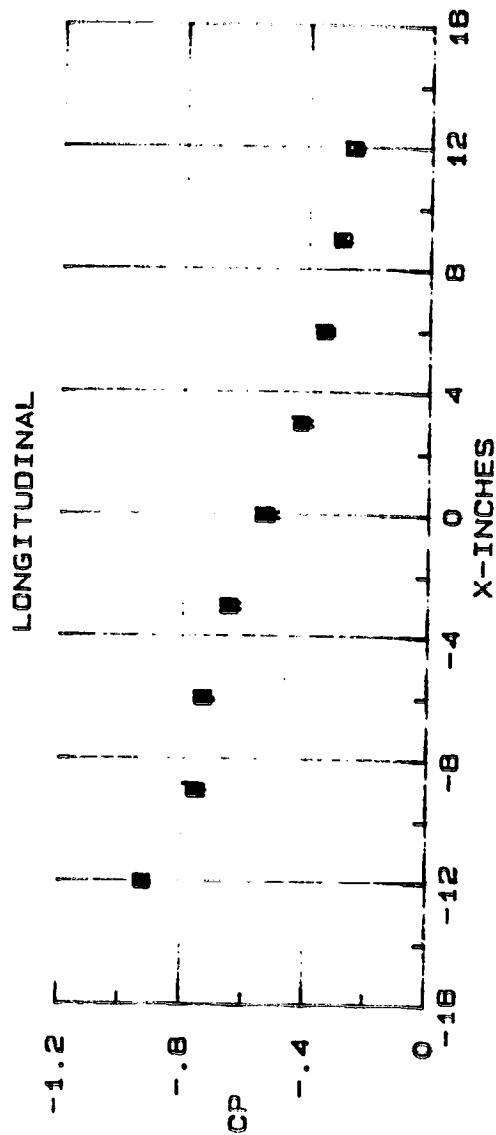
TEST OS-310 ARC 2*2 TUNNEL PANEL PRESSURE COEFFICIENTS



SYB	RUN	SEQ	MACH	Q	WEDGE	HT	LGT	X-STA
□	079	-	01	0.853	0841	1.5	29.80	-18.4
x	100	-	10	0.852	0854	1.5	29.80	-18.4
Δ	109	-	17	0.850	0851	1.5	29.80	-18.4
+	114	-	07	0.851	0852	1.5	29.80	-18.4
∇	116	-	08	0.852	0853	1.5	29.80	-18.4
•	116	-	02	0.852	0853	1.5	29.80	-18.4
∧	117	-	02	0.851	0853	1.5	29.80	-18.4
∩	118	-	02	0.854	0858	1.5	29.80	-18.4

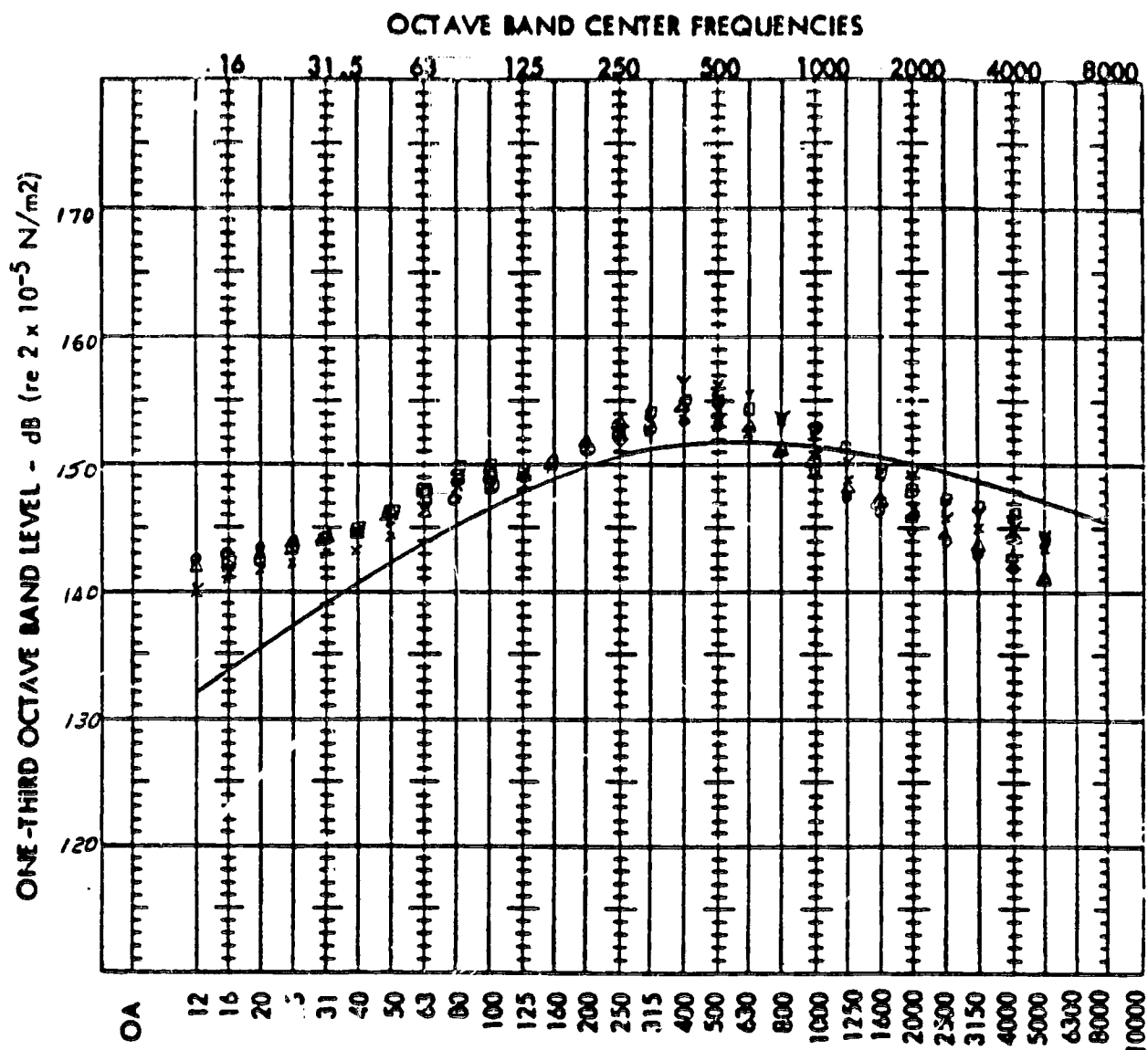
FIGURE 3.A

TEST RESULTS ARC 2*2 TUNNEL PANEL PRESSURE COEFFICIENTS



SYB RUN	SEQ	MACH	Q	WEDGE	HT	LGT	X-STA
0	081	-01	0.951	0983	1.5	23.80	-18.4
1	102	-18	0.850	0902	1.5	23.80	-18.4
2	103	-08	0.850	0901	1.5	23.80	-18.4
3	104	-05	0.853	0905	1.5	23.80	-18.4
4	105	-01	0.851	0902	1.5	23.80	-18.4
5	107	-01	0.852	0907	1.5	23.80	-18.4
6	108	-04	0.854	0900	1.5	23.80	-18.4
7	110	-04	0.852	0904	1.5	23.80	-18.4
8	111	-03	0.854	0908	1.5	23.80	-18.4
9	112	-12	0.850	0901	1.5	23.80	-18.4
10	113	-10	0.851	0903	1.5	23.80	-18.4

FIGURE 8.B

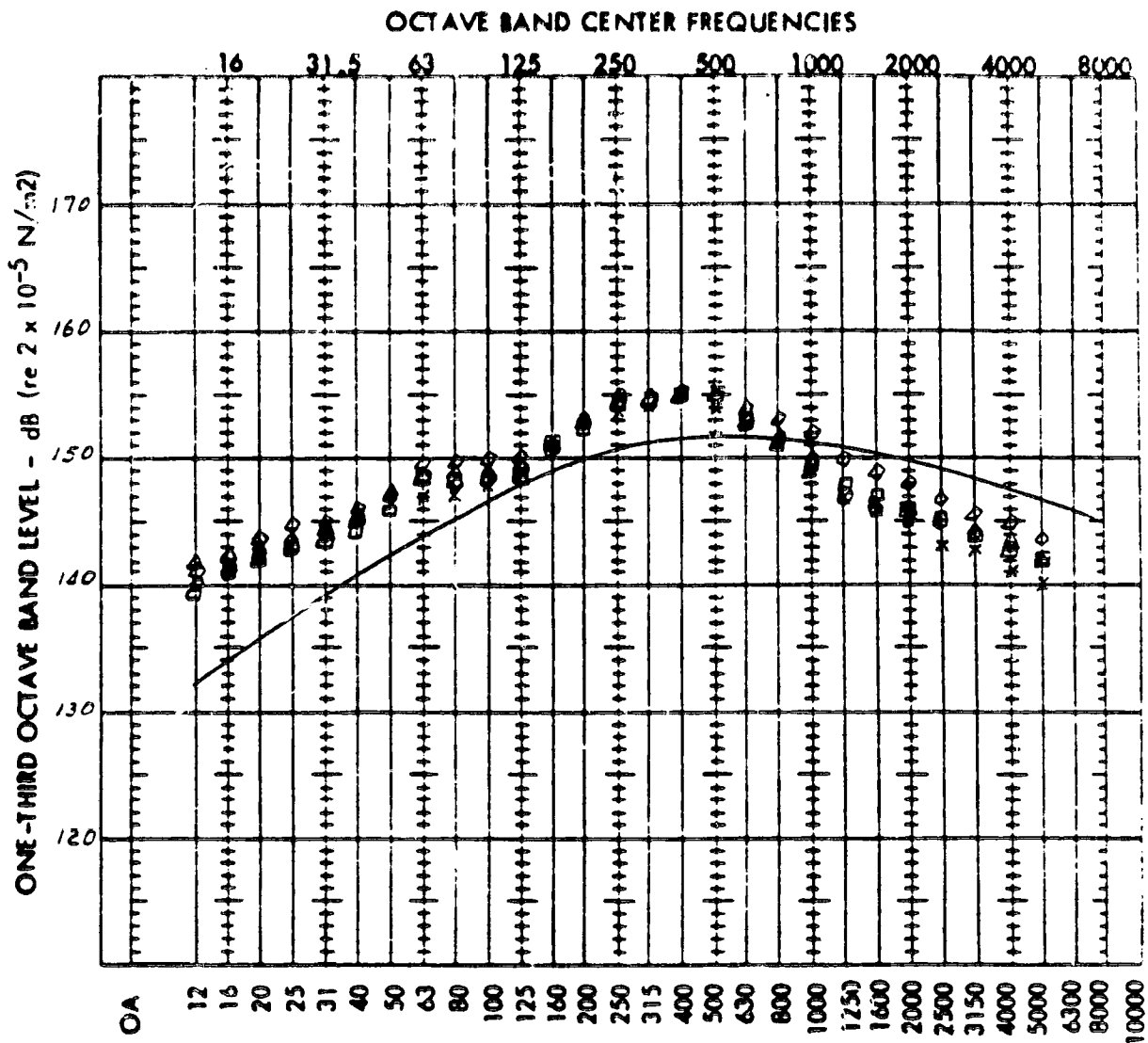


KULITE
 X - No. 1
 O - No. 3
 A - No. 5
 □ - No. 6
 Y - No. 7

$Q = 640$ PSF
 $MACH = 0.65$

— PREDICTED LEVEL FOR CANOPY TOP (NOMINAL)
 FROM SD-74-SH-0082A

FIGURE 9.A



KULITE

· - No. 9

○ - No. 10

△ - No. 11

□ - No. 12

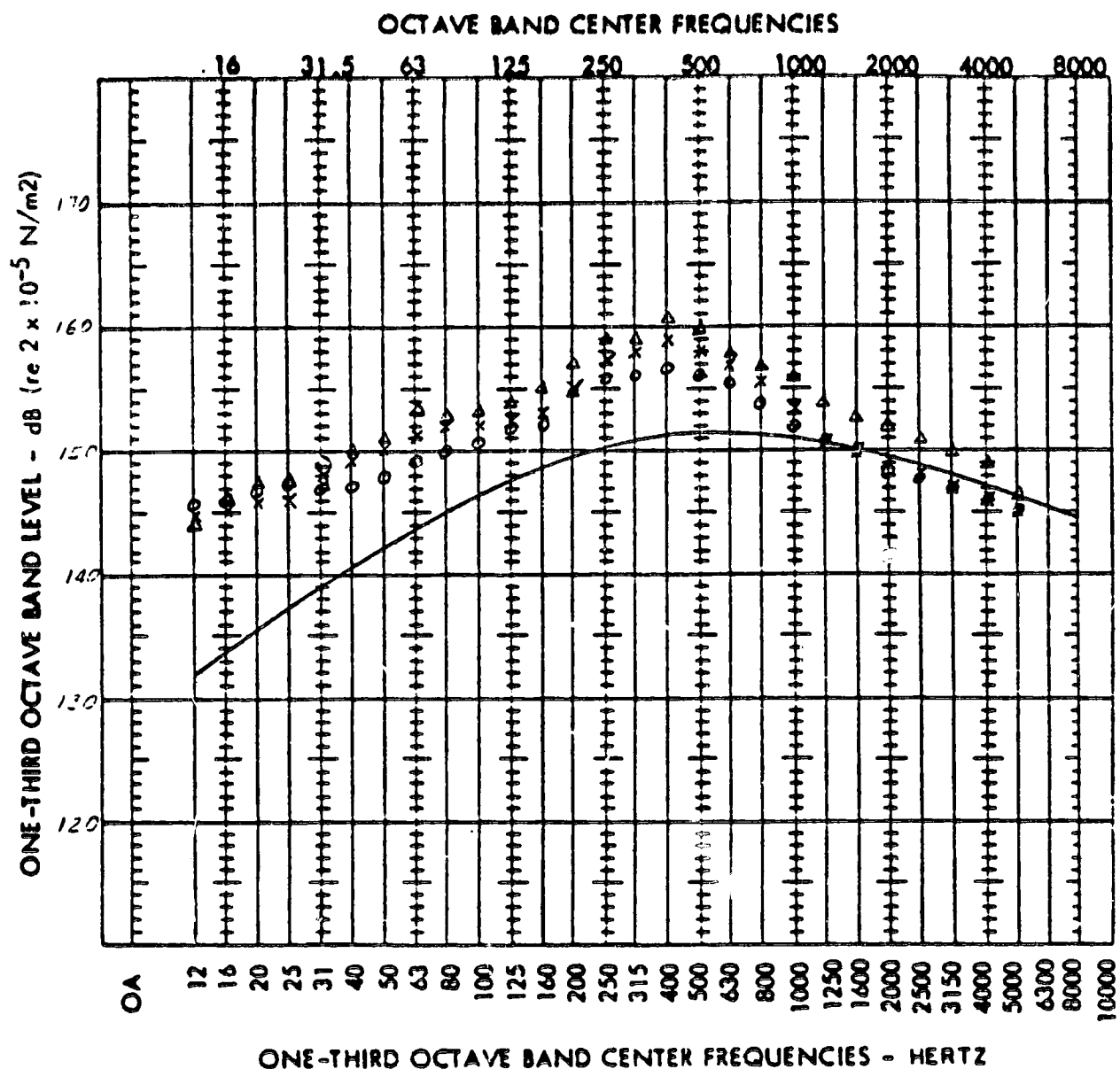
× - No. 15

◇ - No. 18

$Q = 640 \text{ PSF}$
 $MACH = 0.65$

— PREDICTED LEVEL FOR CANOPY TOP (NOMINAL)
 FROM SD-74-SN-0082A

FIGURE 3.1

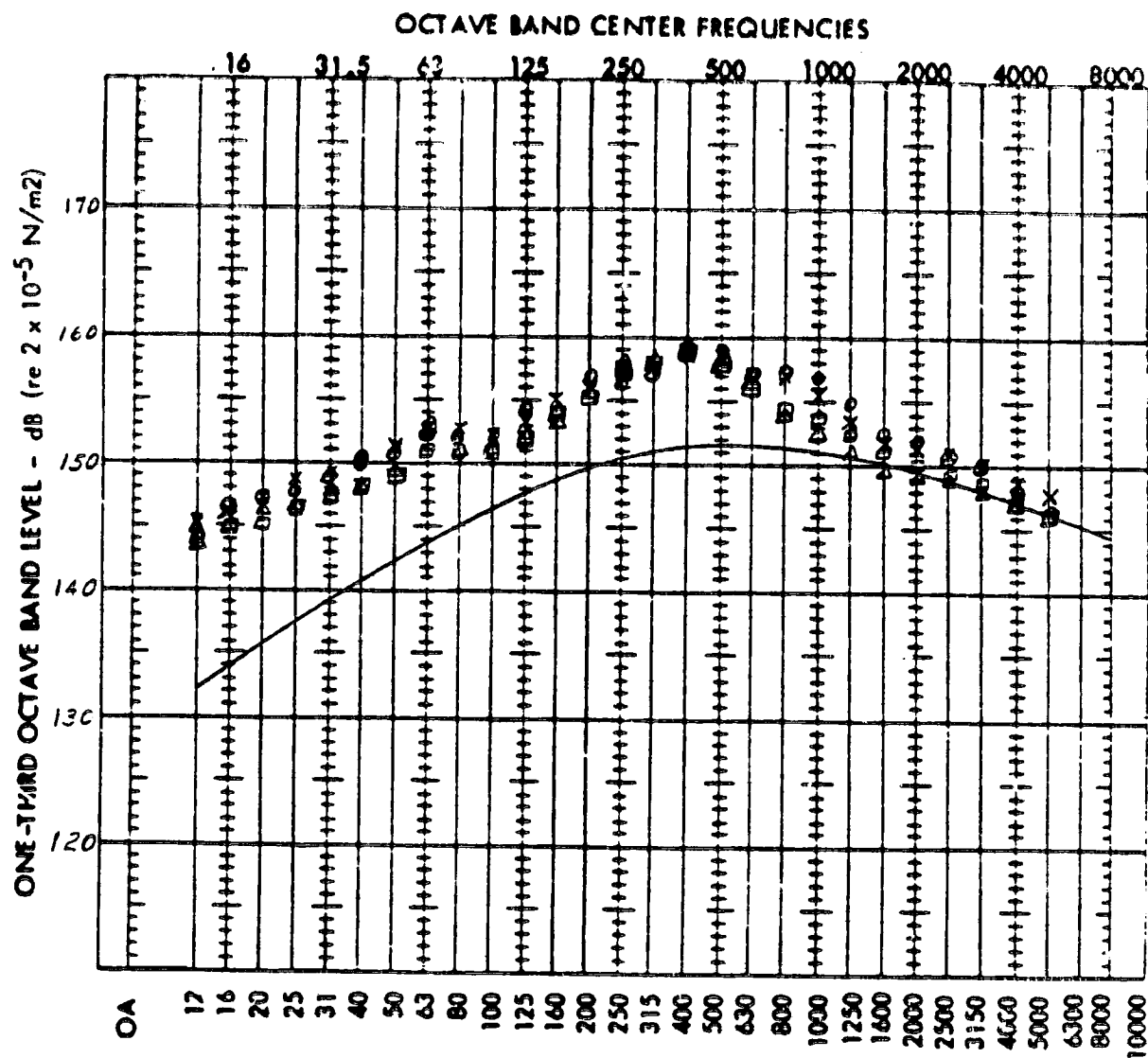


○ - NO. 3
 x - NO. 5
 △ - NO. 7

$Q = 990$ PSF
 $MACH = 0.65$

— PREDICTED LEVEL FOR CANOPY TOP [NOMINAL]
 FROM SD-74-SH-0082A

FIGURE 10.A



- Δ - No. 10
- \square - No. 11
- \times - No. 15
- \circ - No. 21

$Q = 990 \text{ PSF}$
 $MACH = 0.65$

— PREDICTED LEVEL FOR CANOPY TOP (NOMINAL)
 FROM SD-74-SH-0082A

FIGURE 10.B

APPENDIX A

Time-Averaged Pressure Coefficient Tabulated Data

	<u>Page</u>
OIL FLOW RUNS	88
CALIBRATION RUNS	95
DATA RUNS	99

TEST OS-310

DATA SHEET IDENTIFICATION

RUN: SEQ
XXX: XXX

MACH	PT	P	Q	RN	TTF	RO	HW	CONF	TIME
XXX	XXX	XXX	XXX	XXX	XXX	XXX	XXX	XXX	XXX
W01	W02	W03	W04	W05	W06	W07	W08	W09	W10
W11	W12	W13	W14	W15	W16	W17	W18	W19	W20
W21	W22	W23	W24	W25	W26	W27	W28	W29	W30
W31	W32	W33	W34	W35	W36	W37	W38	W39	W40
W41	W42	W43	W44	W45	W46	W47	W48	W49	W50
W51	W52	W53	W54	W55	W56	W57	W58	W59	W60
W61	W62	W63	W64	W65	W66	W67	W68	W69	W70
W71	W72	W73	W74	W75	W76	W77	W78	W79	W80
W81	W82	W83	W84	W85	W86	W87	W88	W89	W90
W91	W92	W93	W94	W95	W96	W97	W98	W99	W00

1	1751-560 P1-1 1A-22 4016	10-PRESSOUT3	10 JAN 83217343	PAGE 0
0	1751-560 P1-1 1A-22 4016	10-PRESSOUT3	10 JAN 83217343	PAGE 1
0	4016			
0	0.751 2132.3 1468.8 577.7 3.575 85.0 0.001748 0.069 0.937			
0	-1.464 -1.161 -1.019 -0.896 -0.820 -0.807 -0.798 -0.841 -0.869 -1.352 -1.218 -1.045 -0.890 -0.877 -0.800 -0.835			
0	-0.870 -0.855 -1.400 -1.524 -1.508 -1.557 -1.560 -1.565 -1.537 1.069 0.448 0.525 1.078 -0.976 0.589 0.774			
0	4017			
0	0.751 2132.3 1468.8 577.7 3.575 85.0 0.001748 0.069 0.937			
0	-1.464 -1.161 -1.019 -0.896 -0.820 -0.807 -0.798 -0.841 -0.869 -1.352 -1.218 -1.045 -0.890 -0.877 -0.800 -0.835			
0	-0.870 -0.855 -1.400 -1.524 -1.508 -1.557 -1.560 -1.565 -1.537 1.069 0.448 0.525 1.078 -0.976 0.589 0.774			
0	4018			
0	0.751 2132.3 1468.8 577.7 3.575 85.0 0.001748 0.069 0.937			
0	-1.464 -1.161 -1.019 -0.896 -0.820 -0.807 -0.798 -0.841 -0.869 -1.352 -1.218 -1.045 -0.890 -0.877 -0.800 -0.835			
0	-0.870 -0.855 -1.400 -1.524 -1.508 -1.557 -1.560 -1.565 -1.537 1.069 0.448 0.525 1.078 -0.976 0.589 0.774			
0	4019			
0	0.751 2132.3 1468.8 577.7 3.575 85.0 0.001748 0.069 0.937			
0	-1.464 -1.161 -1.019 -0.896 -0.820 -0.807 -0.798 -0.841 -0.869 -1.352 -1.218 -1.045 -0.890 -0.877 -0.800 -0.835			
0	-0.870 -0.855 -1.400 -1.524 -1.508 -1.557 -1.560 -1.565 -1.537 1.069 0.448 0.525 1.078 -0.976 0.589 0.774			
0	4020			
0	0.751 2132.3 1468.8 577.7 3.575 85.0 0.001748 0.069 0.937			
0	-1.464 -1.161 -1.019 -0.896 -0.820 -0.807 -0.798 -0.841 -0.869 -1.352 -1.218 -1.045 -0.890 -0.877 -0.800 -0.835			
0	-0.870 -0.855 -1.400 -1.524 -1.508 -1.557 -1.560 -1.565 -1.537 1.069 0.448 0.525 1.078 -0.976 0.589 0.774			
0	4021			
0	0.751 2132.3 1468.8 577.7 3.575 85.0 0.001748 0.069 0.937			
0	-1.464 -1.161 -1.019 -0.896 -0.820 -0.807 -0.798 -0.841 -0.869 -1.352 -1.218 -1.045 -0.890 -0.877 -0.800 -0.835			
0	-0.870 -0.855 -1.400 -1.524 -1.508 -1.557 -1.560 -1.565 -1.537 1.069 0.448 0.525 1.078 -0.976 0.589 0.774			
0	4022			
0	0.751 2132.3 1468.8 577.7 3.575 85.0 0.001748 0.069 0.937			
0	-1.464 -1.161 -1.019 -0.896 -0.820 -0.807 -0.798 -0.841 -0.869 -1.352 -1.218 -1.045 -0.890 -0.877 -0.800 -0.835			
0	-0.870 -0.855 -1.400 -1.524 -1.508 -1.557 -1.560 -1.565 -1.537 1.069 0.448 0.525 1.078 -0.976 0.589 0.774			
0	4023			
0	0.751 2132.3 1468.8 577.7 3.575 85.0 0.001748 0.069 0.937			
0	-1.464 -1.161 -1.019 -0.896 -0.820 -0.807 -0.798 -0.841 -0.869 -1.352 -1.218 -1.045 -0.890 -0.877 -0.800 -0.835			
0	-0.870 -0.855 -1.400 -1.524 -1.508 -1.557 -1.560 -1.565 -1.537 1.069 0.448 0.525 1.078 -0.976 0.589 0.774			
0	4024			
0	0.751 2132.3 1468.8 577.7 3.575 85.0 0.001748 0.069 0.937			
0	-1.464 -1.161 -1.019 -0.896 -0.820 -0.807 -0.798 -0.841 -0.869 -1.352 -1.218 -1.045 -0.890 -0.877 -0.800 -0.835			
0	-0.870 -0.855 -1.400 -1.524 -1.508 -1.557 -1.560 -1.565 -1.537 1.069 0.448 0.525 1.078 -0.976 0.589 0.774			
0	4025			
0	0.751 2132.3 1468.8 577.7 3.575 85.0 0.001748 0.069 0.937			
0	-1.464 -1.161 -1.019 -0.896 -0.820 -0.807 -0.798 -0.841 -0.869 -1.352 -1.218 -1.045 -0.890 -0.877 -0.800 -0.835			
0	-0.870 -0.855 -1.400 -1.524 -1.508 -1.557 -1.560 -1.565 -1.537 1.069 0.448 0.525 1.078 -0.976 0.589 0.774			
0				

[illegible]

0	0.257	2453.2	1708.7	684.5	4.409	110.5	0.001942	0.035	0.1344	-1.373	-1.095	-0.975	-0.862	-0.825
-	0.216	-1.548	-1.117	-0.952	-0.854	-0.796	-0.010	-0.026	-0.262	-1.571	0.377	-0.906	-0.947	0.315
-	0.030	0.050	0.468	0.477	0.427	0.439	0.462	0.428	0.242	-0.098	0.030	-0.906	-0.947	0.315
0	RUN:SEC													
0	5412													
0	0.313	2146.1	2005.4	137.4	2.094	71.1	0.002245	0.066	0.1449	-0.203	-0.097	-0.100	-0.029	-0.014
-	0.510	-0.518	-0.125	-0.071	-0.036	-0.027	-0.026	-0.553	-0.563	-0.203	-0.369	-0.028	-0.031	-0.613
-	0.097	-0.004	-0.609	-0.221	-0.470	-0.452	-0.542	-0.564	-0.997	-2.567	-2.034	-0.028	-0.031	-0.613
1751-500 PM-1 JAN-22 5413	10-PRESSOUT3 10 JAN 0321743													
0	RUN:SEC													
0	5412													
0	0.314	2144.8	2002.9	138.4	2.102	70.9	0.002243	0.077	0.1450	-0.183	-0.059	-0.102	-0.032	-0.018
-	0.450	-0.251	-0.166	-0.075	-0.042	-0.010	-0.014	-0.012	-0.539	-0.334	-0.183	-0.059	-0.032	-0.018
-	0.011	-0.010	-0.615	-0.221	-0.473	-0.467	-0.544	-0.548	-0.969	-2.494	-1.990	-0.356	-0.023	-0.601
0	RUN:SEC													
0	5511													
0	0.405	2144.4	1911.4	223.5	2.656	70.7	0.002170	0.060	0.1455	-0.142	-0.138	-0.060	-0.042	-0.042
-	0.545	-0.367	-0.231	-0.164	-0.104	-0.062	-0.050	-0.048	-0.595	-0.421	-0.259	-0.159	-0.054	-0.002
-	0.034	-0.021	-0.650	-0.239	-0.570	-0.525	-0.516	-0.579	-0.223	-1.146	-0.839	-0.148	-0.056	-0.004
0	RUN:SEC													
0	5512													
0	0.410	2145.7	1911.5	224.0	2.664	70.5	0.002172	0.071	0.1455	-0.237	-0.133	-0.131	-0.054	-0.037
-	0.525	-0.344	-0.216	-0.150	-0.095	-0.054	-0.036	-0.030	-0.571	-0.393	-0.237	-0.133	-0.054	-0.037
-	0.025	-0.026	-0.672	-0.242	-0.581	-0.544	-0.531	-0.610	-0.233	-1.132	-0.834	-0.148	-0.056	-0.004
0	RUN:SEC													
0	5511													
0	0.410	2145.7	1910.8	223.2	2.668	70.5	0.002171	0.071	0.1456	-0.233	-0.139	-0.139	-0.059	-0.040
-	0.518	-0.344	-0.216	-0.150	-0.092	-0.052	-0.032	-0.030	-0.569	-0.385	-0.233	-0.139	-0.059	-0.040
-	0.032	-0.030	-0.673	-0.251	-0.581	-0.539	-0.533	-0.608	-0.239	-1.118	-0.829	-0.142	-0.056	-0.009
1751-500 PM-1 JAN-22 5611	10-PRESSOUT3 10 JAN 0321743													
0	RUN:SEC													
0	5611													
0	0.508	2146.2	1799.9	324.8	3.168	71.9	0.002075	0.065	0.1501	-0.292	-0.181	-0.177	-0.037	-0.067
-	0.546	-0.401	-0.257	-0.153	-0.130	-0.086	-0.063	-0.057	-0.615	-0.437	-0.292	-0.177	-0.034	0.311
-	0.016	-0.021	-0.653	-0.267	-0.625	-0.581	-0.571	-0.646	-0.143	-0.452	-0.252	-0.077	-0.034	0.311
0	RUN:SEC													
0	5612													
0	0.508	2147.1	1800.2	325.3	3.171	71.9	0.002075	0.059	0.1501	-0.179	-0.170	-0.083	-0.083	-0.065
-	0.563	-0.404	-0.259	-0.190	-0.134	-0.087	-0.063	-0.056	-0.612	-0.440	-0.293	-0.077	-0.084	0.311
-	0.014	-0.021	-0.652	-0.267	-0.621	-0.572	-0.575	-0.642	-0.125	-0.457	-0.227	-0.077	-0.084	0.311

0	HLA:SLC	56:2	2146.7	1000.1	325.1	3.169	71.9	0.002075	0.053	0	1502	-0.619	-0.437	-0.285	-0.173	-0.168	-0.082	-0.062
0	HLA:SLC	56:2	-0.608	-0.407	-0.175	-0.131	-0.086	-0.059	-0.047	-0.619	-0.437	-0.285	-0.173	-0.168	-0.082	-0.062	-0.069	-0.259
0	HLA:SLC	56:2	-0.052	-0.048	-0.045	-0.017	-0.279	-0.565	-0.640	-0.642	0.110	-0.461	-0.262	0.339	-0.091	-0.089	-0.089	-0.259
0	HLA:SLC	57:1	2146.7	1000.1	325.1	3.586	75.1	0.001962	0.058	0	1507	-0.675	-0.520	-0.378	-0.244	-0.225	-0.129	-0.106
0	HLA:SLC	57:1	-0.608	-0.407	-0.175	-0.131	-0.086	-0.059	-0.047	-0.675	-0.520	-0.378	-0.244	-0.225	-0.129	-0.106	-0.125	-0.450
0	HLA:SLC	57:1	-0.052	-0.048	-0.045	-0.017	-0.279	-0.565	-0.640	-0.642	0.110	-0.461	-0.262	0.339	-0.091	-0.089	-0.089	-0.259
0	HLA:SLC	57:2	2146.7	1000.1	325.1	3.586	75.1	0.001962	0.058	0	1507	-0.675	-0.520	-0.378	-0.244	-0.225	-0.129	-0.106
0	HLA:SLC	57:2	-0.608	-0.407	-0.175	-0.131	-0.086	-0.059	-0.047	-0.675	-0.520	-0.378	-0.244	-0.225	-0.129	-0.106	-0.125	-0.450
0	HLA:SLC	57:2	-0.052	-0.048	-0.045	-0.017	-0.279	-0.565	-0.640	-0.642	0.110	-0.461	-0.262	0.339	-0.091	-0.089	-0.089	-0.259
0	HLA:SLC	57:2	2146.7	1000.1	325.1	3.586	75.1	0.001962	0.058	0	1507	-0.675	-0.520	-0.378	-0.244	-0.225	-0.129	-0.106
0	HLA:SLC	57:2	-0.608	-0.407	-0.175	-0.131	-0.086	-0.059	-0.047	-0.675	-0.520	-0.378	-0.244	-0.225	-0.129	-0.106	-0.125	-0.450
0	HLA:SLC	57:2	-0.052	-0.048	-0.045	-0.017	-0.279	-0.565	-0.640	-0.642	0.110	-0.461	-0.262	0.339	-0.091	-0.089	-0.089	-0.259
0	HLA:SLC	57:2	2146.7	1000.1	325.1	3.586	75.1	0.001962	0.058	0	1507	-0.675	-0.520	-0.378	-0.244	-0.225	-0.129	-0.106
0	HLA:SLC	57:2	-0.608	-0.407	-0.175	-0.131	-0.086	-0.059	-0.047	-0.675	-0.520	-0.378	-0.244	-0.225	-0.129	-0.106	-0.125	-0.450
0	HLA:SLC	57:2	-0.052	-0.048	-0.045	-0.017	-0.279	-0.565	-0.640	-0.642	0.110	-0.461	-0.262	0.339	-0.091	-0.089	-0.089	-0.259
0	HLA:SLC	57:2	2146.7	1000.1	325.1	3.586	75.1	0.001962	0.058	0	1507	-0.675	-0.520	-0.378	-0.244	-0.225	-0.129	-0.106
0	HLA:SLC	57:2	-0.608	-0.407	-0.175	-0.131	-0.086	-0.059	-0.047	-0.675	-0.520	-0.378	-0.244	-0.225	-0.129	-0.106	-0.125	-0.450
0	HLA:SLC	57:2	-0.052	-0.048	-0.045	-0.017	-0.279	-0.565	-0.640	-0.642	0.110	-0.461	-0.262	0.339	-0.091	-0.089	-0.089	-0.259
0	HLA:SLC	57:2	2146.7	1000.1	325.1	3.586	75.1	0.001962	0.058	0	1507	-0.675	-0.520	-0.378	-0.244	-0.225	-0.129	-0.106
0	HLA:SLC	57:2	-0.608	-0.407	-0.175	-0.131	-0.086	-0.059	-0.047	-0.675	-0.520	-0.378	-0.244	-0.225	-0.129	-0.106	-0.125	-0.450
0	HLA:SLC	57:2	-0.052	-0.048	-0.045	-0.017	-0.279	-0.565	-0.640	-0.642	0.110	-0.461	-0.262	0.339	-0.091	-0.089	-0.089	-0.259
0	HLA:SLC	57:2	2146.7	1000.1	325.1	3.586	75.1	0.001										

0	0.774	2143.7	1446.5	506.0	3.969	96.2	0.501698	0.068	0	1521	-0.346	-1.036	-0.919	-0.793	-0.873	-0.739	-0.797
-	-1.140	-1.065	-0.879	-0.012	-0.757	-0.758	-0.756	-0.794	-0.840	-1.346	-0.474	0.209	0.370	0.697	-0.853	-0.944	0.697
-	-0.915	-0.824	-1.454	-1.476	-1.406	-1.445	-1.435	-1.408	-1.456								
0	RUM:SEC																
0	5912	2148.8	1446.6	604.0	3.961	97.2	0.501695	0.067	0	1522	-1.343	-1.041	-0.921	-0.793	-0.877	-0.749	-0.814
-	-1.126	-1.064	-0.901	-0.698	-0.760	-0.764	-0.759	-0.790	-0.832	0.440	0.180	0.354	0.667	-0.896	-0.943	0.693	
-	-0.933	-0.864	-1.452	-1.474	-1.406	-1.447	-1.439	-1.406	-1.446								
0	RUM:SEC																
0	5911	2825.4	2022.7	709.2	5.033	90.4	0.002338	0.085	0	1523	-0.239	-0.674	-0.545	-0.403	-0.375	-0.251	-0.221
-	-0.708	-0.683	-0.475	-0.290	-0.246	-0.284	-0.242	-0.211	-0.190	-0.437	-0.655	-0.503	-0.238	-0.207	-0.159	-0.201	
-	-0.103	-0.174	-0.146	-0.872	-0.835	-0.807	-0.782	-0.867	-0.920								
1157-560 PM-1 IN-22 41:11	10-PRESSRU73																
0	RUM:SEC																
0	6121	3103.7	2293.6	708.4	5.622	91.6	0.002463	0.031	0	1528	-0.867	-0.705	-0.570	-0.436	-0.401	-0.283	-0.250
-	-0.810	-0.712	-0.511	-0.421	-0.376	-0.316	-0.266	-0.235	-0.213	-0.736	-0.928	-0.791	-0.536	-0.226	-0.248	-0.521	
-	-0.122	-0.204	-0.522	-0.940	-0.898	-0.865	-0.833	-0.928	-0.891								
0	RUM:SEC																
0	6231	3523.2	2440.9	882.3	6.227	94.3	0.002938	0.048	0	1532	-0.862	-0.694	-0.564	-0.438	-0.406	-0.283	-0.251
-	-0.704	-0.725	-0.522	-0.429	-0.386	-0.325	-0.264	-0.237	-0.215	-0.931	-1.092	-0.980	-0.770	-0.228	-0.241	-0.740	
-	-0.222	-0.204	-0.531	-0.942	-0.898	-0.862	-0.825	-0.917	-0.878								
0	RUM:SEC																
0	6411	4253.2	1856.7	425.9	3.677	60.3	0.001993	0.055	0	934	-0.771	-0.621	-0.585	-0.303	-0.394	-0.290	-0.231
-	-0.711	-0.553	-0.450	-0.489	-0.366	-0.286	-0.219	-0.178	-0.142	0.517	0.449	0.529	0.341	-0.173	-0.140	0.693	
-	-0.184	-0.161	-0.810	-0.732	-0.679	-0.643	-0.685	-0.724	-0.749								
0	RUM:SEC																
0	6517	4777.6	1665.9	477.6	3.675	62.7	0.001999	0.070	0	936	-0.783	-0.627	-0.591	-0.308	-0.398	-0.291	-0.221
-	-0.725	-0.666	-0.563	-0.501	-0.386	-0.296	-0.219	-0.186	-0.141	0.564	0.497	0.577	0.370	-0.173	-0.162	0.662	2
-	-0.177	-0.153	-0.852	-0.741	-0.691	-0.689	-0.709	-0.741	-0.768								
1157-560 PM-1 IN-22 65:11	10-PRESSRU73																
0	RUM:SEC																
0	6511	2856.0	2227.6	573.4	4.083	65.7	0.002653	0.061	0	945	-0.801	-0.651	-0.617	-0.342	-0.427	-0.324	-0.255
-	-0.761	-0.632	-0.625	-0.532	-0.408	-0.316	-0.242	-0.195	-0.167	-0.536	-0.656	-0.611	-0.449	-0.150	-0.179	-0.461	
-	-1.205	-0.171	-0.831	-0.748	-0.695	-0.682	-0.717	-0.757	-0.777								

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PAGE 11

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PAGE 12

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0	0.653	2177.7	2160.7	645.3	5.052	75.4	0.002534	0.056	0	1054	-0.698	-0.615	-0.509	-0.396	-0.317
-	-0.437	-0.701	-0.592	-0.477	-0.390	-0.334	-0.285	-0.252	-0.090	-0.741	-0.374	-0.241	-0.247	-0.240	-0.237
-	-0.266	-0.229	-0.511	-0.844	-0.788	-0.796	-0.843	-0.860	-0.315	-0.394	-0.364	-0.232	-0.245	-0.237	-0.274
0	RUN:SEC														
0	7112														
0	0.554	2367.6	2152.1	643.7	5.020	76.1	0.002561	0.037	0	1056	-0.686	-0.623	-0.517	-0.404	-0.323
-	-0.842	-0.712	-0.705	-0.595	-0.475	-0.386	-0.323	-0.273	-0.880	-0.726	-0.368	-0.236	-0.245	-0.237	-0.274
-	-0.269	-0.224	-0.520	-0.847	-0.785	-0.793	-0.788	-0.834	-0.311	-0.368	-0.364	-0.232	-0.245	-0.237	-0.274
0	RUN:SEC														
0	7211														
0	0.654	3512.0	2680.5	802.0	6.136	81.3	0.003134	0.052	0	1100	-0.710	-0.639	-0.523	-0.416	-0.338
-	-0.355	-0.732	-0.723	-0.617	-0.458	-0.413	-0.345	-0.298	-0.890	-0.739	-0.938	-0.833	-0.760	-0.751	-0.859
-	-0.287	-0.251	-0.949	-0.873	-0.812	-0.819	-0.810	-0.863	-0.877	-0.946	-0.938	-0.833	-0.760	-0.751	-0.859
0	RUN:SEC														
0	7212														
0	0.653	3553.3	2685.0	797.5	6.136	82.6	0.003113	0.053	0	1103	-0.702	-0.634	-0.531	-0.417	-0.335
-	-0.855	-0.729	-0.715	-0.615	-0.456	-0.409	-0.337	-0.287	-0.891	-0.735	-0.924	-0.820	-0.738	-0.735	-0.846
-	-0.278	-0.242	-0.952	-0.859	-0.804	-0.808	-0.802	-0.851	-0.878	-0.931	-0.924	-0.820	-0.738	-0.735	-0.846
0	1751-560 PM-1 IN-22 7311 10-JAN 8317:43 PAGE 13														
0	RUN:SEC														
0	7211														
0	0.651	4177.5	3366.6	765.3	85.9	85.9	0.003902	0.096	0	1108	-0.739	-0.673	-0.558	-0.441	-0.359
-	-0.849	-0.757	-0.748	-0.643	-0.513	-0.427	-0.353	-0.305	-0.871	-0.774	-1.446	-1.363	-0.277	-0.264	-1.367
-	-0.392	-0.265	-0.967	-0.854	-0.825	-0.844	-0.849	-0.889	-0.928	-1.301	-1.446	-1.363	-0.277	-0.264	-1.367
0	RUN:SEC														
0	7212														
0	0.652	4177.1	3365.1	761.9	87.9	87.9	0.003885	0.046	0	1111	-0.721	-0.656	-0.552	-0.437	-0.350
-	-0.872	-0.741	-0.729	-0.623	-0.500	-0.407	-0.342	-0.293	-0.897	-0.744	-1.397	-1.317	-0.268	-0.256	-1.326
-	-0.222	-0.258	-0.953	-0.874	-0.825	-0.839	-0.821	-0.874	-0.892	-1.322	-1.374	-1.397	-0.268	-0.256	-1.326
0	1751-560 PM-1 IN-22 1001 10-JAN 8317:43 PAGE 14														
0	RUN:SEC														
0	10011														
0	0.653	2521.1	2193.9	654.8	5.060	80.9	0.002566	0.056	2	1444	-0.696	-0.601	-0.490	-0.384	-0.315
-	-0.824	-0.657	-0.689	-0.577	-0.470	-0.375	-0.313	-0.265	-0.885	-0.711	-0.696	-0.601	-0.490	-0.384	-0.315
-	-0.252	-0.228	-0.922	-0.838	-0.746	-0.774	-0.799	-0.851	-0.865	-0.214	-0.997	-0.218	-0.218	-0.218	-0.227
0	RUN:SEC														
0	10012														
0	0.652	2522.5	2197.2	652.9	5.052	81.1	0.002569	0.051	2	1445	-0.699	-0.612	-0.497	-0.391	-0.318
-	-0.835	-0.701	-0.701	-0.604	-0.480	-0.395	-0.316	-0.266	-0.890	-0.728	-0.699	-0.612	-0.497	-0.391	-0.318
-	-0.264	-0.233	-0.926	-0.825	-0.794	-0.746	-0.802	-0.852	-0.879	-0.220	-0.917	-0.226	-0.224	-0.219	-0.231

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0	0.750	2126.0	1464.5	576.0	4.027	70.4	0.001764	0.033	100	1113	-0.203	-0.202	-0.232	-0.131	-0.126
	-0.522	-0.374	-0.261	-0.212	-0.186	-0.159	-0.129	-0.116	-0.099	-0.607	-0.309	-0.126	-0.109	-0.122	-0.124
	-0.124	-0.102	-0.804	-0.742	-0.677	-0.602	-0.670	-0.720	-0.763	-0.114	-0.103	-0.145	-0.116	-0.113	
	-0.351	-0.238	-0.168	-0.135	-0.123	-0.301	-0.245	-0.169	-0.132	-0.120	-0.368	-0.218	-0.145	-0.113	
0	MUNISEC														
	0.751	2122.9	1461.3	576.7	4.036	77.5	0.001764	0.028	100	1117	-0.297	-0.210	-0.241	-0.138	-0.133
	-0.574	-0.381	-0.269	-0.216	-0.192	-0.163	-0.139	-0.129	-0.112	-0.615	-0.402	-0.112	-0.103	-0.115	-0.117
	-0.130	-0.108	-0.805	-0.744	-0.669	-0.673	-0.661	-0.722	-0.733	-0.100	-0.086	-0.140	-0.161	-0.132	
	-0.351	-0.228	-0.157	-0.128	-0.121	-0.302	-0.238	-0.161	-0.127	-0.112	-0.366	-0.240	-0.161	-0.122	
0	MUNISEC														
	0.752	2136.2	1543.2	770.9	5230	81.1	0.002332	0.023	100	1120	-0.319	-0.224	-0.233	-0.151	-0.138
	-0.551	-0.405	-0.283	-0.226	-0.200	-0.175	-0.151	-0.143	-0.124	-0.643	-0.427	-0.132	-0.131	-0.134	-0.139
	-0.134	-0.113	-0.815	-0.763	-0.703	-0.691	-0.673	-0.742	-0.769	-0.130	-0.119	-0.132	-0.131	-0.142	-0.129
	-0.371	-0.247	-0.181	-0.153	-0.130	-0.427	-0.277	-0.194	-0.146	-0.131	-0.410	-0.266	-0.181	-0.142	-0.129
0	MUNISEC														
	0.752	2136.0	1549.2	771.4	5237	82.6	0.002331	0.026	100	1124	-0.316	-0.225	-0.238	-0.152	-0.138
	-0.557	-0.403	-0.277	-0.221	-0.192	-0.170	-0.152	-0.143	-0.123	-0.631	-0.419	-0.123	-0.112	-0.120	-0.134
	-0.134	-0.112	-0.829	-0.771	-0.707	-0.697	-0.690	-0.731	-0.768	-0.120	-0.107	-0.126	-0.131	-0.139	-0.125
	-0.380	-0.252	-0.176	-0.144	-0.134	-0.413	-0.269	-0.178	-0.138	-0.126	-0.421	-0.276	-0.183	-0.139	-0.125
	10 JAN 83/17:56														
0	MUNISEC														
	0.751	3710.9	2552.5	6.081	97.0	0.003023	0.018	100	1124	-0.344	-0.237	-0.264	-0.160	-0.147	
	-0.561	-0.418	-0.297	-0.245	-0.222	-0.194	-0.156	-0.137	-0.066	-0.666	-0.449	-0.144	-0.136	-0.140	-0.145
	-0.141	-0.119	-0.842	-0.787	-0.719	-0.722	-0.706	-0.775	-0.775	-0.136	-0.123	-0.144	-0.136	-0.140	-0.145
	-0.407	-0.270	-0.191	-0.158	-0.156	-0.438	-0.293	-0.202	-0.159	-0.147	-0.453	-0.297	-0.204	-0.161	-0.145
0	MUNISEC														
	0.752	2112.9	2227.5	9.878	87.0	0.003028	0.015	100	1131	-0.346	-0.231	-0.276	-0.171	-0.138	
	-0.567	-0.423	-0.300	-0.248	-0.221	-0.194	-0.161	-0.156	-0.130	-0.675	-0.454	-0.143	-0.135	-0.142	-0.147
	-0.153	-0.130	-0.844	-0.797	-0.732	-0.728	-0.704	-0.772	-0.786	-0.135	-0.124	-0.143	-0.135	-0.142	-0.147
	-0.415	-0.270	-0.186	-0.154	-0.155	-0.452	-0.306	-0.210	-0.166	-0.148	-0.451	-0.302	-0.208	-0.165	-0.150
0	MUNISEC														
	0.859	2116.3	1306.7	675.4	4.305	76.9	0.001629	0.014	100	1240	-0.114	-0.093	-0.169	-0.071	-0.074
	-0.215	-0.169	-0.125	-0.100	-0.089	-0.078	-0.056	-0.041	-0.042	-0.269	-0.139	-0.114	-0.093	-0.065	-0.062
	-0.419	-0.256	-0.471	-0.412	-0.358	-0.417	-0.427	-0.431	-0.467	-0.049	-0.054	-0.054	-0.049	-0.052	-0.062

0 -0.101 -0.021 -0.070 -0.060 -0.060 -0.100 -0.077 -0.072 -0.070 -0.060 -0.115 -0.083 -0.075 -0.078 -0.076

RUN:SF0

87:2
0 0.952 2121.0 1320.0 670.4 4.281 70.5 0.001637 0.013 100 1245
-0.201 -0.155 -0.115 -0.091 -0.080 -0.069 -0.051 -0.047 -0.040 -0.258 -0.131 -0.107 -0.077 -0.153 -0.097 -0.080
-0.065 -0.047 -0.039 -0.032 -0.028 -0.025 -0.022 -0.020 -0.018 -0.055 -0.044 -0.036 -0.030 -0.038 -0.039
-0.105 -0.085 -0.076 -0.073 -0.066 -0.103 -0.075 -0.070 -0.067 -0.065 -0.101 -0.070 -0.065 -0.070 -0.069
1157-560 P1-17-22 87:2 10-PRESSOUT3 10 JAN 03217:56 PAGE 6

RUN:SF0

87:3
0 0.949 2121.0 1320.0 668.2 4.274 70.7 0.001639 0.010 100 1245
-0.222 -0.172 -0.126 -0.109 -0.094 -0.083 -0.054 -0.041 -0.043 -0.260 -0.135 -0.111 -0.079 -0.153 -0.099 -0.083
-0.068 -0.044 -0.042 -0.043 -0.037 -0.034 -0.022 -0.023 -0.027 -0.058 -0.049 -0.064 -0.059 -0.053 -0.066 -0.077
-0.113 -0.093 -0.082 -0.081 -0.068 -0.106 -0.078 -0.073 -0.070 -0.069 -0.106 -0.073 -0.066 -0.071 -0.069

RUN:SF0

88:1
0 0.954 2030.5 1437.6 836.6 5.220 67.4 0.001999 0.012 100 1255
-0.215 -0.170 -0.123 -0.099 -0.089 -0.078 -0.049 -0.076 -0.056 -0.284 -0.152 -0.127 -0.099 -0.166 -0.070 -0.068
-0.073 -0.049 -0.070 -0.056 -0.031 -0.039 -0.046 -0.039 -0.033 -0.062 -0.054 -0.064 -0.058 -0.053 -0.066 -0.078
-0.116 -0.092 -0.081 -0.080 -0.068 -0.120 -0.087 -0.076 -0.073 -0.072 -0.117 -0.083 -0.076 -0.076 -0.075

RUN:SF0

88:2
0 0.951 3170.0 1979.3 6.302 85.9 0.002421 0.013 100 1305
-0.212 -0.172 -0.129 -0.100 -0.085 -0.075 -0.075 -0.082 -0.063 -0.294 -0.157 -0.132 -0.099 -0.182 -0.077 -0.075
-0.079 -0.054 -0.070 -0.049 -0.026 -0.049 -0.046 -0.039 -0.076 -0.059 -0.050 -0.059 -0.054 -0.051 -0.066 -0.078
-0.117 -0.091 -0.080 -0.079 -0.077 -0.124 -0.069 -0.077 -0.074 -0.074 -0.117 -0.083 -0.076 -0.075 -0.073

RUN:SF0

89:1
0 0.948 3157.7 1971.7 6.277 89.4 0.002425 0.008 100 1310
-0.235 -0.187 -0.142 -0.112 -0.101 -0.091 -0.073 -0.080 -0.061 -0.289 -0.153 -0.131 -0.097 -0.178 -0.074 -0.071
-0.075 -0.051 -0.070 -0.056 -0.029 -0.038 -0.044 -0.036 -0.076 -0.061 -0.054 -0.063 -0.057 -0.054 -0.070 -0.082
-0.170 -0.093 -0.082 -0.084 -0.080 -0.126 -0.092 -0.080 -0.079 -0.077 -0.128 -0.090 -0.082 -0.078 -0.077

LINE COUNT = 153

0	RUN:SEC									
0	10013	2422.3	2154.1	655.3	5.047	82.3	0.002561	0.054	2	1449
0	0.652	-0.707	-0.699	-0.558	-0.470	-0.387	-0.318	-0.274	-0.243	-0.905
0	-0.833	-0.707	-0.699	-0.558	-0.470	-0.387	-0.318	-0.274	-0.243	-0.905
0	-0.214	-0.241	-0.241	-0.241	-0.241	-0.241	-0.241	-0.241	-0.241	-0.241
0	RUN:SEC									
0	10014	2522.3	2174.8	655.4	5.035	83.3	0.002556	0.048	2	1454
0	0.653	-0.705	-0.703	-0.607	-0.461	-0.393	-0.321	-0.274	-0.239	-0.900
0	-0.835	-0.705	-0.703	-0.607	-0.461	-0.393	-0.321	-0.274	-0.239	-0.900
0	-0.274	-0.237	-0.234	-0.234	-0.234	-0.234	-0.234	-0.234	-0.234	-0.234
0	1157-560 PM-1 1A-22 10015 ID-PRESSOUT3 10 JAN 93017143 PAGE 15									
0	RUN:SEC									
0	10015	2521.7	2172.8	655.8	5.023	86.4	0.002549	0.053	2	1459
0	0.654	-0.703	-0.699	-0.600	-0.477	-0.386	-0.320	-0.276	-0.243	-0.893
0	-0.829	-0.703	-0.699	-0.600	-0.477	-0.386	-0.320	-0.276	-0.243	-0.893
0	-0.270	-0.236	-0.235	-0.235	-0.235	-0.235	-0.235	-0.235	-0.235	-0.235
0	RUN:SEC									
0	10016	2521.6	2191.2	657.0	5.316	85.3	0.002544	0.053	2	1504
0	0.654	-0.712	-0.702	-0.605	-0.484	-0.392	-0.319	-0.273	-0.241	-0.894
0	-0.840	-0.712	-0.702	-0.605	-0.484	-0.392	-0.319	-0.273	-0.241	-0.894
0	-0.261	-0.232	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231	-0.231
0	RUN:SEC									
0	10017	2521.4	2192.3	655.9	5.036	85.3	0.002554	0.054	2	1509
0	0.654	-0.701	-0.699	-0.593	-0.469	-0.392	-0.317	-0.270	-0.237	-0.890
0	-0.823	-0.701	-0.699	-0.593	-0.469	-0.392	-0.317	-0.270	-0.237	-0.890
0	-0.262	-0.229	-0.229	-0.229	-0.229	-0.229	-0.229	-0.229	-0.229	-0.229
0	RUN:SEC									
0	10018	2521.1	2154.5	654.0	5.014	84.5	0.002550	0.051	2	1515
0	0.652	-0.701	-0.701	-0.596	-0.475	-0.386	-0.306	-0.259	-0.220	-0.880
0	-0.831	-0.701	-0.701	-0.596	-0.475	-0.386	-0.306	-0.259	-0.220	-0.880
0	-0.272	-0.229	-0.229	-0.229	-0.229	-0.229	-0.229	-0.229	-0.229	-0.229
0	1157-560 PM-1 1A-22 10019 ID-PRESSOUT3 10 JAN 93017143 PAGE 16									
0	RUN:SEC									
0	10019	2521.4	2155.4	653.6	5.007	85.0	0.002543	0.050	2	1520
0	0.652	-0.707	-0.702	-0.605	-0.481	-0.390	-0.321	-0.275	-0.243	-0.904
0	-0.837	-0.707	-0.702	-0.605	-0.481	-0.390	-0.321	-0.275	-0.243	-0.904
0	-0.265	-0.233	-0.233	-0.233	-0.233	-0.233	-0.233	-0.233	-0.233	-0.233
0	RUN:SEC									
0	10020	2521.4	2155.4	653.6	5.007	85.0	0.002543	0.050	2	1520
0	0.652	-0.707	-0.702	-0.605	-0.481	-0.390	-0.321	-0.275	-0.243	-0.904
0	-0.837	-0.707	-0.702	-0.605	-0.481	-0.390	-0.321	-0.275	-0.243	-0.904
0	-0.265	-0.233	-0.233	-0.233	-0.233	-0.233	-0.233	-0.233	-0.233	-0.233

0	0.652	2.22.3	215.9	653.5	4.993	86.4	0.002543	0.048	2	1525	-0.892	-0.236	-0.699	-0.619	-0.508	-0.401	-0.329
-	-0.340	-0.708	-0.707	-0.608	-0.486	-0.1	-0.316	-0.269	-0.236	-0.210	-0.191	-0.216	-0.214	-0.210	-0.222	-0.222	-0.227
-	-0.278	-0.754	-0.508	-0.839	-0.782	-0.1	-0.801	-0.845	-0.856	-0.820	-0.819	-0.826	-0.824	-0.826	-0.826	-0.826	-0.827
0	NUM:SEC																
0	10212.0																
0	0.652	3036.6	504.6	7.000	80.6	0.003553	0.042	1	1004	-0.911	-0.240	-0.741	-0.717	-0.644	-0.530	-0.421	-0.342
-	-0.659	-0.745	-0.738	-0.635	-0.506	-0.414	-0.335	-0.291	-0.240	-0.244	-0.230	-0.242	-0.245	-0.232	-0.236	-0.243	-0.245
-	-0.236	-0.450	-0.969	-0.867	-0.830	-0.797	-0.801	-0.801	-0.811	-0.824	-0.820	-0.822	-0.822	-0.822	-0.822	-0.822	-0.822
0	NUM:SEC																
0	10212.0																
0	0.646	3050.1	495.7	6.945	82.2	0.003557	0.046	1	1006	-0.920	-0.240	-0.751	-0.722	-0.644	-0.529	-0.416	-0.345
-	-0.659	-0.707	-0.720	-0.621	-0.498	-0.408	-0.344	-0.292	-0.240	-0.232	-0.209	-0.238	-0.237	-0.238	-0.231	-0.231	-0.244
-	-0.238	-0.252	-0.532	-0.867	-0.914	-0.824	-0.830	-0.871	-0.885	-0.885	-0.885	-0.885	-0.885	-0.885	-0.885	-0.885	-0.885
0	10213.0																
0	NUM:SEC																
0	10213.0																
0	0.646	3050.1	500.0	6.941	82.7	0.003557	0.039	1	1007	-0.922	-0.240	-0.755	-0.739	-0.654	-0.541	-0.429	-0.356
-	-0.657	-0.724	-0.734	-0.623	-0.508	-0.414	-0.346	-0.296	-0.246	-0.237	-0.221	-0.246	-0.244	-0.244	-0.244	-0.244	-0.245
-	-0.230	-0.264	-0.954	-0.865	-0.825	-0.808	-0.820	-0.878	-0.884	-0.884	-0.884	-0.884	-0.884	-0.884	-0.884	-0.884	-0.884
0	NUM:SEC																
0	10214.0																
0	0.654	3028.5	502.0	6.933	84.0	0.003517	0.044	1	1008	-0.928	-0.246	-0.761	-0.734	-0.633	-0.542	-0.430	-0.353
-	-0.663	-0.718	-0.732	-0.633	-0.508	-0.421	-0.350	-0.301	-0.246	-0.237	-0.221	-0.246	-0.244	-0.249	-0.238	-0.238	-0.253
-	-0.227	-0.429	-0.923	-0.872	-0.821	-0.801	-0.829	-0.884	-0.889	-0.889	-0.889	-0.889	-0.889	-0.889	-0.889	-0.889	-0.889
0	NUM:SEC																
0	10215.0																
0	0.654	3039.1	509.1	6.923	86.7	0.003518	0.039	1	1011	-0.934	-0.271	-0.766	-0.741	-0.649	-0.536	-0.422	-0.346
-	-0.659	-0.723	-0.734	-0.638	-0.513	-0.422	-0.356	-0.305	-0.241	-0.225	-0.225	-0.246	-0.247	-0.247	-0.247	-0.247	-0.260
-	-0.241	-0.429	-0.923	-0.875	-0.823	-0.808	-0.837	-0.889	-0.889	-0.889	-0.889	-0.889	-0.889	-0.889	-0.889	-0.889	-0.889
0	NUM:SEC																
0	10216.0																
0	0.655	3043.9	510.2	6.918	87.0	0.003508	0.018	1	1012	-0.915	-0.244	-0.673	-0.651	-0.573	-0.475	-0.383	-0.321
-	-0.664	-0.639	-0.658	-0.558	-0.461	-0.383	-0.319	-0.276	-0.244	-0.222	-0.222	-0.223	-0.225	-0.225	-0.225	-0.225	-0.235
-	-0.274	-0.242	-0.834	-0.762	-0.717	-0.711	-0.732	-0.770	-0.784	-0.784	-0.784	-0.784	-0.784	-0.784	-0.784	-0.784	-0.784
0	10217.0																
0	NUM:SEC																
0	10217.0																
0	0.653	3036.1	504.6	6.879	87.8	0.003501	0.018	1	1013	-0.905	-0.244	-0.661	-0.642	-0.572	-0.479	-0.385	-0.326
-	-0.671	-0.643	-0.651	-0.568	-0.460	-0.379	-0.317	-0.274	-0.244	-0.228	-0.228	-0.232	-0.233	-0.233	-0.233	-0.233	-0.237
-	-0.278	-0.254	-0.843	-0.745	-0.725	-0.720	-0.739	-0.782	-0.793	-0.793	-0.793	-0.793	-0.793	-0.793	-0.793	-0.793	-0.793

[illegible]

0	0.652	4044.9	3040.0	904.6	6.963	89.3	0.003501	0.043	1	1022	-0.726	-0.762	-0.917	-0.238	-0.242	-0.243	-0.243	-0.238	-0.231
-	0.413	-0.714	-0.729	-0.628	-0.508	-0.418	-0.348	-0.294	-0.260	-0.917	-0.762	-0.917	-0.238	-0.222	-0.242	-0.243	-0.241	-0.238	-0.231
-	0.294	-0.255	-0.946	-0.866	-0.811	-0.809	-0.830	-0.867	-0.890	-0.238	-0.222	-0.242	-0.238	-0.222	-0.242	-0.243	-0.241	-0.238	-0.231
0	RUN:SEC																		
0	102:16																		
0	0.651	4044.8	3041.9	903.0	6.856	89.4	0.003503	0.042	1	1023	-0.716	-0.748	-0.911	-0.236	-0.243	-0.243	-0.241	-0.235	-0.251
-	0.459	-0.713	-0.721	-0.621	-0.501	-0.405	-0.338	-0.290	-0.256	-0.911	-0.748	-0.911	-0.236	-0.222	-0.243	-0.243	-0.241	-0.235	-0.251
-	0.293	-0.256	-0.946	-0.866	-0.811	-0.809	-0.830	-0.867	-0.890	-0.236	-0.222	-0.242	-0.236	-0.222	-0.242	-0.243	-0.241	-0.235	-0.251
0	RUN:SEC																		
0	102:17																		
0	0.651	4044.7	3041.7	903.1	6.851	89.7	0.003500	0.044	1	1023	-0.720	-0.763	-0.918	-0.236	-0.243	-0.243	-0.241	-0.235	-0.253
-	0.459	-0.717	-0.728	-0.622	-0.501	-0.413	-0.341	-0.293	-0.256	-0.918	-0.763	-0.918	-0.236	-0.222	-0.243	-0.243	-0.241	-0.235	-0.253
-	0.297	-0.257	-0.946	-0.866	-0.813	-0.803	-0.823	-0.870	-0.880	-0.232	-0.243	-0.243	-0.239	-0.222	-0.243	-0.243	-0.241	-0.239	-0.253
0	RUN:SEC																		
0	102:18																		
0	0.650	4044.7	3042.3	901.9	6.847	89.8	0.003503	0.039	1	1024	-0.727	-0.757	-0.923	-0.236	-0.239	-0.239	-0.239	-0.239	-0.251
-	0.470	-0.722	-0.734	-0.635	-0.506	-0.419	-0.348	-0.299	-0.266	-0.923	-0.757	-0.923	-0.236	-0.239	-0.239	-0.239	-0.239	-0.239	-0.251
-	0.254	-0.256	-0.953	-0.878	-0.821	-0.803	-0.838	-0.877	-0.885	-0.231	-0.211	-0.239	-0.236	-0.239	-0.239	-0.239	-0.239	-0.239	-0.251
0	1157:50 PJ-1 1A-22 102:19 10-PRESSCUT3 10 JAN 83 17:43 PAGE 21																		
0	RUN:SEC																		
0	102:19																		
0	0.652	4044.7	3038.2	905.8	6.855	90.0	0.003455	0.045	1	1024	-0.708	-0.745	-0.898	-0.238	-0.222	-0.243	-0.243	-0.235	-0.244
-	0.457	-0.715	-0.728	-0.627	-0.503	-0.413	-0.334	-0.285	-0.250	-0.898	-0.745	-0.898	-0.238	-0.222	-0.243	-0.243	-0.243	-0.235	-0.244
-	0.298	-0.255	-0.939	-0.825	-0.804	-0.789	-0.819	-0.863	-0.889	-0.238	-0.222	-0.243	-0.238	-0.222	-0.243	-0.243	-0.243	-0.235	-0.244
0	RUN:SEC																		
0	102:20																		
0	0.652	4043.3	3028.5	904.5	6.846	90.2	0.003494	0.078	1	1025	-0.719	-0.753	-0.913	-0.240	-0.224	-0.248	-0.243	-0.231	-0.244
-	0.451	-0.716	-0.727	-0.631	-0.504	-0.416	-0.350	-0.249	-0.264	-0.913	-0.753	-0.913	-0.240	-0.224	-0.248	-0.248	-0.243	-0.231	-0.244
-	0.294	-0.257	-0.938	-0.855	-0.818	-0.810	-0.833	-0.871	-0.882	-0.240	-0.224	-0.248	-0.240	-0.224	-0.248	-0.248	-0.243	-0.231	-0.244
0	RUN:SEC																		
0	102:21																		
0	0.645	4051.0	3052.5	900.3	6.903	86.3	0.003533	0.041	1	1228	-0.728	-0.739	-0.920	-0.239	-0.225	-0.246	-0.243	-0.240	-0.247
-	0.424	-0.737	-0.728	-0.635	-0.510	-0.421	-0.339	-0.288	-0.253	-0.920	-0.739	-0.920	-0.239	-0.225	-0.246	-0.244	-0.243	-0.240	-0.247
-	0.288	-0.250	-0.942	-0.815	-0.829	-0.801	-0.829	-0.877	-0.917	-0.239	-0.225	-0.246	-0.239	-0.225	-0.246	-0.244	-0.243	-0.240	-0.247
0	RUN:SEC																		
0	102:22																		
0	0.652	4054.4	3048.3	905.8	6.915	86.8	0.003526	0.039	1	1229	-0.721	-0.737	-0.911	-0.232	-0.217	-0.239	-0.237	-0.232	-0.244
-	0.420	-0.732	-0.726	-0.626	-0.500	-0.407	-0.325	-0.282	-0.248	-0.911	-0.737	-0.911	-0.232	-0.217	-0.239	-0.237	-0.232	-0.232	-0.244
-	0.281	-0.252	-0.931	-0.858	-0.811	-0.811	-0.813	-0.864	-0.884	-0.232	-0.217	-0.239	-0.232	-0.217	-0.239	-0.237	-0.232	-0.232	-0.244

3753-560 PH-1 TA-22 10303	10-PRESSOUT3	10 JAN 03017:43	PAGE 22
0 RUN:SEC			
10322			
0 0.651 4046.1 3042.2 903.8 6.894 87.2 0.003517 0.040			1 1230
-0.914 -0.730 -0.722 -0.628 -0.506 -0.418 -0.343 -0.259 -0.923 -0.752 -0.731 -0.647 -0.533 -0.425 -0.351			
-0.267 -0.255 -0.557 -0.858 -0.814 -0.802 -0.621 -0.870 -0.829 -0.229 -0.216 -0.237 -0.236 -0.234 -0.241			
0 RUN:SEC			
10324			
0 0.652 4035.3 3032.3 922.8 5.876 87.9 0.003502 0.041			1 1230
-0.911 -0.725 -0.710 -0.615 -0.489 -0.402 -0.344 -0.292 -0.929 -0.744 -0.734 -0.638 -0.521 -0.485 -0.332			
-0.280 -0.247 -0.949 -0.871 -0.820 -0.807 -0.627 -0.877 -0.878 -0.224 -0.211 -0.232 -0.230 -0.229 -0.248			
0 RUN:SEC			
10325			
0 0.652 4039.3 3036.0 902.3 6.864 88.3 0.003503 0.035			1 1231
-0.911 -0.725 -0.710 -0.627 -0.501 -0.412 -0.337 -0.283 -0.928 -0.741 -0.705 -0.641 -0.523 -0.412 -0.341			
-0.287 -0.259 -0.949 -0.872 -0.815 -0.796 -0.639 -0.874 -0.883 -0.221 -0.207 -0.226 -0.224 -0.229 -0.239			
0 RUN:SEC			
10326			
0 0.650 4045.7 3049.1 901.3 6.866 88.7 0.003514 0.041			1 1232
-0.923 -0.736 -0.717 -0.631 -0.509 -0.415 -0.344 -0.294 -0.921 -0.755 -0.724 -0.633 -0.510 -0.402 -0.332			
-0.275 -0.244 -0.959 -0.879 -0.824 -0.822 -0.637 -0.885 -0.887 -0.236 -0.223 -0.242 -0.240 -0.234 -0.245			
3757-560 PH-1 TA-22 10405	10-PRESSOUT5	10 JAN 03017:43	PAGE 23
0 RUN:SEC			
10412			
0 0.653 4032.4 3021.1 904.5 6.559 82.8 0.003534 0.041			11 1412
-0.927 -0.744 -0.736 -0.624 -0.503 -0.418 -0.348 -0.298 -0.924 -0.767 -0.730 -0.650 -0.536 -0.419 -0.343			
-0.287 -0.250 -0.944 -0.877 -0.824 -0.791 -0.625 -0.871 -0.912 -0.245 -0.239 -0.245 -0.243 -0.239 -0.251			
0 RUN:SEC			
10413			
0 0.651 4044.5 3042.8 902.1 6.925 84.8 0.003532 0.050			12 1526
-0.939 -0.725 -0.724 -0.615 -0.494 -0.401 -0.336 -0.286 -0.925 -0.736 -0.721 -0.636 -0.518 -0.411 -0.336			
-0.283 -0.247 -0.947 -0.871 -0.818 -0.786 -0.623 -0.876 -0.899 -0.224 -0.209 -0.229 -0.224 -0.226 -0.237			
0 RUN:SEC			
10711			
0 0.652 4054.8 3047.0 907.1 6.980 83.2 0.003549 0.047			13 1038
-0.906 -0.744 -0.730 -0.639 -0.513 -0.426 -0.354 -0.303 -0.928 -0.761 -0.738 -0.656 -0.543 -0.424 -0.340			
-0.245 -0.259 -0.952 -0.876 -0.821 -0.792 -0.620 -0.869 -0.902 -0.239 -0.226 -0.240 -0.238 -0.240 -0.248			
0 RUN:SEC			
10911			

0	0.05	4006.5	2023.9	910.7	6.255	85.1	0.00324	0.039	2	1234	-0.927	-0.742	-0.729	-0.651	-0.537	-0.425	-0.348
	-0.094	-0.741	-0.737	-0.621	-0.458	-0.408	-0.346	-0.297	-0.260	-0.233	-0.221	-0.233	-0.242	-0.241	-0.233	-0.233	-0.244
	-0.251	-0.222	-0.557	-0.871	-0.821	-0.795	-0.831	-0.873	-0.904	-0.904	-0.904	-0.904	-0.904	-0.904	-0.904	-0.904	-0.904
1757-560	PT-1	1A-22	10032	10-PRESSOUT3	10 JAN 83	17:43											
0	RUA:SEC																
0	10812	4000.4	2032.8	904.4	6.872	88.9	0.003497	0.046	2	1238	-0.928	-0.759	-0.729	-0.635	-0.525	-0.410	-0.333
	-0.065	-0.728	-0.724	-0.623	-0.496	-0.405	-0.343	-0.292	-0.258	-0.238	-0.221	-0.238	-0.244	-0.241	-0.231	-0.245	
	-0.275	-0.251	-0.554	-0.871	-0.824	-0.811	-0.841	-0.885	-0.894	-0.894	-0.894	-0.894	-0.894	-0.894	-0.894	-0.894	-0.894
0	RUA:SEC																
0	10812	4042.0	3035.7	905.6	6.857	89.7	0.003495	0.042	2	1239	-0.918	-0.741	-0.724	-0.638	-0.519	-0.428	-0.348
	-0.064	-0.726	-0.722	-0.620	-0.494	-0.404	-0.338	-0.293	-0.259	-0.242	-0.225	-0.244	-0.244	-0.244	-0.244	-0.244	-0.255
	-0.279	-0.252	-0.562	-0.889	-0.824	-0.812	-0.837	-0.879	-0.898	-0.898	-0.898	-0.898	-0.898	-0.898	-0.898	-0.898	-0.898
0	RUA:SEC																
0	10814	4041.9	3032.1	900.4	6.853	90.5	0.003486	0.048	2	1240	-0.917	-0.740	-0.716	-0.641	-0.524	-0.410	-0.334
	-0.077	-0.736	-0.735	-0.639	-0.513	-0.419	-0.339	-0.293	-0.259	-0.241	-0.224	-0.244	-0.244	-0.244	-0.246	-0.227	-0.244
	-0.279	-0.242	-0.557	-0.874	-0.824	-0.810	-0.837	-0.879	-0.908	-0.908	-0.908	-0.908	-0.908	-0.908	-0.908	-0.908	-0.908
0	RUA:SEC																
0	10815	4043.5	3031.6	910.0	6.842	91.7	0.003479	0.044	2	1241	-0.916	-0.737	-0.719	-0.653	-0.539	-0.423	-0.341
	-0.063	-0.729	-0.725	-0.625	-0.500	-0.405	-0.341	-0.291	-0.258	-0.236	-0.215	-0.237	-0.237	-0.240	-0.238	-0.240	-0.240
	-0.287	-0.251	-0.564	-0.882	-0.825	-0.792	-0.831	-0.881	-0.881	-0.881	-0.881	-0.881	-0.881	-0.881	-0.881	-0.881	-0.881
1757-560	PT-1	1A-22	10931	10-PRESSOUT3	10 JAN 83	17:43											
0	RUA:SEC																
0	10521	2412.2	2179.4	658.6	5.082	79.5	0.002559	0.043	8	1401	-0.760	-0.705	-0.705	-0.601	-0.488	-0.390	-0.343
	-0.084	-0.249	-0.249	-0.626	-0.505	-0.409	-0.304	-0.253	-0.222	-0.203	-0.199	-0.243	-0.243	-0.243	-0.243	-0.243	-0.243
	-0.250	-0.249	-0.249	-0.249	-0.249	-0.249	-0.249	-0.249	-0.249	-0.249	-0.249	-0.249	-0.249	-0.249	-0.249	-0.249	-0.249
0	RUA:SEC																
0	10512	2411.1	2212.2	656.3	5.078	81.4	0.002584	0.049	6	1409	-0.746	-0.702	-0.702	-0.596	-0.478	-0.374	-0.332
	-0.087	-0.243	-0.243	-0.617	-0.454	-0.397	-0.298	-0.245	-0.214	-0.188	-0.178	-0.221	-0.220	-0.224	-0.202	-0.202	-0.206
	-0.249	-0.243	-0.243	-0.243	-0.243	-0.243	-0.243	-0.243	-0.243	-0.243	-0.243	-0.243	-0.243	-0.243	-0.243	-0.243	-0.243
0	RUA:SEC																
0	10513	2534.5	2205.5	656.8	5.059	82.7	0.002571	0.049	8	1411	-0.752	-0.702	-0.702	-0.589	-0.478	-0.371	-0.332
	-0.081	-0.249	-0.249	-0.617	-0.451	-0.397	-0.298	-0.243	-0.213	-0.195	-0.189	-0.221	-0.220	-0.224	-0.202	-0.202	-0.205
	-0.278	-0.249	-0.249	-0.249	-0.249	-0.249	-0.249	-0.249	-0.249	-0.249	-0.249	-0.249	-0.249	-0.249	-0.249	-0.249	-0.249

0	RUMASEG	10214	2921.0	2191.2	656.4	5.033	83.6	0.002551	0.043	0	1413	-0.757	-0.701	-0.539	-0.478	-0.368	-0.374
0	0.054	2921.0	-0.670	-0.616	-0.492	-0.394	-0.305	-0.250	-0.219	0	-0.192	-0.182	-0.231	-0.232	-0.231	-0.203	-0.203
0	0.817	-0.225	-0.225	-0.225	-0.225	-0.225	-0.225	-0.225	-0.225	0	-0.192	-0.182	-0.231	-0.232	-0.231	-0.203	-0.203
0	0.272	-0.225	-0.225	-0.225	-0.225	-0.225	-0.225	-0.225	-0.225	0	-0.192	-0.182	-0.231	-0.232	-0.231	-0.203	-0.203
0	1751-540	FR-1	TA-22	10915	10-PRESSOUT3	10-PRESSOUT3	10-PRESSOUT3	10-PRESSOUT3	10-PRESSOUT3	0	-0.192	-0.182	-0.231	-0.232	-0.231	-0.203	-0.203
0	RUMASEG	10515	2924.3	2193.4	657.4	5.020	85.3	0.002546	0.051	0	1416	-0.750	-0.710	-0.538	-0.477	-0.373	-0.329
0	0.054	2924.3	-0.674	-0.617	-0.496	-0.399	-0.303	-0.249	-0.219	0	-0.196	-0.186	-0.227	-0.228	-0.224	-0.194	-0.197
0	0.820	-0.226	-0.226	-0.226	-0.226	-0.226	-0.226	-0.226	-0.226	0	-0.196	-0.186	-0.227	-0.228	-0.224	-0.194	-0.197
0	0.276	-0.226	-0.226	-0.226	-0.226	-0.226	-0.226	-0.226	-0.226	0	-0.196	-0.186	-0.227	-0.228	-0.224	-0.194	-0.197
0	RUMASEG	10516	2923.0	2192.0	657.0	5.012	85.0	0.002543	0.040	0	1417	-0.750	-0.703	-0.537	-0.470	-0.369	-0.327
0	0.054	2923.0	-0.666	-0.605	-0.478	-0.382	-0.287	-0.245	-0.214	0	-0.191	-0.178	-0.228	-0.231	-0.227	-0.197	-0.197
0	0.808	-0.227	-0.227	-0.227	-0.227	-0.227	-0.227	-0.227	-0.227	0	-0.191	-0.178	-0.228	-0.231	-0.227	-0.197	-0.197
0	0.277	-0.227	-0.227	-0.227	-0.227	-0.227	-0.227	-0.227	-0.227	0	-0.191	-0.178	-0.228	-0.231	-0.227	-0.197	-0.197
0	RUMASEG	10517	2921.7	2191.7	656.6	5.004	86.2	0.002540	0.045	0	1419	-0.751	-0.703	-0.538	-0.472	-0.365	-0.331
0	0.054	2921.7	-0.672	-0.621	-0.498	-0.403	-0.294	-0.243	-0.213	0	-0.186	-0.175	-0.230	-0.227	-0.200	-0.205	-0.205
0	0.822	-0.229	-0.229	-0.229	-0.229	-0.229	-0.229	-0.229	-0.229	0	-0.186	-0.175	-0.230	-0.227	-0.200	-0.205	-0.205
0	0.279	-0.229	-0.229	-0.229	-0.229	-0.229	-0.229	-0.229	-0.229	0	-0.186	-0.175	-0.230	-0.227	-0.200	-0.205	-0.205
0	RUMASEG	10518	2921.7	2190.5	657.6	5.003	86.6	0.002537	0.051	0	1420	-0.753	-0.710	-0.535	-0.480	-0.376	-0.334
0	0.055	2921.7	-0.667	-0.618	-0.501	-0.405	-0.301	-0.249	-0.220	0	-0.196	-0.182	-0.234	-0.233	-0.201	-0.203	-0.203
0	0.815	-0.229	-0.229	-0.229	-0.229	-0.229	-0.229	-0.229	-0.229	0	-0.196	-0.182	-0.234	-0.233	-0.201	-0.203	-0.203
0	0.282	-0.229	-0.229	-0.229	-0.229	-0.229	-0.229	-0.229	-0.229	0	-0.196	-0.182	-0.234	-0.233	-0.201	-0.203	-0.203
0	1751-540	FR-1	TA-22	10919	10-PRESSOUT3	10-PRESSOUT3	10-PRESSOUT3	10-PRESSOUT3	10-PRESSOUT3	0	-0.196	-0.182	-0.234	-0.233	-0.201	-0.203	-0.203
0	RUMASEG	10519	2923.7	2194.4	656.2	4.994	87.1	0.002530	0.048	0	1422	-0.765	-0.710	-0.537	-0.437	-0.378	-0.338
0	0.054	2923.7	-0.673	-0.619	-0.490	-0.396	-0.314	-0.250	-0.229	0	-0.196	-0.184	-0.235	-0.236	-0.204	-0.205	-0.205
0	0.815	-0.226	-0.226	-0.226	-0.226	-0.226	-0.226	-0.226	-0.226	0	-0.196	-0.184	-0.235	-0.236	-0.204	-0.205	-0.205
0	0.286	-0.226	-0.226	-0.226	-0.226	-0.226	-0.226	-0.226	-0.226	0	-0.196	-0.184	-0.235	-0.236	-0.204	-0.205	-0.205
0	RUMASEG	10520	2921.7	2190.7	657.4	4.988	87.0	0.002532	0.051	0	1425	-0.877	-0.742	-0.688	-0.585	-0.469	-0.376
0	0.055	2921.7	-0.664	-0.612	-0.491	-0.397	-0.290	-0.237	-0.206	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	0.810	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	0.274	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	RUMASEG	10521	2921.7	2190.7	657.4	4.988	87.0	0.002532	0.051	0	1425	-0.877	-0.742	-0.688	-0.585	-0.469	-0.376
0	0.055	2921.7	-0.664	-0.612	-0.491	-0.397	-0.290	-0.237	-0.206	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	0.810	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	0.274	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	RUMASEG	10522	2921.7	2190.7	657.4	4.988	87.0	0.002532	0.051	0	1425	-0.877	-0.742	-0.688	-0.585	-0.469	-0.376
0	0.055	2921.7	-0.664	-0.612	-0.491	-0.397	-0.290	-0.237	-0.206	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	0.810	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	0.274	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	RUMASEG	10523	2921.7	2190.7	657.4	4.988	87.0	0.002532	0.051	0	1425	-0.877	-0.742	-0.688	-0.585	-0.469	-0.376
0	0.055	2921.7	-0.664	-0.612	-0.491	-0.397	-0.290	-0.237	-0.206	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	0.810	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	0.274	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	RUMASEG	10524	2921.7	2190.7	657.4	4.988	87.0	0.002532	0.051	0	1425	-0.877	-0.742	-0.688	-0.585	-0.469	-0.376
0	0.055	2921.7	-0.664	-0.612	-0.491	-0.397	-0.290	-0.237	-0.206	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	0.810	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	0.274	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	RUMASEG	10525	2921.7	2190.7	657.4	4.988	87.0	0.002532	0.051	0	1425	-0.877	-0.742	-0.688	-0.585	-0.469	-0.376
0	0.055	2921.7	-0.664	-0.612	-0.491	-0.397	-0.290	-0.237	-0.206	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	0.810	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	0.274	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	RUMASEG	10526	2921.7	2190.7	657.4	4.988	87.0	0.002532	0.051	0	1425	-0.877	-0.742	-0.688	-0.585	-0.469	-0.376
0	0.055	2921.7	-0.664	-0.612	-0.491	-0.397	-0.290	-0.237	-0.206	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	0.810	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	0.274	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	RUMASEG	10527	2921.7	2190.7	657.4	4.988	87.0	0.002532	0.051	0	1425	-0.877	-0.742	-0.688	-0.585	-0.469	-0.376
0	0.055	2921.7	-0.664	-0.612	-0.491	-0.397	-0.290	-0.237	-0.206	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	0.810	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	0.274	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	RUMASEG	10528	2921.7	2190.7	657.4	4.988	87.0	0.002532	0.051	0	1425	-0.877	-0.742	-0.688	-0.585	-0.469	-0.376
0	0.055	2921.7	-0.664	-0.612	-0.491	-0.397	-0.290	-0.237	-0.206	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	0.810	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	0.274	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	RUMASEG	10529	2921.7	2190.7	657.4	4.988	87.0	0.002532	0.051	0	1425	-0.877	-0.742	-0.688	-0.585	-0.469	-0.376
0	0.055	2921.7	-0.664	-0.612	-0.491	-0.397	-0.290	-0.237	-0.206	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	0.810	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	0.274	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	RUMASEG	10530	2921.7	2190.7	657.4	4.988	87.0	0.002532	0.051	0	1425	-0.877	-0.742	-0.688	-0.585	-0.469	-0.376
0	0.055	2921.7	-0.664	-0.612	-0.491	-0.397	-0.290	-0.237	-0.206	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	0.810	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	0.274	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	-0.224	0	-0.187	-0.175	-0.224	-0.222	-0.207	-0.204	-0.204
0	RUMASEG																

0	0.654	2521.6	2191.4	494.7	4.978	88.4	0.002529	0.047	0	1427	-0.756	-0.701	-0.589	-0.475	-0.373	-0.334
	-0.817	-0.668	-0.614	-0.497	-0.397	-0.297	-0.244	-0.214		-0.193	-0.188	-0.234	-0.235	-0.234	-0.196	-0.200
	-0.280	-0.241	-0.874		-0.788	-0.808	-0.843	-0.832								
0	RUN:SEC															
	109:12															
0	0.654	2522.2	2193.0	496.1	4.992	87.1	0.002537	0.053	0	1431	-0.748	-0.704	-0.594	-0.470	-0.363	-0.328
	-0.808	-0.665	-0.605	-0.481	-0.388	-0.294	-0.243	-0.212		-0.191	-0.177	-0.223	-0.232	-0.232	-0.192	-0.194
	-0.280	-0.241	-0.874	-0.710	-0.762	-0.802	-0.836	-0.831								
1757-560 PM-1 1A-22	109:13															
0	RUN:SEC															
	109:13															
0	0.654	2521.5	2192.5	495.8	4.989	87.2	0.002536	0.049	0	1434	-0.743	-0.682	-0.591	-0.478	-0.375	-0.333
	-0.807	-0.663	-0.603	-0.488	-0.394	-0.286	-0.234	-0.205		-0.186	-0.174	-0.222	-0.223	-0.220	-0.192	-0.195
	-0.280	-0.233	-0.863	-0.779	-0.779	-0.810	-0.845	-0.814								
0	RUN:SEC															
	109:14															
0	0.652	2522.0	2195.6	493.8	4.974	88.0	0.002535	0.049	0	1436	-0.887	-0.750	-0.698	-0.577	-0.459	-0.316
	-0.809	-0.668	-0.615	-0.487	-0.389	-0.296	-0.245	-0.217		-0.186	-0.177	-0.221	-0.222	-0.224	-0.200	-0.199
	-0.245	-0.228	-0.883	-0.675	-0.764	-0.807	-0.842	-0.819								
0	RUN:SEC															
	109:15															
0	0.652	2521.6	2194.9	493.2	4.966	88.4	0.002539	0.053	0	1439	-0.886	-0.748	-0.709	-0.584	-0.467	-0.323
	-0.811	-0.666	-0.613	-0.491	-0.390	-0.288	-0.237	-0.208		-0.190	-0.180	-0.223	-0.223	-0.226	-0.192	-0.192
	-0.272	-0.232	-0.874	-0.676	-0.769	-0.819	-0.842	-0.821								
0	RUN:SEC															
	109:16															
0	0.651	2522.5	2199.2	491.4	4.957	88.8	0.002534	0.047	0	1441	-0.883	-0.732	-0.683	-0.579	-0.465	-0.318
	-0.809	-0.668	-0.603	-0.482	-0.392	-0.277	-0.229	-0.200		-0.186	-0.174	-0.224	-0.227	-0.225	-0.193	-0.197
	-0.268	-0.230	-0.862	-0.655	-0.788	-0.819	-0.854	-0.824								
1757-560 PM-1 1A-22	109:17															
0	RUN:SEC															
	109:17															
0	0.650	2521.0	2198.0	490.5	4.947	89.2	0.002532	0.047	0	1443	-0.886	-0.751	-0.705	-0.587	-0.472	-0.325
	-0.808	-0.670	-0.602	-0.484	-0.390	-0.291	-0.241	-0.213		-0.186	-0.182	-0.233	-0.231	-0.230	-0.195	-0.198
	-0.274	-0.233	-0.876	-0.678	-0.783	-0.810	-0.841	-0.811								
0	RUN:SEC															
	110:12															
0	0.645	4037.1	3041.6	513.3	7.024	81.9	0.003553	0.051	0	1442	-0.919	-0.757	-0.725	-0.641	-0.538	-0.340
	-0.881	-0.728	-0.744	-0.643	-0.522	-0.434	-0.355	-0.303		-0.233	-0.219	-0.238	-0.237	-0.237	-0.236	-0.245
	-0.262	-0.244	-0.518	-0.870	-0.816	-0.836	-0.880	-0.880								

[illegible]

0	0.654	4042.7	3052.3	508.9	6.914	86.9	0.003510	0.046	2	1115	-0.938	-0.775	-0.741	-0.650	-0.534	-0.426	-0.348
	-0.884	-0.725	-0.741	-0.636	-0.511	-0.419	-0.366	-0.310	-0.272	-0.230	-0.223	-0.244	-0.241	-0.244	-0.236	-0.243	-0.243
	-0.250	-0.224	-0.227	-0.877	-0.821	-0.812	-0.836	-0.876	-0.893								
0	RUA:SEC																
	11215																
0	0.654	4043.7	3035.7	508.6	6.891	88.4	0.003503	0.046	2	1117	-0.916	-0.758	-0.724	-0.668	-0.548	-0.436	-0.349
	-0.873	-0.722	-0.734	-0.627	-0.504	-0.408	-0.344	-0.293	-0.263	-0.238	-0.220	-0.238	-0.243	-0.243	-0.237	-0.249	-0.249
	-0.248	-0.228	-0.245	-0.879	-0.821	-0.804	-0.837	-0.878	-0.898								
0	RUA:SEC																
	11218																
0	0.654	4042.4	3033.6	507.6	6.863	89.7	0.003493	0.052	2	1119	-0.912	-0.754	-0.723	-0.644	-0.534	-0.419	-0.339
	-0.871	-0.720	-0.730	-0.629	-0.504	-0.413	-0.341	-0.291	-0.256	-0.230	-0.220	-0.234	-0.235	-0.236	-0.244	-0.250	-0.250
	-0.227	-0.224	-0.244	-0.876	-0.829	-0.810	-0.838	-0.884	-0.888								
1151-560 Pr-1 IN-22	11217																
0	RUA:SEC																
	11218																
0	0.654	4042.7	3033.7	507.7	6.854	90.4	0.003489	0.043	2	1121	-0.909	-0.748	-0.721	-0.640	-0.530	-0.415	-0.338
	-0.883	-0.728	-0.738	-0.634	-0.505	-0.410	-0.348	-0.293	-0.258	-0.240	-0.228	-0.244	-0.245	-0.245	-0.237	-0.245	-0.245
	-0.240	-0.244	-0.244	-0.864	-0.815	-0.805	-0.828	-0.877	-0.903								
1151-560 Pr-1 IN-22	11217																
0	RUA:SEC																
	11218																
0	0.652	4042.0	3027.2	504.4	6.819	91.8	0.003482	0.043	2	1123	-0.910	-0.752	-0.717	-0.638	-0.525	-0.410	-0.335
	-0.867	-0.716	-0.725	-0.622	-0.500	-0.405	-0.337	-0.288	-0.253	-0.229	-0.217	-0.227	-0.226	-0.231	-0.237	-0.247	-0.247
	-0.275	-0.242	-0.254	-0.853	-0.804	-0.797	-0.811	-0.858	-0.886								
0	RUA:SEC																
	11219																
0	0.650	4044.7	3043.8	501.4	6.799	92.6	0.003483	0.046	2	1125	-0.912	-0.752	-0.725	-0.642	-0.528	-0.416	-0.334
	-0.876	-0.725	-0.738	-0.631	-0.505	-0.422	-0.339	-0.291	-0.257	-0.232	-0.219	-0.239	-0.234	-0.236	-0.237	-0.250	-0.250
	-0.276	-0.240	-0.256	-0.862	-0.811	-0.805	-0.828	-0.870	-0.897								
0	RUA:SEC																
	11219																
0	0.652	4044.4	3037.5	506.2	6.807	93.1	0.003475	0.042	2	1127	-0.912	-0.741	-0.719	-0.654	-0.538	-0.424	-0.347
	-0.882	-0.726	-0.730	-0.636	-0.509	-0.415	-0.336	-0.286	-0.252	-0.232	-0.214	-0.234	-0.235	-0.235	-0.232	-0.244	-0.244
	-0.225	-0.220	-0.242	-0.874	-0.814	-0.808	-0.824	-0.866	-0.887								
1151-560 Pr-1 IN-22	11211																
0	RUA:SEC																
	11211																
0	0.651	4043.4	3040.9	502.6	6.784	93.7	0.003474	0.043	2	1129	-0.917	-0.751	-0.724	-0.647	-0.535	-0.422	-0.345
	-0.868	-0.718	-0.726	-0.627	-0.505	-0.415	-0.338	-0.290	-0.257	-0.231	-0.220	-0.232	-0.235	-0.234	-0.244	-0.254	-0.254
	-0.281	-0.250	-0.259	-0.859	-0.810	-0.804	-0.823	-0.863	-0.881								

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0	RUM:SEU	11212	4032.7	3042.4	300.9	6.768	94.4	0.003471	0.039	2	1131	0.922	-0.752	-0.730	-0.650	-0.534	-0.424	-0.347
0		0.650	-0.728	-0.740	-0.635	-0.507	-0.417	-0.340	-0.293	-0.254	-0.248	-0.243	-0.254	-0.248	-0.240	-0.243	-0.243	-0.250
0		-0.832	-0.224	-0.241	-0.862	-0.810	-0.794	-0.830	-0.863	-0.915	-0.234	-0.234	-0.234	-0.248	-0.240	-0.243	-0.243	-0.250
0		-0.291	-0.224	-0.241	-0.862	-0.810	-0.794	-0.830	-0.863	-0.915	-0.234	-0.234	-0.234	-0.248	-0.240	-0.243	-0.243	-0.250
0	RUM:SFC	11213	4044.0	3042.5	901.0	6.757	95.3	0.003465	0.040	2	1133	-0.910	-0.767	-0.725	-0.652	-0.545	-0.432	-0.353
0		0.651	-0.719	-0.734	-0.673	-0.505	-0.408	-0.348	-0.297	-0.263	-0.235	-0.235	-0.235	-0.242	-0.239	-0.240	-0.239	-0.238
0		-0.850	-0.227	-0.248	-0.869	-0.817	-0.804	-0.825	-0.866	-0.894	-0.234	-0.234	-0.234	-0.248	-0.240	-0.243	-0.243	-0.250
0		-0.291	-0.224	-0.241	-0.862	-0.810	-0.794	-0.830	-0.863	-0.915	-0.234	-0.234	-0.234	-0.248	-0.240	-0.243	-0.243	-0.250
0	RUM:SEC	11214	4045.4	3044.5	901.4	6.751	95.7	0.003465	0.041	2	1135	-0.909	-0.752	-0.713	-0.649	-0.535	-0.423	-0.343
0		0.650	-0.725	-0.736	-0.641	-0.516	-0.419	-0.337	-0.287	-0.252	-0.240	-0.240	-0.240	-0.242	-0.241	-0.233	-0.243	-0.243
0		-0.879	-0.248	-0.263	-0.869	-0.817	-0.804	-0.825	-0.866	-0.894	-0.234	-0.234	-0.234	-0.248	-0.240	-0.243	-0.243	-0.250
0		-0.291	-0.224	-0.241	-0.862	-0.810	-0.794	-0.830	-0.863	-0.915	-0.234	-0.234	-0.234	-0.248	-0.240	-0.243	-0.243	-0.250
0	1131-560 PT-1 1A-22 11311	11311	4035.3	3032.7	903.7	6.820	99.5	0.003493	0.042	15	1245	-0.919	-0.762	-0.726	-0.643	-0.533	-0.419	-0.337
0		0.652	-0.727	-0.730	-0.626	-0.504	-0.414	-0.348	-0.299	-0.262	-0.237	-0.237	-0.237	-0.238	-0.235	-0.239	-0.240	-0.249
0		-0.877	-0.247	-0.263	-0.861	-0.809	-0.794	-0.819	-0.860	-0.889	-0.237	-0.237	-0.237	-0.238	-0.235	-0.239	-0.240	-0.249
0		-0.291	-0.224	-0.241	-0.862	-0.810	-0.794	-0.830	-0.863	-0.915	-0.234	-0.234	-0.234	-0.248	-0.240	-0.243	-0.243	-0.250
0	RUM:SEC	11312	4046.0	3039.0	905.2	6.801	91.0	0.003490	0.046	15	1247	-0.919	-0.754	-0.720	-0.641	-0.529	-0.417	-0.341
0		0.653	-0.736	-0.736	-0.633	-0.507	-0.415	-0.344	-0.297	-0.260	-0.236	-0.236	-0.236	-0.241	-0.237	-0.242	-0.233	-0.245
0		-0.875	-0.241	-0.263	-0.869	-0.823	-0.819	-0.836	-0.877	-0.891	-0.236	-0.236	-0.236	-0.241	-0.237	-0.242	-0.233	-0.245
0		-0.291	-0.224	-0.241	-0.862	-0.810	-0.794	-0.830	-0.863	-0.915	-0.234	-0.234	-0.234	-0.248	-0.240	-0.243	-0.243	-0.250
0	RUM:SEU	11313	4042.6	3034.6	906.9	6.813	92.8	0.003474	0.043	15	1250	-0.914	-0.754	-0.726	-0.651	-0.538	-0.429	-0.350
0		0.653	-0.743	-0.736	-0.637	-0.513	-0.419	-0.347	-0.297	-0.263	-0.236	-0.236	-0.236	-0.241</				

0	0.652	4041.0	3038.0	903.6	6.776	96.4	0.003467	0.042	15	1254	-0.733	-0.655	-0.590	-0.437	-0.353
	-0.992	-0.740	-0.726	-0.639	-0.914	-0.422	-0.347	-0.298	-0.263	-0.924	-0.746	-0.650	-0.590	-0.437	-0.353
	-0.256	-0.255	-0.241	-0.862	-0.809	-0.791	-0.824	-0.863	-0.896	-0.237	-0.228	-0.241	-0.240	-0.240	-0.247
0	RUN:SEC														
	11216														
0	0.652	4043.6	3037.4	903.6	6.815	92.4	0.003479	0.047	15	1256	-0.729	-0.650	-0.537	-0.419	-0.344
	-0.879	-0.737	-0.731	-0.626	-0.501	-0.417	-0.348	-0.296	-0.260	-0.920	-0.757	-0.650	-0.537	-0.419	-0.344
	-0.270	-0.251	-0.289	-0.874	-0.821	-0.803	-0.833	-0.882	-0.890	-0.238	-0.221	-0.243	-0.241	-0.241	-0.248
0	RUN:SEC														
	11217														
0	0.652	4042.7	3037.6	904.7	6.799	53.2	0.003474	0.044	15	1258	-0.726	-0.645	-0.535	-0.419	-0.340
	-0.864	-0.726	-0.722	-0.620	-0.498	-0.409	-0.343	-0.296	-0.260	-0.923	-0.787	-0.645	-0.535	-0.419	-0.340
	-0.286	-0.248	-0.256	-0.869	-0.818	-0.804	-0.830	-0.868	-0.889	-0.241	-0.224	-0.244	-0.243	-0.236	-0.246
0	RUN:SEC														
	11218														
0	0.652	4044.0	3037.7	904.7	6.789	93.8	0.003470	0.044	15	1300	-0.747	-0.639	-0.531	-0.428	-0.346
	-0.849	-0.750	-0.723	-0.616	-0.453	-0.404	-0.337	-0.291	-0.255	-0.914	-0.747	-0.639	-0.531	-0.428	-0.346
	-0.295	-0.245	-0.258	-0.858	-0.803	-0.795	-0.819	-0.866	-0.895	-0.239	-0.223	-0.244	-0.243	-0.231	-0.238
1151-560 FH-1 TA-22	11219														
0	RUN:SEC														
	11215														
0	0.652	4043.6	3038.0	903.1	6.782	94.4	0.003467	0.044	15	1301	-0.753	-0.636	-0.521	-0.408	-0.337
	-0.874	-0.735	-0.727	-0.627	-0.504	-0.416	-0.337	-0.289	-0.245	-0.909	-0.753	-0.636	-0.521	-0.408	-0.337
	-0.282	-0.242	-0.250	-0.859	-0.810	-0.809	-0.823	-0.862	-0.883	-0.231	-0.213	-0.231	-0.240	-0.232	-0.242
0	RUN:SEC														
	11210														
0	0.651	4044.0	3041.5	902.7	6.767	94.9	0.003467	0.045	15	1304	-0.725	-0.643	-0.534	-0.422	-0.348
	-0.870	-0.725	-0.727	-0.614	-0.488	-0.399	-0.338	-0.286	-0.251	-0.917	-0.753	-0.643	-0.534	-0.422	-0.348
	-0.250	-0.248	-0.233	-0.856	-0.811	-0.788	-0.823	-0.866	-0.900	-0.238	-0.226	-0.242	-0.241	-0.235	-0.242
0	RUN:SEC														
	11413														
0	0.651	2504.0	2184.5	647.6	5.004	82.2	0.002548	0.034	3	1422	-0.740	-0.610	-0.498	-0.383	-0.320
	-0.885	-0.700	-0.697	-0.604	-0.481	-0.389	-0.307	-0.257	-0.225	-0.902	-0.740	-0.610	-0.498	-0.383	-0.320
	-0.268	-0.230	-0.212	-0.830	-0.781	-0.774	-0.803	-0.836	-0.867	-0.205	-0.188	-0.219	-0.215	-0.203	-0.209
0	RUN:SEC														
	11412														
0	0.653	2522.0	2144.4	654.8	5.035	83.0	0.002357	0.038	3	1423	-0.791	-0.606	-0.495	-0.382	-0.315
	-0.870	-0.650	-0.634	-0.598	-0.476	-0.385	-0.301	-0.253	-0.221	-0.898	-0.791	-0.606	-0.495	-0.382	-0.315
	-0.262	-0.222	-0.211	-0.831	-0.788	-0.786	-0.811	-0.850	-0.883	-0.203	-0.188	-0.217	-0.219	-0.208	-0.215

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0	0.653	2520.3	2193.0	654.5	5.110	76.0	0.002599	0.046	4	945	-0.914	-0.744	-0.714	-0.601	-0.491	-0.381	-0.324
	-0.879	-0.655	-0.696	-0.613	-0.485	-0.393	-0.306	-0.260	-0.229	-0.211	-0.197	-0.230	-0.230	-0.233	-0.206	-0.213	-0.213
	-0.272	-0.225	-0.515	-0.937	-0.706	-0.708	-0.824	-0.860	-0.871	-0.211	-0.197	-0.230	-0.230	-0.233	-0.206	-0.213	-0.213
	ATS1-560 PH-1	1A-22	11514	10-PRESSOUT3	10 JAN 83	17143	PAGE 39										
0	RUA1SEC																
	11514																
0	0.653	2517.9	2191.6	653.7	5.097	77.3	0.002581	0.056	4	949	-0.906	-0.745	-0.707	-0.590	-0.477	-0.365	-0.305
	-0.881	-0.698	-0.693	-0.602	-0.487	-0.394	-0.302	-0.254	-0.223	-0.210	-0.194	-0.221	-0.224	-0.229	-0.206	-0.210	-0.210
	-0.254	-0.220	-0.902	-0.826	-0.777	-0.795	-0.810	-0.850	-0.880	-0.210	-0.194	-0.221	-0.224	-0.229	-0.206	-0.210	-0.210
0	ALA1SEC																
	11515																
0	0.653	2520.3	2192.8	654.6	5.070	80.0	0.002570	0.046	4	1006	-0.905	-0.744	-0.709	-0.604	-0.488	-0.376	-0.313
	-0.864	-0.687	-0.682	-0.593	-0.470	-0.381	-0.312	-0.261	-0.230	-0.210	-0.195	-0.219	-0.219	-0.222	-0.198	-0.207	-0.207
	-0.263	-0.229	-0.508	-0.929	-0.782	-0.784	-0.810	-0.845	-0.868	-0.210	-0.195	-0.219	-0.219	-0.222	-0.198	-0.207	-0.207
0	RUA1SEC																
	11516																
0	0.652	2919.6	2193.7	653.4	5.062	80.2	0.002569	0.048	4	1008	-0.903	-0.742	-0.710	-0.603	-0.492	-0.379	-0.317
	-0.361	-0.559	-0.659	-0.609	-0.491	-0.396	-0.307	-0.255	-0.224	-0.208	-0.193	-0.228	-0.216	-0.219	-0.208	-0.209	-0.209
	-0.267	-0.225	-0.509	-0.829	-0.780	-0.790	-0.815	-0.852	-0.864	-0.208	-0.193	-0.228	-0.216	-0.219	-0.208	-0.209	-0.209
0	MUA1SEC																
	11517																
0	0.653	2521.5	2194.1	654.4	5.065	80.4	0.002569	0.049	4	1022	-0.912	-0.754	-0.712	-0.613	-0.496	-0.384	-0.325
	-0.875	-0.701	-0.702	-0.615	-0.492	-0.396	-0.315	-0.263	-0.233	-0.212	-0.193	-0.228	-0.229	-0.228	-0.216	-0.216	-0.216
	-0.276	-0.229	-0.921	-0.828	-0.789	-0.793	-0.819	-0.857	-0.870	-0.212	-0.193	-0.228	-0.229	-0.228	-0.216	-0.216	-0.216
	ATS1-560 PH-1	1A-22	11621	10-PRESSOUT3	10 JAN 83	17143	PAGE 40										
0	RUA1SEC																
	11621																
0	0.654	2514.1	2189.6	654.5	5.136	74.2	0.002593	0.058	5	1220	-0.895	-0.716	-0.693	-0.602	-0.483	-0.372	-0.312
	-0.883	-0.662	-0.673	-0.584	-0.462	-0.365	-0.293	-0.244	-0.200	-0.200	-0.185	-0.219	-0.218	-0.217	-0.205	-0.210	-0.210
	-0.225	-0.220	-0.502	-0.827	-0.778	-0.790	-0.806	-0.845	-0.877	-0.200	-0.185	-0.219	-0.218	-0.217	-0.205	-0.210	-0.210
0	ALA1SEC																
	11622																
0	0.652	2524.8	2197.4	654.6	5.008	78.0	0.002584	0.049	5	1227	-0.894	-0.721	-0.694	-0.589	-0.469	-0.362	-0.303
	-0.876	-0.655	-0.692	-0.602	-0.475	-0.383	-0.296	-0.249	-0.219	-0.202	-0.182	-0.221	-0.220	-0.220	-0.208	-0.213	-0.213
	-0.227	-0.220	-0.500	-0.825	-0.777	-0.791	-0.800	-0.840	-0.871	-0.202	-0.182	-0.221	-0.220	-0.220	-0.208	-0.213	-0.213
0	RUA1SEC																
	11623																
0	0.653	2921.5	2194.0	654.7	5.065	80.5	0.002569	0.056	5	1244	-0.892	-0.722	-0.697	-0.595	-0.486	-0.380	-0.315
	-0.859	-0.680	-0.679	-0.593	-0.474	-0.377	-0.296	-0.250	-0.220	-0.200	-0.184	-0.210	-0.210	-0.216	-0.201	-0.204	-0.204
	-0.263	-0.226	-0.896	-0.821	-0.767	-0.771	-0.795	-0.836	-0.868	-0.199	-0.184	-0.210	-0.210	-0.216	-0.201	-0.204	-0.204

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